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DISEÑO ESTRUCTURAL CONSTRUCCION CUBIERTA CON ILUMINACION DEL POLIDEPORTIVO DE LA VEREDA EL CEDRO DEL MUNICIPIO DE TARQUI HUILA

ALCALDIA MUNICIPAL

PITALITO, AGOSTO DE 2024

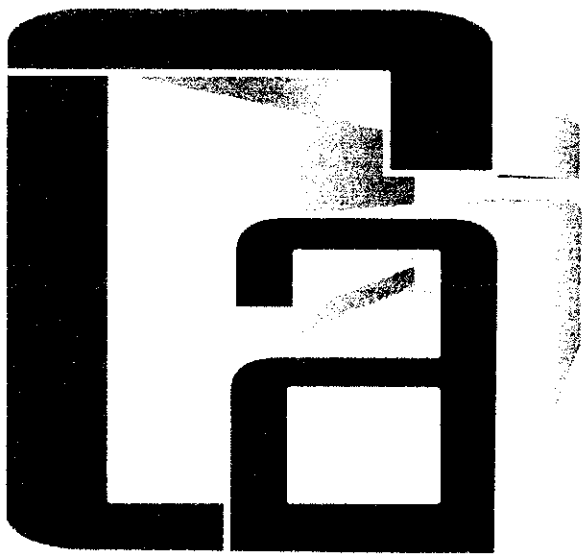
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DISEÑO ESTRUCTURAL CONSTRUCCION CUBIERTA CON ILUMINACION DEL POLIDEPORTIVO DE LA VEREDA EL CEDRO DEL MUNICIPIO DE TARQUI HUILA



MEMORIAS DE CALCULO

ING. GERMAN A. LOZADA LOZADA

PITALITO, JULIO DE 2024

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MEMORIAS DE CÁLCULO

INTRODUCCION

A lo largo de la historia el hombre ha tenido que construir estructuras que le permitan satisfacer sus necesidades, desde las más básicas como las de un hogar donde protegerse del clima, hasta otras sofisticadas como puentes, captaciones de agua, plantas de tratamiento o estructuras metálicas como cubiertas. Todas estas estructuras se han ido adaptando a lo largo del tiempo debido a varios factores, como los materiales disponibles para su construcción, las condiciones climáticas, la estética, el tipo de suelo, los recursos económicos, los avances tecnológicos, pero sobre todo, para asegurar la permanencia de lo que se ha construido ante los diferentes movimientos telúricos, que ha sido el principal problema para establecer un mínimo de seguridad en las construcciones y es, a través de la experiencia, que el hombre ha modificado y regulado la forma de hacer las edificaciones estableciendo códigos y reglamentos particulares a las necesidades de la zona donde se construye

Una estructura diseñada debe seguir los requisitos consagrados en la Norma Colombiana Sismo Resistente, debe ser capaz de resistir, además de las fuerzas que le impone su uso, temblores de poca intensidad sin daño, temblores moderados sin daño estructural, pero posiblemente con algún daño en elementos no estructurales y un temblor fuerte con daños a elementos estructurales y no estructurales, pero sin colapso

El presente informe corresponde a las memorias de diseño estructural de un proyecto arquitectónico de la cubierta de un polideportivo con sistema estructural de pórticos a momento en estructura metálica con pedestales en concreto que se describe a continuación, de igual manera, se informa que este documento contiene los criterios y especificaciones generales de análisis y diseño de la estructura de acuerdo con lo establecido en la Ley 400 de 1997, Decretos 926 de 2010,2525 de 2010, 092 de 2011, 340 de 2012, 0945 e 2017 y 2113 de 2019 Reglamento Colombiano de Construcción Sismo Resistente NSR-10

1. MARCO TEORICO

El marco teórico para el diseño de la cubierta metálica se basa en la normativa de construcción vigente (NSR10 y AISC 360-16 LRFD), los principios de la ingeniería estructural y las especificaciones del proyecto, considerando la geometría, la tipología de la cubierta, los materiales, las cargas (vivas y muertas), y los sistemas de evacuación de agua, todo esto adaptado a las condiciones climáticas y funcionales. Los componentes

principales de este diseño incluyen el análisis de cargas, la selección de elementos estructurales (columnas, vigas, cerchas, etc) y los sistemas de soporte (marcos rígidos, contravientos), así como la aplicación de principios para garantizar la estabilidad, durabilidad y eficiencia de la estructura.

2. DESCRIPCION DE LA ESTRUCTURA

Diseño estructural de una Cubierta metálica para el polideportivo de la Vereda El Cedro del Municipio de Tarqui en el Departamento del Hula, es una estructura de pórticos a momento en estructura metálica con capacidad especial de disipación de energía (DES) en una zona considerada de alta sismicidad.

La estructura diseñada y descrita anteriormente consta de pórticos de acero conformados por Perfiles Estructurales Tubulares Circulares (PETC) y correas en perfil en C doble. Su cimentación consta de zapatas aisladas con vigas de cimentación en concreto reforzado y contrapesos en concreto simple. De igual manera, se diseñó pedestales en concreto reforzado para sostener la estructura metálica. Este diseño se realizó con el programa CYPE3D, versión 2023g y con licencia No 111068.

3. CARACTERISTICAS GENERALES DE LA ESTRUCTURA

3.1. Datos de la Obra se presenta lo siguiente:

- La versión del programa y su número de licencia: Programa basado en elementos finitos.
- Normas consideradas
- Datos generales del sismo
  - Aa 0.30 g
  - Av 0.15 g
  - Vm 170 m/s
- Acciones consideradas: Las cargas consideradas se especifican en el anexo **Valoración de Cargas** de acuerdo con el uso de la edificación.
  - Grupo de Uso I
  - Coeficiente de importancia I =1.00
  - Carga viva en cubierta (≤ 15%) 50 kgf/m2
  - Carga muerta en cubierta 160 kgf/m2
  - El peso propio de los elementos el programa los calcula automáticamente
- Método de cálculo: *Análisis dinámico espectral*
- Irregularidades
  - Coeficiente de irregularidad en altura $\phi a = 1.00$
  - Coeficiente de irregularidad en planta $\phi p = 1.00$
- Coeficientes por ausencia de redundancia $\phi_{rx} = 1.00$

$\phi_{ry} = 0.75$

- Materiales utilizados:
  - Concreto e cimentación f'c = 245 kp/cm2
  - Concreto de losas, vigas y columnas f'c = 210 kp/cm2
  - Aceros grados 60 fy = 4200 kp/cm2

3.2. Análisis y resultados de la estructura

Las cargas sobre las barras, hipótesis, valores y direcciones de la misma están en el Capítulo 2. Estructuras de la página 3 a la página 101, con sus respectivas comprobaciones.

El análisis y resultados de los pedestales y la cimentación se encuentra a partir de la página 101

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Listados

1. DATOS DE OBRA

1.1. Normas consideradas

Cimentación: NSR-10

Acero conformado: AISI S100-2016 (LRFD)

Aceros laminados y armados: ANSI/AISC 360-16 (LRFD)

Hormigón: NSR-10

Categoría de uso: Cubiertas

1.2. Sismo

Norma utilizada: NSR-10

Reglamento Colombiano de Construcción Sismo Resistente (2010)

Método de cálculo: Análisis dinámico espectral (NSR-10, A.3.4.2.2)

1.2.1. Datos generales de sismo

Caracterización del emplazamiento

A_a: Aceleración horizontal pico efectiva (NSR-10, A.2.2)	A_a : 0.30 g
A_v: Velocidad horizontal pico efectiva (NSR-10, A.2.2)	A_v : 0.15 g
V_m: Velocidad media de onda de cortante (NSR-10, A.2.4.3)	V_m : 170.00 m/s

Sistema estructural

R_{0X}: Coeficiente de disipación de energía básico (X) (NSR-10, A.3)	R_{0X} : 1.35
R_{0Y}: Coeficiente de disipación de energía básico (Y) (NSR-10, A.3)	R_{0Y} : 1.35
Φ_a: Coeficiente de irregularidad en altura (NSR-10, A.3.3.5)	Φ_a : 1.00
Φ_p: Coeficiente de irregularidad en planta (NSR-10, A.3.3.4)	Φ_p : 1.00
Φ_{rX}: Coeficiente por ausencia de redundancia (X) (NSR-10, A.3.3.8)	Φ_{rX} : 1.00
Φ_{rY}: Coeficiente por ausencia de redundancia (Y) (NSR-10, A.3.3.8)	Φ_{rY} : 0.75

Geometría en altura (NSR-10, A.3.3.4 y A.3.3.5): Regular

Tipo de edificación (NSR-10, A.2.5): II

Se aplica reducción a todos los modos, excepto al fundamental

Parámetros de cálculo

Número de modos de vibración que intervienen en el análisis: Según norma	
Fracción de sobrecarga de uso	: 0.00
Fracción de sobrecarga de nieve	: 0.00
Factor multiplicador del espectro	: 1.00

Efectos de la componente sísmica vertical

No se consideran

Se realiza análisis de los efectos de 2º orden

Valor para multiplicar los desplazamientos 1.00

Direcciones de análisis

Acción sísmica según X

Acción sísmica según Y

2. ESTRUCTURA

2.1. Cargas

2.1.1. Barras

Referencias:

'P1', 'P2':

- Cargas puntuales, uniformes, en faja y momentos puntuales: 'P1' es el valor de la carga. 'P2' no se utiliza.
- Cargas trapeciales: 'P1' es el valor de la carga en el punto donde comienza (L1) y 'P2' es el valor de la carga en el punto donde termina (L2).
- Cargas triangulares: 'P1' es el valor máximo de la carga. 'P2' no se utiliza.
- Incrementos de temperatura: 'P1' y 'P2' son los valores de la temperatura en las caras exteriores o paramentos de la pieza. La orientación de la variación del incremento de temperatura sobre la sección transversal dependerá de la dirección seleccionada.

'L1', 'L2':

- Cargas y momentos puntuales: 'L1' es la distancia entre el nudo inicial de la barra y la posición donde se aplica la carga. 'L2' no se utiliza.
- Cargas trapeciales, en faja, y triangulares: 'L1' es la distancia entre el nudo inicial de la barra y la posición donde comienza la carga, 'L2' es la distancia entre el nudo inicial de la barra y la posición donde termina la carga.

Unidades:

- Cargas puntuales: t
- Momentos puntuales: t·m.
- Cargas uniformes, en faja, triangulares y trapeciales: t/m.
- Incrementos de temperatura: °C.

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N1/N7	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N7/N8	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N8/N9	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N9/N5	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N9/N13	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N13/N6	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N1/N10	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N10/N7	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N7/N11	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N11/N8	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N8/N12	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N12/N9	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N13/N5	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N4/N26	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N26/N27	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N27/N28	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N28/N22	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N26/N24	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N24/N27	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N27/N25	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N25/N28	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N28/N29	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N29/N23	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N29/N22	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N6/N14	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N14/N15	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N15/N16	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N16/N17	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N17/N18	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N18/N19	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N19/N20	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N20/N21	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N30/N21	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N31/N30	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N32/N31	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N34/N32	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N36/N34	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N40/N36	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N41/N40	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N23/N41	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N35/N33	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N37/N35	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N38/N37	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N39/N38	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N22/N39	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N32/N33	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N34/N33	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N34/N35	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N36/N35	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N36/N37	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N40/N37	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N40/N38	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N41/N38	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N41/N39	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N29/N39	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N2/N42	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N42/N43	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N43/N44	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N44/N45	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N44/N49	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N49/N46	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N42/N48	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N48/N43	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N43/N47	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N47/N44	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N49/N45	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N3/N50	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N50/N51	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N51/N52	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N52/N53	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N50/N56	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N56/N51	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N51/N55	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N55/N52	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N52/N57	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N57/N54	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N57/N53	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N46/N58	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N58/N59	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N59/N60	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N60/N61	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N61/N62	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N62/N63	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N63/N64	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N64/N65	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N66/N65	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N67/N66	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N68/N67	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N69/N68	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N70/N69	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N71/N70	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N72/N71	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N54/N72	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N74/N73	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N75/N74	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N76/N75	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N77/N76	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N53/N77	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N68/N73	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N69/N73	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N69/N74	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N70/N74	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N70/N75	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N71/N75	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N71/N76	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N72/N76	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N72/N77	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N57/N77	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N78/N42	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N2/N78	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N78/N10	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N42/N7	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N48/N11	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N43/N8	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N47/N12	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N44/N9	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N46/N6	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N45/N5	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N49/N13	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N58/N14	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N59/N15	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N60/N16	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N61/N17	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N62/N18	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N63/N19	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N64/N20	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N65/N21	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N66/N30	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N67/N31	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N68/N32	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N73/N33	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N69/N34	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N74/N35	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N70/N36	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N75/N37	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N71/N40	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N76/N38	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N72/N41	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N77/N39	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N54/N23	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N57/N29	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N53/N22	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N52/N28	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N55/N25	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N51/N27	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N56/N24	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N50/N26	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N73/N79	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N33/N80	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N68/N79	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N67/N79	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N32/N80	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N31/N80	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N79/N81	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N81/N82	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N80/N83	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N83/N84	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N79/N80	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N81/N83	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N82/N84	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N67/N81	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N66/N81	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N66/N82	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N65/N82	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N31/N83	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N30/N83	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N30/N84	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N21/N84	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N65/N85	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N64/N85	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N82/N85	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N86/N85	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N87/N86	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N88/N87	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N89/N88	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N90/N89	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N91/N90	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N92/N91	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N45/N92	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N64/N86	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N63/N86	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N63/N87	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N62/N87	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N62/N88	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N61/N88	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N61/N89	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N60/N89	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N60/N90	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N59/N90	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N59/N91	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N58/N91	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N58/N92	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N49/N92	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N21/N93	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N20/N93	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N20/N94	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N84/N93	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N94/N93	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N19/N94	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N95/N94	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N19/N95	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N18/N95	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N18/N96	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N96/N95	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N17/N96	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N97/N96	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N17/N97	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N16/N97	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N16/N98	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N98/N97	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N15/N98	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N99/N98	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N15/N99	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N14/N99	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N100/N99	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N14/N100	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N13/N100	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N5/N100	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N85/N93	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N86/N94	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N87/N95	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N88/N96	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N89/N97	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N90/N98	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N91/N99	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N92/N100	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N101/N102	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N102/N103	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N103/N104	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N104/N105	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N104/N106	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N101/N109	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N109/N102	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N102/N108	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N108/N103	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N103/N107	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N107/N104	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N106/N105	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N114/N110	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N110/N111	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N111/N112	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N112/N113	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N114/N118	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N118/N110	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N110/N117	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N117/N111	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N111/N116	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N116/N112	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N112/N115	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N115/N113	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N106/N119	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N119/N120	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N120/N121	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N121/N122	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N122/N123	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N123/N124	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N124/N125	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N125/N126	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N127/N126	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N128/N127	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N129/N128	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N130/N129	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N131/N130	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N132/N131	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N133/N132	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N115/N133	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N135/N134	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N136/N135	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N137/N136	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N138/N137	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N113/N138	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N129/N134	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N130/N134	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N130/N135	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N131/N135	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N131/N136	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N132/N136	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N132/N137	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N133/N137	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N133/N138	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N115/N138	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N143/N139	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N139/N140	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N140/N141	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N141/N142	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N141/N144	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N139/N145	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N145/N140	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N140/N146	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N146/N141	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N144/N142	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N151/N147	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N147/N148	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N148/N149	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N149/N150	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N155/N147	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N148/N153	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N153/N149	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N149/N152	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N152/N150	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N144/N156	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N156/N157	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N157/N158	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N158/N159	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N159/N160	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N160/N161	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N161/N162	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N162/N163	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N164/N163	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N165/N164	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N166/N165	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N167/N166	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N168/N167	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N169/N168	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N170/N169	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N152/N170	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N172/N171	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N173/N172	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N174/N173	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N175/N174	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N150/N175	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N166/N171	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N167/N171	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N167/N172	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N168/N172	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N168/N173	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N169/N173	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N169/N174	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N170/N174	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N170/N175	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N152/N175	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N151/N155	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N176/N139	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N143/N176	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N176/N109	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N139/N102	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N145/N108	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N141/N104	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N144/N106	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N142/N105	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N156/N119	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N157/N120	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N158/N121	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N159/N122	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N160/N123	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N161/N124	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N162/N125	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N163/N126	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N164/N127	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N165/N128	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N166/N129	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N171/N134	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N167/N130	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N172/N135	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N168/N131	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N173/N136	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N169/N132	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N174/N137	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N170/N133	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N175/N138	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N152/N115	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N150/N113	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N149/N112	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N153/N116	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N147/N110	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N155/N118	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N171/N177	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N134/N178	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N166/N177	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N165/N177	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N129/N178	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N128/N178	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N177/N179	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N179/N180	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N178/N181	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N181/N182	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N177/N178	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N179/N181	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N180/N182	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N165/N179	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N164/N179	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N164/N180	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N163/N180	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N128/N181	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N127/N181	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N127/N182	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N126/N182	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N163/N183	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N162/N183	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N180/N183	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N184/N183	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N185/N184	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N186/N185	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N187/N186	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N188/N187	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N189/N188	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N190/N189	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N142/N190	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N162/N184	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N161/N184	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N161/N185	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N160/N185	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N160/N186	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N159/N186	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N159/N187	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N158/N187	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N158/N188	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N157/N188	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N157/N189	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N156/N189	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N156/N190	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N144/N190	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N126/N191	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N125/N191	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N125/N192	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N182/N191	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N192/N191	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N124/N192	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N193/N192	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N124/N193	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N123/N193	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N123/N194	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N194/N193	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N122/N194	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N195/N194	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N122/N195	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N121/N195	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N121/N196	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N196/N195	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N120/N196	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N197/N196	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N120/N197	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N119/N197	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N198/N197	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N119/N198	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N106/N198	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N105/N198	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N183/N191	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N184/N192	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N185/N193	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N186/N194	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N187/N195	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N188/N196	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N189/N197	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N190/N198	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N113/N207	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N207/N208	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N208/N209	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N209/N210	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N210/N211	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N211/N212	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N212/N213	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N213/N214	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N214/N53	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N112/N206	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N206/N205	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N205/N204	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N204/N203	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N203/N202	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N202/N201	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N201/N200	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N200/N199	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N199/N52	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N52/N214	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N199/N214	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N199/N213	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N200/N213	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N200/N212	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N201/N212	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N201/N211	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N202/N211	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N202/N210	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N203/N210	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N203/N209	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N204/N209	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N204/N208	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N205/N208	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N205/N207	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N206/N207	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N206/N113	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N105/N215	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N215/N216	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N216/N217	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N217/N218	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N218/N219	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N219/N220	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N220/N221	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N221/N222	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N222/N45	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N104/N230	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N230/N229	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N229/N228	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N228/N227	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N227/N226	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N226/N225	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N225/N224	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N224/N223	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N223/N44	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N230/N105	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N230/N215	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N229/N215	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N229/N216	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N228/N216	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N228/N217	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N227/N217	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N227/N218	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N226/N218	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N226/N219	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N225/N219	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N225/N220	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N224/N220	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N224/N221	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N223/N221	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N223/N222	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N44/N222	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N231/N232	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N232/N233	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N233/N234	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N234/N235	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N234/N236	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N231/N239	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N239/N232	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N232/N238	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N238/N233	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N233/N237	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N237/N234	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N236/N235	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N244/N240	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N240/N241	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N241/N242	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N242/N243	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N244/N248	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N248/N240	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N240/N247	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N247/N241	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N241/N246	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N246/N242	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N242/N245	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N245/N243	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N236/N249	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N249/N250	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N250/N251	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N251/N252	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N252/N253	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N253/N254	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N254/N255	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N255/N256	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N257/N256	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N258/N257	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N259/N258	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N260/N259	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N261/N260	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N262/N261	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N263/N262	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N245/N263	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N265/N264	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N266/N265	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N267/N266	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N268/N267	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N243/N268	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N259/N264	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N260/N264	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N260/N265	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N261/N265	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N261/N266	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N262/N266	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N262/N267	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N263/N267	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N263/N268	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N245/N268	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N273/N269	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N269/N270	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N270/N271	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N271/N272	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N271/N274	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N269/N275	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N275/N270	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N270/N276	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N276/N271	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N274/N272	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N281/N277	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N277/N278	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N278/N279	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N279/N280	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N285/N277	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N277/N284	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N284/N278	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N278/N283	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N283/N279	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N279/N282	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N282/N280	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N274/N286	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N286/N287	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N287/N288	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N288/N289	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N289/N290	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N290/N291	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N291/N292	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N292/N293	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N294/N293	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N295/N294	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N296/N295	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N297/N296	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N298/N297	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N299/N298	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N300/N299	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N282/N300	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N302/N301	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N303/N302	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N304/N303	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N305/N304	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N280/N305	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N296/N301	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N297/N301	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N297/N302	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N298/N302	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N298/N303	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N299/N303	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N299/N304	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N300/N304	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N300/N305	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N282/N305	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N281/N285	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N306/N269	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N273/N306	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N306/N239	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N269/N232	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N275/N238	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N270/N233	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N276/N237	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N271/N234	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N274/N236	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N272/N235	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N286/N249	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N287/N250	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N288/N251	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N289/N252	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N290/N253	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N291/N254	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N292/N255	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N293/N256	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N294/N257	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N295/N258	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N296/N259	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N301/N264	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N297/N260	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N302/N265	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N298/N261	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N303/N266	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N299/N262	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N304/N267	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N300/N263	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N305/N268	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N282/N245	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N280/N243	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N279/N242	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N283/N246	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N278/N241	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N284/N247	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N277/N240	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N285/N248	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N301/N307	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N264/N308	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N296/N307	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N295/N307	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N259/N308	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N258/N308	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N307/N309	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N309/N310	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N308/N311	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N311/N312	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N307/N308	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N309/N311	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N310/N312	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N295/N309	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N294/N309	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N294/N310	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N293/N310	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N258/N311	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N257/N311	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N257/N312	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N256/N312	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N293/N313	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N292/N313	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N310/N313	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N314/N313	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N315/N314	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N316/N315	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N317/N316	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N318/N317	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N319/N318	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N320/N319	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N272/N320	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N292/N314	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N291/N314	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N291/N315	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N290/N315	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N290/N316	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N289/N316	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N289/N317	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N288/N317	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N288/N318	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N287/N318	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N287/N319	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N286/N319	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N286/N320	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N274/N320	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N256/N321	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N255/N321	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N255/N322	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N312/N321	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N322/N321	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N254/N322	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N323/N322	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N254/N323	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N253/N323	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N253/N324	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N324/N323	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N252/N324	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N325/N324	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N252/N325	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N251/N325	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N251/N326	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N326/N325	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N250/N326	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N327/N326	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N250/N327	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N249/N327	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N328/N327	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N249/N328	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N236/N328	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N235/N328	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N313/N321	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N314/N322	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N315/N323	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N316/N324	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N317/N325	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N318/N326	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N319/N327	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N320/N328	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N329/N330	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N330/N331	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N331/N332	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N332/N333	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N332/N334	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N329/N337	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N337/N330	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N330/N336	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N336/N331	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N331/N335	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N335/N332	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N334/N333	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N342/N338	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N338/N339	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N339/N340	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N340/N341	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N342/N346	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N346/N338	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N338/N345	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N345/N339	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N339/N344	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N344/N340	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N340/N343	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N343/N341	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N334/N347	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N347/N348	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N348/N349	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N349/N350	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N350/N351	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N351/N352	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N352/N353	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N353/N354	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N355/N354	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N356/N355	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N357/N356	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N358/N357	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N359/N358	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N360/N359	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N361/N360	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N343/N361	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N363/N362	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N364/N363	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N365/N364	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N366/N365	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N341/N366	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N357/N362	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N358/N362	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N358/N363	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N359/N363	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N359/N364	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N360/N364	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N360/N365	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N361/N365	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N361/N366	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N343/N366	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N371/N367	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N367/N368	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N368/N369	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N369/N370	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N369/N372	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N367/N373	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N373/N368	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N368/N374	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N374/N369	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N372/N370	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N379/N375	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N375/N376	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N376/N377	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N377/N378	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N383/N375	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N375/N382	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N382/N376	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N376/N381	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N381/N377	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N377/N380	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N380/N378	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N372/N384	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N384/N385	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N385/N386	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N386/N387	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N387/N388	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N388/N389	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N389/N390	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N390/N391	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N392/N391	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N393/N392	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N394/N393	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N395/N394	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N396/N395	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N397/N396	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N398/N397	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N380/N398	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N400/N399	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N401/N400	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N402/N401	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N403/N402	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N378/N403	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N394/N399	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N395/N399	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N395/N400	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N396/N400	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N396/N401	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N397/N401	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N397/N402	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N398/N402	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N398/N403	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N380/N403	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N379/N383	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N404/N367	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N371/N404	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N404/N337	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N367/N330	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N373/N336	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N368/N331	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N374/N335	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N369/N332	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N372/N334	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N370/N333	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N384/N347	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N385/N348	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N386/N349	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N387/N350	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N388/N351	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N389/N352	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N390/N353	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N391/N354	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N392/N355	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N393/N356	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N394/N357	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N399/N362	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N395/N358	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N400/N363	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N396/N359	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N401/N364	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N397/N360	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N402/N365	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N398/N361	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N403/N366	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N380/N343	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N378/N341	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N377/N340	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N381/N344	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N376/N339	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N382/N345	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N375/N338	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N383/N346	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N399/N405	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N362/N406	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N394/N405	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N393/N405	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N357/N406	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N356/N406	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N405/N407	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N407/N408	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N406/N409	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N409/N410	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N405/N406	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N407/N409	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N408/N410	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N393/N407	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N392/N407	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N392/N408	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N391/N408	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N356/N409	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N355/N409	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N355/N410	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N354/N410	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N391/N411	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N390/N411	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N408/N411	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N412/N411	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N413/N412	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N414/N413	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N415/N414	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N416/N415	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N417/N416	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N418/N417	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N370/N418	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N390/N412	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N389/N412	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N389/N413	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N388/N413	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N388/N414	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N387/N414	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N387/N415	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N386/N415	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N386/N416	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N385/N416	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N385/N417	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N384/N417	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N384/N418	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N372/N418	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N354/N419	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N353/N419	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N353/N420	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N410/N419	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N420/N419	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N352/N420	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N421/N420	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N352/N421	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N351/N421	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N351/N422	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N422/N421	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N350/N422	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N423/N422	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N350/N423	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N349/N423	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N349/N424	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N424/N423	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N348/N424	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N425/N424	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N348/N425	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N347/N425	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N426/N425	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N347/N426	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N334/N426	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N333/N426	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N411/N419	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N412/N420	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N413/N421	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N414/N422	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N415/N423	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N416/N424	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N417/N425	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N418/N426	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N341/N434	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N434/N433	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N433/N432	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N432/N431	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N431/N430	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N430/N429	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N429/N428	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N428/N427	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N427/N280	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N340/N435	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N435/N436	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N436/N437	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N437/N438	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N438/N439	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N439/N440	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N440/N441	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N441/N442	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N442/N279	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N279/N427	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N442/N427	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N442/N428	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N441/N428	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N441/N429	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N440/N429	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N440/N430	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N439/N430	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N439/N431	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N438/N431	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N438/N432	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N437/N432	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N437/N433	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N436/N433	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N436/N434	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N435/N434	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N435/N341	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N333/N443	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N443/N444	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N444/N445	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N445/N446	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N446/N447	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N447/N448	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N448/N449	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N449/N450	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N450/N272	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N332/N458	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N458/N457	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N457/N456	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N456/N455	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N455/N454	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N454/N453	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N453/N452	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N452/N451	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N451/N271	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N458/N333	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N458/N443	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N457/N443	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N457/N444	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N456/N444	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N456/N445	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N455/N445	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N455/N446	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N454/N446	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N454/N447	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N453/N447	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N453/N448	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N452/N448	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N452/N449	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N451/N449	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N451/N450	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N271/N450	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N459/N460	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N460/N461	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N461/N462	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N462/N463	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N462/N464	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N459/N467	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N467/N460	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N460/N466	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N466/N461	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N461/N465	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N465/N462	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N464/N463	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N472/N468	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N468/N469	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N469/N470	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N470/N471	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N472/N476	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N476/N468	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N468/N475	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N475/N469	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N469/N474	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N474/N470	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N470/N473	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N473/N471	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N464/N477	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N477/N478	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N478/N479	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N479/N480	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N480/N481	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N481/N482	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N482/N483	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N483/N484	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N485/N484	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N486/N485	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N487/N486	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N488/N487	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N489/N488	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N490/N489	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N491/N490	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N473/N491	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N493/N492	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N494/N493	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N495/N494	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N496/N495	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N471/N496	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N487/N492	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N488/N492	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N488/N493	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N489/N493	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N489/N494	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N490/N494	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N490/N495	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N491/N495	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N491/N496	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N473/N496	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N501/N497	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N497/N498	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N498/N499	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N499/N500	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N499/N502	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N497/N503	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N503/N498	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N498/N504	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N504/N499	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N502/N500	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N509/N505	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N505/N506	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N506/N507	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N507/N508	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N513/N505	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N505/N512	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N512/N506	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N506/N511	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N511/N507	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N507/N510	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N510/N508	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N502/N514	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N514/N515	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N515/N516	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N516/N517	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N517/N518	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N518/N519	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N519/N520	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N520/N521	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N522/N521	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N523/N522	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N524/N523	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N525/N524	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N526/N525	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N527/N526	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N528/N527	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N510/N528	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N530/N529	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N531/N530	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N532/N531	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N533/N532	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N508/N533	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N524/N529	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N525/N529	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N525/N530	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N526/N530	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N526/N531	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N527/N531	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N527/N532	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N528/N532	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N528/N533	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N510/N533	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N509/N513	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N534/N497	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N501/N534	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N534/N467	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N497/N460	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N503/N466	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N498/N461	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N504/N465	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N499/N462	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N502/N464	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N500/N463	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N514/N477	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N515/N478	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N516/N479	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N517/N480	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N518/N481	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N519/N482	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N520/N483	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N521/N484	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N522/N485	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N523/N486	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N524/N487	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N529/N492	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N525/N488	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N530/N493	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N526/N489	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N531/N494	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N527/N490	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N532/N495	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N528/N491	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N533/N496	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N510/N473	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N508/N471	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N507/N470	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N511/N474	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N506/N469	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N512/N475	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N505/N468	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N513/N476	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N529/N535	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N492/N536	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N524/N535	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N523/N535	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N487/N536	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N486/N536	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N535/N537	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N537/N538	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N536/N539	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N539/N540	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N535/N536	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N537/N539	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N538/N540	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N523/N537	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N522/N537	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N522/N538	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N521/N538	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N486/N539	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N485/N539	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N485/N540	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N484/N540	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N521/N541	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N520/N541	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N538/N541	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N542/N541	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N543/N542	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N544/N543	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N545/N544	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N546/N545	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N547/N546	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N548/N547	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N500/N548	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N520/N542	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N519/N542	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N519/N543	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N518/N543	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N518/N544	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N517/N544	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N517/N545	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N516/N545	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N516/N546	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N515/N546	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N515/N547	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N514/N547	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N514/N548	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N502/N548	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N484/N549	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N483/N549	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N483/N550	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N540/N549	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N550/N549	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N482/N550	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N551/N550	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N482/N551	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N481/N551	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N481/N552	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N552/N551	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N480/N552	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N553/N552	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N480/N553	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N479/N553	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N479/N554	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N554/N553	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N478/N554	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N555/N554	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N478/N555	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N477/N555	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N556/N555	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N477/N556	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N464/N556	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N463/N556	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N541/N549	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N542/N550	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N543/N551	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N544/N552	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N545/N553	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N546/N554	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N547/N555	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N548/N556	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N560/N566	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N566/N562	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N557/N565	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N565/N558	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N558/N564	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N564/N559	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N559/N563	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N563/N560	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N566/N561	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N571/N567	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N567/N568	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N568/N569	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N569/N570	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N571/N575	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N575/N567	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N567/N574	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N574/N568	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N568/N573	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N573/N569	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N569/N576	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N576/N572	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N576/N570	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N562/N577	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N577/N578	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N578/N579	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N579/N580	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N580/N581	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N581/N582	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N582/N583	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N583/N584	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N585/N584	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N586/N585	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N587/N586	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N588/N587	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N589/N588	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N590/N589	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N591/N590	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N572/N591	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N593/N592	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N594/N593	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N595/N594	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N596/N595	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N570/N596	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N587/N592	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N588/N592	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N588/N593	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N589/N593	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N589/N594	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N590/N594	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N590/N595	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N591/N595	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N591/N596	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N576/N596	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N599/N602	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N602/N603	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N597/N604	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N604/N598	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N598/N605	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N605/N599	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N602/N600	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N610/N606	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N606/N607	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N607/N608	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N608/N609	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N614/N606	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N606/N613	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N613/N607	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N607/N612	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N612/N608	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N608/N615	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N615/N611	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N615/N609	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N603/N616	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N616/N617	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N617/N618	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N618/N619	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N619/N620	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N620/N621	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N621/N622	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N622/N623	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N624/N623	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N625/N624	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N626/N625	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N627/N626	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N628/N627	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N629/N628	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N630/N629	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N611/N630	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N632/N631	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N633/N632	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N634/N633	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N635/N634	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N609/N635	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N626/N631	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N627/N631	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N627/N632	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N628/N632	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N628/N633	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N629/N633	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N629/N634	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N630/N634	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N630/N635	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N615/N635	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N610/N614	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N636/N597	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N601/N636	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N636/N565	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N597/N558	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N604/N564	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N598/N559	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N605/N563	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N599/N560	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N603/N562	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N600/N561	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N602/N566	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N616/N577	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N617/N578	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N618/N579	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N619/N580	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N620/N581	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N621/N582	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N622/N583	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N623/N584	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N624/N585	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N625/N586	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N626/N587	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N631/N592	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N627/N588	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N632/N593	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N628/N589	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N633/N594	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N629/N590	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N634/N595	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N630/N591	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N635/N596	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N611/N572	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N615/N576	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N609/N570	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N608/N569	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N612/N573	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N607/N568	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N613/N574	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N606/N567	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N614/N575	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N631/N637	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N592/N638	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N626/N637	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N625/N637	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N587/N638	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N586/N638	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N637/N639	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N639/N640	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N638/N641	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N641/N642	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N637/N638	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N639/N641	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N640/N642	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N625/N639	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N624/N639	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N624/N640	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N623/N640	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N586/N641	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N585/N641	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N585/N642	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N584/N642	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N623/N643	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N622/N643	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N640/N643	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N644/N643	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N645/N644	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N646/N645	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N647/N646	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N648/N647	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N649/N648	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N650/N649	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N600/N650	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N622/N644	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N621/N644	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N621/N645	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N620/N645	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N620/N646	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N619/N646	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N619/N647	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N618/N647	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N618/N648	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N617/N648	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N617/N649	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N616/N649	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N616/N650	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N602/N650	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N584/N651	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N583/N651	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N583/N652	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N642/N651	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N652/N651	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N582/N652	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N653/N652	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N582/N653	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N581/N653	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N581/N654	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N654/N653	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N580/N654	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N655/N654	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N580/N655	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N579/N655	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N579/N656	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N656/N655	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N578/N656	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N657/N656	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N578/N657	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N577/N657	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N658/N657	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N577/N658	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N566/N658	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N561/N658	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N643/N651	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N644/N652	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N645/N653	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N646/N654	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N647/N655	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N648/N656	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N649/N657	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N650/N658	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N570/N666	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N666/N665	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N665/N664	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N664/N663	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N663/N662	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N662/N661	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N661/N660	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N660/N659	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N659/N508	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N569/N667	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N667/N668	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N668/N669	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N669/N670	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N670/N671	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N671/N672	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N672/N673	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N673/N674	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N674/N507	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N507/N659	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N674/N659	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N674/N660	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N673/N660	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N673/N661	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N672/N661	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N672/N662	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N671/N662	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N671/N663	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N670/N663	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N670/N664	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N669/N664	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N669/N665	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N668/N665	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N668/N666	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N667/N666	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N667/N570	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N561/N675	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N675/N676	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N676/N677	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N677/N678	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N678/N679	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N679/N680	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N680/N681	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N681/N682	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N682/N500	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N560/N690	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N690/N689	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N689/N688	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N688/N687	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N687/N686	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N686/N685	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N685/N684	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N684/N683	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N683/N499	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N690/N561	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N690/N675	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N689/N675	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N689/N676	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N688/N676	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N688/N677	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N687/N677	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N687/N678	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N686/N678	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N686/N679	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N685/N679	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N685/N680	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N684/N680	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N684/N681	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N683/N681	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N683/N682	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N499/N682	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N243/N698	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N698/N697	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N697/N696	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N696/N695	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N695/N694	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N694/N693	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N693/N692	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N692/N691	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N691/N150	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N242/N699	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N699/N700	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N700/N701	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N701/N702	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N702/N703	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N703/N704	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N704/N705	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N705/N706	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N706/N149	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N706/N691	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N706/N692	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N705/N692	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N705/N693	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N704/N693	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N704/N694	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N703/N694	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N703/N695	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N702/N695	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N702/N696	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N701/N696	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N701/N697	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N700/N697	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N700/N698	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N699/N698	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N149/N691	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N699/N243	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N471/N714	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N714/N713	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N713/N712	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N712/N711	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N711/N710	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N710/N709	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N709/N708	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N708/N707	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N707/N378	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N470/N715	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N715/N716	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N716/N717	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N717/N718	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N718/N719	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N719/N720	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N720/N721	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N721/N722	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N722/N377	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N722/N707	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N722/N708	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N721/N708	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N721/N709	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N720/N709	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N720/N710	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N719/N710	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N719/N711	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N718/N711	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N718/N712	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N717/N712	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N717/N713	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N716/N713	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N716/N714	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N715/N714	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N377/N707	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N715/N471	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N463/N723	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N723/N724	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N724/N725	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N725/N726	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N726/N727	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N727/N736	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N736/N737	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N737/N738	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N738/N370	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N462/N735	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N735/N734	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N734/N733	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N733/N732	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N732/N731	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N731/N730	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N730/N729	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N729/N728	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N728/N369	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N735/N723	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N734/N723	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N734/N724	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N733/N724	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N733/N725	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N732/N725	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N732/N726	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N731/N726	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N731/N727	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N730/N727	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N735/N463	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N730/N736	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N729/N736	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N729/N737	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N728/N737	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N728/N738	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N369/N738	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N235/N739	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N739/N740	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N740/N741	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N741/N742	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N742/N743	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N743/N752	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N752/N753	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N753/N754	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N754/N142	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N234/N751	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N751/N750	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N750/N749	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N749/N748	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N748/N747	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N747/N746	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N746/N745	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N745/N744	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N744/N141	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N751/N739	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N750/N739	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N750/N740	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N749/N740	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N749/N741	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N748/N741	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N748/N742	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N747/N742	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N747/N743	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N746/N743	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N751/N235	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N746/N752	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N745/N752	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N745/N753	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N744/N753	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N744/N754	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N141/N754	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N561/N545	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N500/N655	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N655/N541	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N545/N651	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N530/N642	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N593/N538	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N508/N593	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N570/N530	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N341/N302	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N280/N363	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N302/N410	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N363/N310	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N423/N313	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N317/N419	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N333/N317	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N272/N423	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N53/N135	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N135/N82	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N113/N74	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N74/N182	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N195/N85	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N45/N195	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N105/N89	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N89/N191	Peso propio	Uniforme	0.001	-	-	-	Globales	0.000	0.000	-1.000
N138/N77	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N138/N77	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N138/N77	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N138/N77	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N138/N77	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N137/N76	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N137/N76	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N137/N76	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N137/N76	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N137/N76	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N136/N75	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N136/N75	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N136/N75	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N136/N75	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N136/N75	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N135/N74	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N135/N74	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N135/N74	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N135/N74	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N135/N74	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N134/N73	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N134/N73	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N134/N73	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N134/N73	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N134/N73	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N178/N79	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N178/N79	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N178/N79	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N178/N79	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N178/N79	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N181/N81	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N181/N81	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N181/N81	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N181/N81	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N181/N81	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N182/N82	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N182/N82	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N182/N82	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N182/N82	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N182/N82	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N191/N85	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N191/N85	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N191/N85	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N191/N85	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N191/N85	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N192/N86	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N192/N86	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N192/N86	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N192/N86	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N192/N86	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N193/N87	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N193/N87	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N193/N87	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N193/N87	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N193/N87	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N194/N88	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N194/N88	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N194/N88	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N194/N88	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N194/N88	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N195/N89	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N195/N89	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N195/N89	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N195/N89	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N195/N89	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N196/N90	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N196/N90	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N196/N90	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N196/N90	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N196/N90	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N197/N91	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N197/N91	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N197/N91	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N197/N91	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N197/N91	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N198/N92	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N198/N92	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N198/N92	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N198/N92	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N198/N92	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N268/N175	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N268/N175	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N268/N175	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N268/N175	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N268/N175	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N267/N174	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N267/N174	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N267/N174	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N267/N174	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N267/N174	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N266/N173	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N266/N173	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N266/N173	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N266/N173	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N266/N173	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N265/N172	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N265/N172	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N265/N172	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N265/N172	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N265/N172	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N264/N171	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N264/N171	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N264/N171	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N264/N171	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N264/N171	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N308/N177	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N308/N177	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N308/N177	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N308/N177	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N308/N177	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N311/N179	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N311/N179	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N311/N179	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N311/N179	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N311/N179	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N312/N180	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N312/N180	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N312/N180	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N312/N180	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N312/N180	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N321/N183	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N321/N183	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N321/N183	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N321/N183	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N321/N183	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N322/N184	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N322/N184	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N322/N184	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N322/N184	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N322/N184	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N323/N185	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N323/N185	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N323/N185	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N323/N185	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N323/N185	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N324/N186	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N324/N186	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N324/N186	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N324/N186	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N324/N186	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N325/N187	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N325/N187	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N325/N187	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N325/N187	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N325/N187	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N326/N188	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N326/N188	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N326/N188	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N326/N188	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N326/N188	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N327/N189	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N327/N189	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N327/N189	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N327/N189	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N327/N189	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N328/N190	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N328/N190	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N328/N190	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N328/N190	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N328/N190	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N366/N305	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N366/N305	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N366/N305	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N366/N305	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N366/N305	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N365/N304	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N365/N304	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N365/N304	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N365/N304	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N365/N304	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N364/N303	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N364/N303	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N364/N303	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N364/N303	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N364/N303	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N363/N302	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N363/N302	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N363/N302	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N363/N302	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N363/N302	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N362/N301	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N362/N301	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N362/N301	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N362/N301	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N362/N301	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N406/N307	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N406/N307	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N406/N307	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N406/N307	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N406/N307	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N409/N309	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N409/N309	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N409/N309	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N409/N309	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N409/N309	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N410/N310	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N410/N310	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N410/N310	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N410/N310	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N410/N310	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N419/N313	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N419/N313	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N419/N313	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N419/N313	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N419/N313	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N420/N314	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N420/N314	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N420/N314	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N420/N314	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N420/N314	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N421/N315	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N421/N315	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N421/N315	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N421/N315	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N421/N315	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N422/N316	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N422/N316	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N422/N316	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N422/N316	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N422/N316	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N423/N317	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N423/N317	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N423/N317	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N423/N317	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N423/N317	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N424/N318	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N424/N318	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N424/N318	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N424/N318	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N424/N318	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N425/N319	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N425/N319	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N425/N319	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N425/N319	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N425/N319	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N426/N320	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N426/N320	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N426/N320	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N426/N320	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N426/N320	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N496/N403	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N496/N403	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N496/N403	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N496/N403	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N496/N403	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N495/N402	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N495/N402	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N495/N402	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N495/N402	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N495/N402	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N494/N401	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N494/N401	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N494/N401	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N494/N401	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N494/N401	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N493/N400	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N493/N400	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N493/N400	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N493/N400	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N493/N400	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N492/N399	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N492/N399	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N492/N399	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N492/N399	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N492/N399	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N536/N405	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N536/N405	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N536/N405	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N536/N405	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N536/N405	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N539/N407	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N539/N407	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N539/N407	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N539/N407	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N539/N407	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N540/N408	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N540/N408	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N540/N408	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N540/N408	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N540/N408	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N549/N411	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N549/N411	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N549/N411	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N549/N411	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N549/N411	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N550/N412	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N550/N412	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N550/N412	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N550/N412	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N550/N412	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N551/N413	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N551/N413	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N551/N413	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N551/N413	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N551/N413	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N552/N414	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N552/N414	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N552/N414	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N552/N414	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N552/N414	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N553/N415	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N553/N415	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N553/N415	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N553/N415	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N553/N415	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N554/N416	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N554/N416	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N554/N416	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N554/N416	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N554/N416	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N555/N417	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N555/N417	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N555/N417	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N555/N417	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N555/N417	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N556/N418	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N556/N418	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N556/N418	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N556/N418	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N556/N418	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N596/N533	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N596/N533	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N596/N533	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N596/N533	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N596/N533	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N595/N532	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N595/N532	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N595/N532	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N595/N532	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N595/N532	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N594/N531	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N594/N531	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N594/N531	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N594/N531	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N594/N531	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N593/N530	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N593/N530	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N593/N530	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N593/N530	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N593/N530	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N592/N529	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N592/N529	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N592/N529	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N592/N529	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N592/N529	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N638/N535	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N638/N535	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N638/N535	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N638/N535	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N638/N535	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N641/N537	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N641/N537	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N641/N537	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N641/N537	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N641/N537	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N642/N538	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N642/N538	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N642/N538	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N642/N538	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N642/N538	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N651/N541	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N651/N541	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N651/N541	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N651/N541	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N651/N541	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N652/N542	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N652/N542	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N652/N542	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N652/N542	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N652/N542	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N653/N543	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N653/N543	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N653/N543	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N653/N543	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N653/N543	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N654/N544	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N654/N544	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N654/N544	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N654/N544	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N654/N544	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N655/N545	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N655/N545	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N655/N545	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N655/N545	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N655/N545	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N656/N546	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N656/N546	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N656/N546	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N656/N546	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N656/N546	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N657/N547	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N657/N547	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N657/N547	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N657/N547	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N657/N547	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N658/N548	Peso propio	Uniforme	0.014	-	-	-	Globales	0.000	0.000	-1.000
N658/N548	CM 1	Uniforme	0.022	-	-	-	Globales	0.000	0.000	-1.000
N658/N548	Q 1	Uniforme	0.056	-	-	-	Globales	0.000	0.000	-1.000
N658/N548	V 1	Uniforme	0.040	-	-	-	Globales	0.000	0.000	1.000
N658/N548	V 2	Uniforme	0.044	-	-	-	Globales	0.000	0.000	-1.000
N3/N755	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N755/N50	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N4/N756	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N756/N26	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N755/N756	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N758/N757	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N759/N760	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N761/N762	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N763/N764	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N765/N766	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N767/N768	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N769/N770	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N771/N772	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N773/N774	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N775/N776	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N777/N778	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N779/N780	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N147/N154	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N154/N148	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N154/N117	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N148/N111	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N140/N103	Peso propio	Uniforme	0.004	-	-	-	Globales	0.000	0.000	-1.000
N146/N107	Peso propio	Uniforme	0.003	-	-	-	Globales	0.000	0.000	-1.000
N558/N559	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N559/N560	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N560/N561	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N597/N598	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N598/N599	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N599/N600	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N601/N597	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N557/N558	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N563/N562	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N564/N563	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N565/N564	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N605/N603	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N604/N605	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N636/N604	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N12/N6	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N11/N12	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N10/N11	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N25/N23	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N24/N25	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N756/N24	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N573/N572	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N574/N573	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N575/N574	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N612/N611	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N613/N612	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N614/N613	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N474/N473	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N475/N474	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N476/N475	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N511/N510	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N512/N511	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N513/N512	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N344/N343	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000



Listados

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Cargas en barras

Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N345/N344	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N346/N345	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N381/N380	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N382/N381	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N383/N382	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N246/N245	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N247/N246	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N248/N247	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N283/N282	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N284/N283	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N285/N284	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N116/N115	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N117/N116	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N118/N117	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N153/N152	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N154/N153	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N155/N154	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N55/N54	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N56/N55	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N755/N56	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N47/N46	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N48/N47	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N78/N48	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N107/N106	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N108/N107	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N109/N108	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N146/N144	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N145/N146	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N176/N145	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N237/N236	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N238/N237	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N239/N238	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N276/N274	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N275/N276	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N306/N275	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N335/N334	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N336/N335	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N337/N336	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N374/N372	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N373/N374	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N404/N373	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N465/N464	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N466/N465	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N467/N466	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N504/N502	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N503/N504	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N534/N503	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N794/N575	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Cargas en barras										
Barra	Hipótesis	Tipo	Valores		Posición		Dirección			
			P1	P2	L1 (m)	L2 (m)	Ejes	X	Y	Z
N793/N614	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N781/N795	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N782/N796	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N783/N807	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N784/N808	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N785/N809	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N786/N810	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N787/N811	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N788/N812	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N789/N813	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N790/N814	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N791/N815	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N792/N816	Peso propio	Uniforme	0.625	-	-	-	Globales	0.000	0.000	-1.000
N797/N513	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N798/N476	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N799/N383	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N800/N346	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N801/N285	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N802/N248	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N803/N155	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N804/N118	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N805/N755	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N806/N756	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N817/N636	Peso propio	Uniforme	0.008	-	-	-	Globales	0.000	0.000	-1.000
N818/N565	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N819/N534	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N820/N467	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N821/N404	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N822/N337	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N823/N306	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N824/N239	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N825/N176	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N826/N109	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N827/N78	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000
N828/N10	Peso propio	Uniforme	0.006	-	-	-	Globales	0.000	0.000	-1.000

2.2. Resultados

2.2.1. Barras

2.2.1.1. Comprobaciones E.L.U. (Resumido)

Barras	COMPROBACIONES (AISI S100-16 (2018))																Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV		
N1/N7	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.41 m η = 26.5	x: 1.41 m η = 40.2	η = 1.8	x: 0 m η = 2.0	x: 1.41 m η = 17.9	η = 1.6	x: 0 m η = 0.1	x: 0 m η = 2.8	x: 1.41 m η = 18.7	x: 0 m η = 0.1	x: 1.41 m η = 3.5	x: 1.41 m η = 51.4	x: 1.41 m η = 62.4	x: 1.41 m η = 62.5	CUMPLE η = 62.5
N7/N8	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0 m η = 14.1	x: 0 m η = 17.1	η = 0.5	x: 1.4 m η = 1.3	x: 0 m η = 38.0	η = 4.7	x: 1.4 m η = 0.2	x: 1.4 m η = 1.2	x: 0 m η = 38.2	x: 1.4 m η < 0.1	x: 0 m η = 14.8	x: 0 m η = 62.3	x: 0 m η = 57.2	x: 0 m η = 64.3	CUMPLE η = 64.3
N8/N9	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.35 m η = 5.6	x: 0.225 m η = 1.8	η = 1.0	x: 1.35 m η = 11.9	x: 1.35 m η = 49.0	η = 5.7	x: 0 m η = 1.1	x: 1.35 m η = 12.0	x: 1.35 m η = 49.5	x: 1.35 m η = 1.5	x: 1.35 m η = 24.8	x: 1.35 m η = 74.5	x: 1.35 m η = 50.3	x: 1.35 m η = 65.2	CUMPLE η = 74.5
N9/N5	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.79 m η = 10.2	x: 0 m η = 4.6	x: 0.79 m η = 6.3	x: 0 m η = 2.2	x: 0 m η = 49.7	x: 0.79 m η = 9.7	x: 0.79 m η = 0.4	x: 0 m η = 3.5	x: 0 m η = 52.6	x: 0 m η = 0.1	x: 0 m η = 28.5	x: 0 m η = 77.4	x: 0 m η = 57.6	x: 0 m η = 69.6	CUMPLE η = 77.4

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Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N9/N13	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.61 m η = 2.4	x: 0 m η = 3.7	x: 0.153 m η = 2.2	x: 0.61 m η = 29.6	x: 0.61 m η = 8.8	η = 2.5	x: 0 m η = 6.2	x: 0.61 m η = 30.0	x: 0.61 m η = 9.5	x: 0.61 m η = 9.4	x: 0.61 m η = 1.0	x: 0.61 m η = 25.5	x: 0.61 m η = 33.1	x: 0.61 m η = 38.6	CUMPLE η = 38.6
N13/N6	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.463 m η = 4.3	x: 0 m η = 7.3	η = 6.0	x: 0.463 m η = 53.4	x: 0.463 m η = 11.2	η = 1.8	x: 0.463 m η = 18.5	x: 0.463 m η = 53.5	x: 0.463 m η = 13.8	x: 0.463 m η = 32.0	x: 0.463 m η = 1.9	x: 0.463 m η = 40.7	x: 0.463 m η = 58.5	x: 0.463 m η = 70.8	CUMPLE η = 70.8
N1/N10	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.755 m η = 19.5	x: 0 m η = 41.0	x: 0.378 m η = 4.9	x: 0.755 m η = 11.0	x: 0 m η = 19.7	x: 0.378 m η = 1.8	x: 0 m η = 1.2	x: 0.755 m η = 13.1	x: 0 m η = 21.8	x: 0.755 m η = 1.7	x: 0 m η = 4.8	x: 0 m η = 12.6	x: 0.755 m η = 45.5	x: 0.755 m η = 45.6	CUMPLE η = 45.6
N10/N7	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.847 m η = 21.0	x: 0 m η = 16.2	x: 0.424 m η = 0.9	x: 0 m η = 8.7	x: 0 m η = 55.8	x: 0.424 m η = 6.5	x: 0 m η = 0.8	x: 0 m η = 8.7	x: 0 m η = 56.2	x: 0 m η = 0.8	x: 0 m η = 32.0	x: 0 m η = 81.3	x: 0 m η = 24.4	x: 0 m η = 76.0	CUMPLE η = 81.3
N7/N11	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 8.3	x: 0 m η = 18.3	η = 1.7	x: 0.869 m η = 3.0	x: 0 m η = 7.9	η = 0.6	x: 0 m η = 0.4	x: 0.869 m η = 3.7	x: 0 m η = 8.6	x: 0.869 m η = 0.1	x: 0 m η = 0.7	x: 0 m η = 15.9	x: 0 m η = 22.3	x: 0.869 m η = 21.7	CUMPLE η = 22.3
N11/N8	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.983 m η = 11.6	x: 0 m η = 9.6	η = 0.4	x: 0.983 m η = 2.9	x: 0 m η = 28.5	x: 0.738 m η = 2.9	x: 0.983 m η = 0.3	x: 0.983 m η = 2.9	x: 0 m η = 28.7	x: 0.983 m η = 0.1	x: 0 m η = 8.3	x: 0 m η = 43.6	x: 0 m η = 33.5	x: 0 m η = 42.6	CUMPLE η = 43.6
N8/N12	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.685 m η = 5.3	x: 0.685 m η = 11.7	η = 0.5	x: 0 m η = 3.6	x: 0 m η = 2.4	η = 0.1	x: 0 m η = 0.3	x: 0 m η = 3.5	x: 0 m η = 2.6	x: 0 m η = 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 15.4	x: 0 m η = 16.0	CUMPLE η = 16.0
N12/N9	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.557 m η = 6.9	x: 0.557 m η = 7.7	x: 0.186 m η = 4.6	x: 1.114 m η = 7.7	x: 1.114 m η = 25.5	x: 0.186 m η = 2.0	x: 0 m η = 0.5	x: 1.114 m η = 6.7	x: 1.114 m η = 27.5	x: 1.114 m η = 0.6	x: 1.114 m η = 7.6	x: 1.114 m η = 47.2	x: 1.114 m η = 38.2	x: 1.114 m η = 38.9	CUMPLE η = 47.2
N13/N5	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.819 m η = 7.6	x: 0 m η = 24.0	x: 0.614 m η = 1.1	x: 0 m η = 16.1	x: 0 m η = 18.0	x: 0.614 m η = 1.5	x: 0.819 m η = 1.5	x: 0 m η = 16.2	x: 0 m η = 18.4	x: 0 m η = 2.7	x: 0 m η = 3.4	N.P.[1]	x: 0 m η = 41.1	x: 0 m η = 42.7	CUMPLE η = 42.7
N4/N26	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.41 m η = 26.4	x: 1.41 m η = 38.7	η = 1.8	x: 0 m η = 1.9	x: 1.41 m η = 18.1	η = 1.6	x: 0 m η = 0.1	x: 0 m η = 2.7	x: 1.41 m η = 18.9	x: 0 m η = 0.1	x: 1.41 m η = 3.6	x: 1.41 m η = 51.5	x: 1.41 m η = 60.8	x: 1.41 m η = 61.2	CUMPLE η = 61.2
N26/N27	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 14.1	x: 0 m η = 15.9	η = 0.6	x: 0 m η = 1.0	x: 0 m η = 35.6	η = 4.4	x: 1.4 m η = 0.1	x: 1.4 m η = 1.0	x: 0 m η = 35.8	x: 0 m η < 0.1	x: 0 m η = 13.0	x: 0 m η = 59.4	x: 0 m η = 53.4	x: 0 m η = 60.2	CUMPLE η = 60.2
N27/N28	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.35 m η = 6.8	x: 0.225 m η = 2.7	η = 0.9	x: 1.35 m η = 9.7	x: 1.35 m η = 47.4	η = 5.6	x: 0.225 m η = 0.9	x: 1.35 m η = 9.8	x: 1.35 m η = 47.8	x: 1.35 m η = 1.0	x: 1.35 m η = 23.2	x: 1.35 m η = 72.2	x: 1.35 m η = 6.1	x: 1.35 m η = 63.6	CUMPLE η = 72.2
N28/N22	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.79 m η = 11.4	x: 0 m η = 5.4	η = 6.3	x: 0 m η = 1.3	x: 0 m η = 49.6	η = 9.6	x: 0 m η = 0.2	x: 0.79 m η = 3.4	x: 0 m η = 52.4	x: 0.79 m η = 0.1	x: 0 m η = 28.3	x: 0 m η = 76.7	x: 0 m η = 57.4	x: 0 m η = 69.9	CUMPLE η = 76.7
N26/N24	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.217 m η = 9.0	x: 0.217 m η = 18.9	η = 1.6	x: 0.869 m η = 3.3	x: 0 m η = 6.5	η = 0.5	x: 0 m η = 0.4	x: 0.869 m η = 3.9	x: 0 m η = 7.2	x: 0.869 m η = 0.2	x: 0 m η = 0.5	x: 0 m η = 14.5	x: 0.869 m η = 22.5	x: 0.869 m η = 22.8	CUMPLE η = 22.8
N24/N27	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.983 m η = 11.8	x: 0 m η = 10.2	x: 0.738 m η = 0.4	x: 0 m η = 3.1	x: 0 m η = 27.1	x: 0.738 m η = 2.8	x: 0.983 m η = 0.3	x: 0 m η = 3.1	x: 0 m η = 27.3	x: 0 m η = 0.1	x: 0 m η = 7.5	x: 0 m η = 41.6	x: 0 m η = 32.6	x: 0 m η = 41.0	CUMPLE η = 41.6
N27/N25	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.028 m η = 5.7	x: 1.028 m η = 12.0	x: 0.685 m η = 0.5	x: 0 m η = 2.5	x: 0 m η = 2.4	η = 0.1	x: 0 m η = 0.2	x: 0 m η = 2.5	x: 0 m η = 2.6	x: 0 m η = 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 14.7	x: 0 m η = 15.0	CUMPLE η = 15.0
N25/N28	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.557 m η = 7.5	x: 0.557 m η = 7.7	η = 4.4	x: 1.114 m η = 7.0	x: 1.114 m η = 24.8	η = 1.9	x: 0 m η = 0.5	x: 1.114 m η = 6.4	x: 1.114 m η = 26.7	x: 1.114 m η = 0.5	x: 1.114 m η = 7.2	x: 1.114 m η = 46.8	x: 1.114 m η = 36.7	x: 1.114 m η = 38.1	CUMPLE η = 46.8
N28/N29	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.8 m η = 2.7	x: 0.8 m η = 4.1	x: 0.2 m η = 0.8	x: 0.8 m η = 26.2	x: 0.8 m η = 10.8	x: 0.2 m η = 2.1	x: 0 m η = 4.2	x: 0.8 m η = 26.5	x: 0.8 m η = 11.0	x: 0.8 m η = 7.2	x: 0.8 m η = 1.2	x: 0.8 m η = 23.7	x: 0.8 m η = 30.2	x: 0.8 m η = 34.2	CUMPLE η = 34.2
N29/N23	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.273 m η = 4.9	x: 0 m η = 8.4	η = 6.8	x: 0.273 m η = 48.2	x: 0.273 m η = 10.9	η = 1.8	x: 0.273 m η = 28.5	x: 0.273 m η = 48.2	x: 0.273 m η = 13.8	x: 0.273 m η = 31.3	x: 0.273 m η = 1.9	x: 0.273 m η = 36.3	x: 0.273 m η = 53.0	x: 0.273 m η = 65.0	CUMPLE η = 65.0
N29/N22	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.915 m η = 9.9	x: 0 m η = 31.9	x: 0.686 m η = 2.4	x: 0 m η = 15.6	x: 0 m η = 13.5	η = 0.9	x: 0.915 m η = 1.3	x: 0 m η = 14.5	x: 0 m η = 14.6	x: 0 m η = 2.4	x: 0 m η = 2.1	N.P.[1]	x: 0 m η = 48.5	x: 0 m η = 50.0	CUMPLE η = 50.0
N6/N14	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.617 m η = 5.4	x: 0 m η = 11.5	η = 7.1	x: 0 m η = 58.3	x: 0 m η = 6.1	η = 1.0	x: 0 m η = 12.9	x: 0 m η = 59.6	x: 0 m η = 9.2	x: 0 m η = 37.2	x: 0 m η = 0.9	x: 0 m η = 31.2	x: 0 m η = 72.1	x: 0 m η = 81.2	CUMPLE η = 81.2
N14/N15	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.54 m η = 7.1	x: 0.54 m η = 11.7	x: 0.721 m η = 2.8	x: 0 m η = 18.5	x: 0 m η = 5.6	x: 0.721 m η = 0.9	x: 1.081 m η = 2.2	x: 0 m η = 19.5	x: 0 m η = 6.8	x: 0 m η = 3.9	x: 0 m η = 0.5	x: 0 m η = 13.0	x: 0 m η = 29.0	x: 0 m η = 31.2	CUMPLE η = 31.2
N15/N16	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.363 m η = 7.8	x: 0.363 m η = 8.8	x: 0.544 m η = 2.3	x: 0 m η = 4.6	x: 1.088 m η = 3.4	η = 0.5	x: 0 m η = 0.6	x: 0 m η = 5.3	x: 1.088 m η = 4.2	x: 0 m η = 0.3	x: 1.088 m η = 0.2	x: 0 m η = 11.2	x: 0 m η = 15.1	x: 0 m η = 14.6	CUMPLE η = 15.1
N16/N17	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.08 m η = 8.3	x: 0 m η = 6.3	η = 1.4	x: 0 m η = 1.0	x: 0 m η = 3.7	η = 0.5	x: 1.08 m η = 0.1	x: 0 m η = 1.6	x: 0 m η = 4.2	x: 0 m η < 0.1	x: 0 m η = 0.2	x: 1.08 m η = 10.9	x: 1.08 m η = 8.0	x: 1.08 m η = 9.5	CUMPLE η = 10.9
N17/N18	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.085 m η = 8.8	x: 1.085 m η = 4.5	η = 1.2	x: 1.085 m η = 1.0	x: 1.085 m η = 4.2	η = 0.6	x: 0 m η = 0.1	x: 1.085 m η = 1.5	x: 1.085 m η = 4.4	x: 1.085 m η < 0.1	x: 1.085 m η = 0.2	x: 1.085 m η = 14.2	x: 0 m η = 5.6	x: 1.085 m η = 11.9	CUMPLE η = 14.2
N18/N19	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.082 m η = 10.9	x: 0.18 m η = 2.9	η = 0.8	x: 0.721 m η = 1.1	x: 1.082 m η = 3.4	η = 0.3	x: 0 m η = 0.1	x: 0.721 m η = 1.5	x: 1.082 m η = 3.7	x: 0.721 m η < 0.1	x: 1.082 m η = 0.1	x: 1.082 m η = 15.9	x: 0 m η = 3.8	x: 1.082 m η = 14.0	CUMPLE η = 15.9
N19/N20	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.085 m η = 12.4	x: 0 m η = 1.0	η = 0.8	x: 0.723 m η = 1.1	x: 0 m η = 2.5	η = 0.4	x: 0 m η = 0.1	x: 0.723 m η = 1.4	x: 0 m η = 2.9	x: 0.723 m η < 0.1	x: 0 m η = 0.1	x: 1.085 m η = 16.5	x: 0 m η = 3.2	x: 1.085 m η = 15.0	CUMPLE η = 16.5
N20/N21	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.081 m η = 13.4	N.P.[2]	η = 0.3	x: 0.72 m η = 1.3	x: 1.081 m η = 2.1	η = 0.2	x: 0 m η = 0.1	x: 0.72 m η = 1.4	x: 1.081 m η = 2.1	x: 0.72 m η < 0.1	x: 1.081 m η < 0.1	x: 1.081 m η = 16.8	N.P.[3]	x: 1.081 m η = 15.6	CUMPLE η = 16.8
N30/N21	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.08 m η = 13.6	N.P.[2]	x: 0 m η = 0.4	x: 0.72 m η = 1.3	x: 1.08 m η = 2.2	x: 0 m η = 0.2	x: 0 m η = 0.1	x: 0.72 m η = 1.3	x: 1.08 m η = 2.3	x: 0.54 m η < 0.1	x: 1.08 m η = 0.1	x: 1.08 m η = 16.6	N.P.[3]	x: 1.08 m η = 15.7	CUMPLE η = 16.6
N31/N30	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.084 m η = 12.8	N.P.[2]	η = 0.6	x: 0.722 m η = 1.2	x: 0 m η = 3.3	x: 0 m η = 0.4	x: 0 m η = 0.1	x: 0.722 m η = 1.4	x: 0 m η = 3.5	x: 0.722 m η < 0.1	x: 0 m η = 0.1	x: 1.084 m η = 16.8	N.P.[3]	x: 1.084 m η = 15.4	CUMPLE η = 16.8
N32/N31	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.08 m η = 11.2	x: 1.08 m η = 0.4	η = 0.8	x: 0.72 m η = 1.2	x: 1.08 m η = 5.2	x: 0.18 m η = 0.6	x: 0 m η = 0.1	x: 0.72 m η = 1.5	x: 1.08 m η = 5.5	x: 0.72 m η < 0.1	x: 1.08 m η = 0.3	x: 1.08 m η = 16.2	x: 1.08 m η = 4.3	x: 1.08 m η = 14.3	CUMPLE η = 16.2
N34/N32	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.083 m η = 8.7	x: 1.083 m η = 3.1	η = 1.1	x: 1.083 m η = 1.1	x: 1.083 m η = 3.9	η = 0.7	x: 0 m η = 0.1	x: 1.083 m η = 1.6	x: 1.083 m η = 4.2	x: 1.083 m η < 0.1	x: 1.083 m η = 0.2	x: 1.083 m η = 14.6	x: 0 m η = 5.4	x: 1.083 m η = 12.2	CUMPLE η = 14.6
N36/N34	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.087 m η = 8.1	x: 0 m η = 6.0	η = 1.5	x: 0.543 m η = 0.8	x: 0 m η = 3.4	x: 0.724 m η = 0.5	x: 0 m η = 0.1	x: 0.543 m η = 1.4	x: 0 m η = 4.0	x: 0.543 m η < 0.1	x: 0 m η = 0.2	x: 1.087 m η = 11.3	x: 0 m η = 8.3	x: 0.543 m η = 9.3	CUMPLE η = 11.3
N40/N36	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.542 m η = 8.0	x: 0.542 m η = 8.9	x: 1.085 m η = 2.2	x: 0 m η = 3.6	x: 1.085 m η = 3.5	η = 0.5	x: 0 m η = 0.4	x: 0 m η = 3.9	x: 1.085 m η = 4.3	x: 0 m η = 0.2	x: 1.085 m η = 0.2	x: 0 m η = 10.8	x: 0 m η = 14.2	x: 0 m η = 13.7	CUMPLE η = 14.2
N41/N40	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.539 m η = 7.5	x: 0.539 m η = 12.1	x: 0.718 m η = 2.4	x: 0 m η = 11.9	x: 0 m η = 4.3	η = 0.7	x: 1.077 m η = 1.4	x: 0 m η = 12.9	x: 0 m η = 5.4	x: 0 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 12.4	x: 0 m η = 23.7	x: 0 m η = 25.0	CUMPLE η = 25.0
N23/N41	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.801 m η = 6.3	x: 0 m η = 13.4	x: 0.801 m η = 5.3	x: 0 m η = 44.2	x: 0 m η = 6.0	x: 0.801 m η = 0.8	x: 0 m η = 7.2	x: 0 m η = 45.4	x: 0 m η = 8.3	x: 0 m η = 21.1	x: 0 m η = 0.7	x: 0 m η = 22.8	x: 0 m η = 59.8	x: 0 m η = 64.9	CUMPLE η = 64.9
N35/N33	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.128 m η = 4.5	x: 1.128 m η = 11.0	η = 1.2	x: 1.128 m η = 1.0	x: 0 m η = 8.7	η = 1.2	x: 0 m η = 0.1	x: 1.128 m η = 1.5	x: 0 m η = 8.8	x: 1.128 m η < 0.1	x: 0 m η = 0.8	x: 0 m η = 3.8	x: 0 m η = 13.3	x: 0 m η = 14.8	CUMPLE η = 14.8
N37/N35	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.126 m η = 7.0	x: 0 m η = 10.8	η = 1.8	x: 0 m η = 0.9	x: 1.126 m η = 6.6	η = 0.9	x: 0 m η = 0.1	x: 0.939 m η = 1.2	x: 1.126 m η = 7.1	x: 0.939 m η < 0.1	x: 1.126 m η = 0.5	x: 0 m η = 10.9	x: 0 m η = 14.0	x: 0 m η = 13.7	CUMPLE η = 14.0

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2018))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N38/N37	$w/t \le (w/t)_{Máx}$ Cumple	x: 1.126 m η = 8.8	x: 0 m η = 9.4	η = 1.9	x: 0 m η = 1.3	x: 0 m η = 2.3	x: 0.375 m η = 0.3	x: 0 m η = 0.2	x: 0 m η = 1.6	x: 0 m η = 3.1	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 12.6	x: 0 m η = 12.8	x: 0 m η = 11.9	CUMPLE η = 12.8
N39/N38	$w/t \le (w/t)_{Máx}$ Cumple	x: 1.12 m η = 11.7	x: 0 m η = 8.1	η = 1.9	x: 0 m η = 2.9	x: 1.12 m η = 3.7	x: 0.187 m η = 0.5	x: 0 m η = 0.3	x: 0 m η = 3.7	x: 1.12 m η = 4.0	x: 0 m η = 0.1	x: 1.12 m η = 0.2	x: 0 m η = 16.8	x: 0 m η = 10.9	x: 0 m η = 15.5	CUMPLE η = 16.8
N22/N39	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.594 m η = 11.5	x: 0.594 m η = 5.7	x: 0.989 m η = 4.0	x: 1.187 m η = 4.0	x: 0 m η = 10.5	x: 0.989 m η = 1.2	x: 1.187 m η = 0.6	x: 1.187 m η = 4.5	x: 0 m η = 12.3	x: 1.187 m η = 0.2	x: 0 m η = 1.5	x: 0 m η = 22.1	x: 0 m η = 7.9	x: 0 m η = 17.7	CUMPLE η = 22.1
N32/N33	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.934 m η = 5.6	x: 0 m η = 1.6	x: 0.467 m η = 0.2	x: 0 m η = 1.0	x: 0 m η = 1.3	η = 0.1	x: 0 m η = 0.1	x: 0 m η = 1.1	x: 0 m η = 0.8	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0.934 m η = 2.5	x: 0 m η = 7.4	CUMPLE η = 7.4
N34/N33	$w/t \le (w/t)_{Máx}$ Cumple	x: 1.006 m η = 2.0	x: 0 m η = 8.0	x: 0.335 m η = 0.3	x: 0 m η = 0.9	x: 1.006 m η = 2.0	η = 0.1	x: 1.006 m η = 0.1	x: 0 m η = 1.0	x: 1.006 m η = 2.1	x: 0 m η < 0.1	x: 1.006 m η < 0.1	N.P.(1)	x: 1.006 m η = 10.6	x: 1.006 m η = 10.5	CUMPLE η = 10.6
N34/N35	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.94 m η = 6.9	x: 0 m η = 0.4	x: 0.705 m η = 0.6	x: 0 m η = 1.1	x: 0.94 m η = 4.7	x: 0.705 m η = 0.5	x: 0 m η = 0.1	x: 0 m η = 1.1	x: 0.94 m η = 5.0	x: 0 m η < 0.1	x: 0.94 m η = 0.3	N.P.(1)	x: 0 m η = 1.1	x: 0.94 m η = 10.0	CUMPLE η = 10.0
N36/N35	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.169 m η = 1.5	x: 0 m η = 10.2	x: 0.845 m η = 0.2	x: 0 m η = 1.4	x: 0 m η = 3.2	x: 0.676 m η = 0.3	x: 1.014 m η = 0.1	x: 0 m η = 1.5	x: 0 m η = 3.3	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.(1)	x: 1.014 m η = 13.6	x: 1.014 m η = 13.3	CUMPLE η = 13.6
N36/N37	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.935 m η = 7.4	N.P.(2)	x: 0.701 m η = 0.7	x: 0 m η = 1.8	x: 0 m η = 2.4	x: 0.234 m η = 0.2	x: 0 m η = 0.2	x: 0 m η = 1.7	x: 0 m η = 2.8	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.(3)	N.P.(3)	x: 0 m η = 10.6	CUMPLE η = 10.6
N40/N37	$w/t \le (w/t)_{Máx}$ Cumple	N.P.(4)	x: 0 m η = 11.8	η = 0.3	x: 0 m η = 1.4	x: 1.015 m η = 4.6	x: 0.338 m η = 0.3	x: 0 m η = 0.1	x: 0 m η = 1.4	x: 1.015 m η = 4.7	x: 0 m η < 0.1	x: 1.015 m η = 0.2	N.P.(1)	x: 1.015 m η = 14.7	x: 1.015 m η = 15.1	CUMPLE η = 15.1
N40/N38	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.932 m η = 9.3	N.P.(2)	η = 0.2	x: 0 m η = 0.8	x: 0 m η = 4.8	x: 0 m η = 0.5	x: 0.932 m η = 0.1	x: 0 m η = 0.8	x: 0 m η = 4.9	x: 0 m η < 0.1	x: 0 m η = 0.2	N.P.(1)	N.P.(3)	x: 0 m η = 11.9	CUMPLE η = 11.9
N41/N38	$w/t \le (w/t)_{Máx}$ Cumple	N.P.(4)	x: 0 m η = 15.8	η = 0.5	x: 0 m η = 9.4	x: 1.017 m η = 4.7	x: 0.508 m η = 0.3	x: 1.017 m η = 0.7	x: 0 m η = 7.9	x: 1.017 m η = 4.9	x: 0 m η = 0.9	x: 1.017 m η = 0.2	N.P.(1)	x: 0 m η = 26.3	x: 0 m η = 27.6	CUMPLE η = 27.6
N41/N39	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.932 m η = 4.3	x: 0 m η = 2.9	η = 0.3	x: 0 m η = 11.1	x: 0 m η = 1.9	η = 0.1	x: 0 m η = 0.9	x: 0 m η = 11.2	x: 0 m η = 2.1	x: 0 m η = 1.3	x: 0 m η < 0.1	x: 0 m η = 19.6	x: 0 m η = 11.9	x: 0 m η = 17.1	CUMPLE η = 19.6
N29/N39	$w/t \le (w/t)_{Máx}$ Cumple	N.P.(4)	x: 0 m η = 8.8	η = 2.8	x: 0 m η = 16.9	x: 1.02 m η = 3.7	x: 0.51 m η = 0.4	x: 0 m η = 1.2	x: 0 m η = 17.0	x: 1.02 m η = 4.9	x: 0 m η = 2.9	x: 1.02 m η = 0.2	N.P.(1)	x: 0 m η = 26.2	x: 0 m η = 29.9	CUMPLE η = 29.9
N2/N42	$w/t \le (w/t)_{Máx}$ Cumple	x: 1.41 m η = 22.1	x: 1.41 m η = 35.2	x: 1.41 m η = 1.8	x: 0 m η = 1.8	x: 1.41 m η = 18.1	x: 1.41 m η = 1.6	x: 0 m η = 0.1	x: 0 m η = 2.6	x: 1.41 m η = 18.9	x: 0 m η = 0.1	x: 1.41 m η = 3.6	x: 1.41 m η = 47.6	x: 1.41 m η = 57.1	x: 1.41 m η = 57.5	CUMPLE η = 57.5
N42/N43	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.467 m η = 12.0	x: 0.467 m η = 15.3	x: 0.467 m η = 0.5	x: 1.4 m η = 1.5	x: 0 m η = 37.8	x: 0.467 m η = 4.7	x: 1.4 m η = 0.2	x: 1.4 m η = 1.2	x: 0 m η = 38.0	x: 1.4 m η < 0.1	x: 0 m η = 14.7	x: 0 m η = 60.6	x: 0 m η = 55.0	x: 0 m η = 62.2	CUMPLE η = 62.2
N43/N44	$w/t \le (w/t)_{Máx}$ Cumple	x: 1.35 m η = 4.9	x: 0 m η = 3.0	x: 0.225 m η = 1.2	x: 1.35 m η = 13.2	x: 1.35 m η = 53.3	x: 0.225 m η = 6.2	x: 0 m η = 1.2	x: 1.35 m η = 13.3	x: 1.35 m η = 53.8	x: 1.35 m η = 1.8	x: 1.35 m η = 29.3	x: 1.35 m η = 75.3	x: 1.35 m η = 61.6	x: 1.35 m η = 70.2	CUMPLE η = 75.3
N44/N45	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.79 m η = 10.1	x: 0 m η = 4.9	x: 0.395 m η = 5.9	x: 0 m η = 1.9	x: 0 m η = 44.5	x: 0.395 m η = 8.9	x: 0 m η = 0.4	x: 0 m η = 3.2	x: 0 m η = 47.0	x: 0 m η = 0.1	x: 0 m η = 22.9	x: 0 m η = 67.5	x: 0 m η = 20.8	x: 0 m η = 60.3	CUMPLE η = 67.5
N44/N49	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.61 m η = 1.6	x: 0 m η = 3.4	x: 0 m η = 0.9	x: 0.61 m η = 33.7	x: 0.61 m η = 9.4	η = 2.7	x: 0 m η = 7.2	x: 0.61 m η = 34.1	x: 0.61 m η = 9.5	x: 0.61 m η = 12.1	x: 0.61 m η = 1.0	x: 0.61 m η = 38.6	x: 0.61 m η = 38.7	x: 0.61 m η = 44.9	CUMPLE η = 44.9
N49/N46	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.463 m η = 3.5	x: 0 m η = 7.0	η = 6.7	x: 0.463 m η = 60.4	x: 0.463 m η = 11.1	x: 0.231 m η = 1.6	x: 0.463 m η = 21.0	x: 0.463 m η = 60.5	x: 0.463 m η = 14.0	x: 0.463 m η = 41.0	x: 0.463 m η = 2.0	x: 0.463 m η = 67.0	x: 0.463 m η = 66.5	x: 0.463 m η = 80.6	CUMPLE η = 80.6
N42/N48	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.869 m η = 8.5	x: 0 m η = 18.3	x: 0.652 m η = 1.7	x: 0.869 m η = 2.8	x: 0 m η = 8.0	x: 0.652 m η = 0.6	x: 0 m η = 0.3	x: 0.869 m η = 3.1	x: 0 m η = 8.7	x: 0.869 m η = 0.1	x: 0 m η = 0.8	N.P.(1)	x: 0.869 m η = 21.6	x: 0.869 m η = 21.8	CUMPLE η = 21.8
N48/N43	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.983 m η = 11.8	x: 0 m η = 10.0	η = 0.5	x: 0.983 m η = 2.9	x: 0 m η = 28.2	η = 2.8	x: 0.983 m η = 0.3	x: 0.983 m η = 2.9	x: 0 m η = 28.4	x: 0.983 m η = 0.1	x: 0 m η = 8.2	x: 0 m η = 41.5	x: 0 m η = 13.0	x: 0 m η = 39.8	CUMPLE η = 41.5
N43/N47	$w/t \le (w/t)_{Máx}$ Cumple	x: 1.028 m η = 5.3	x: 0 m η = 11.9	x: 0.514 m η = 0.6	x: 0 m η = 4.0	x: 0 m η = 2.0	η = 0.1	x: 0 m η = 0.4	x: 0 m η = 3.6	x: 0 m η = 2.2	x: 0 m η = 0.2	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 15.9	x: 0 m η = 16.4	CUMPLE η = 16.4
N47/N44	$w/t \le (w/t)_{Máx}$ Cumple	x: 1.114 m η = 6.6	x: 0 m η = 6.5	x: 0.557 m η = 4.9	x: 1.114 m η = 8.5	x: 1.114 m η = 28.4	η = 2.1	x: 0 m η = 0.6	x: 1.114 m η = 7.6	x: 1.114 m η = 30.5	x: 1.114 m η = 0.7	x: 1.114 m η = 9.3	x: 1.114 m η = 48.1	x: 1.114 m η = 42.3	x: 1.114 m η = 41.7	CUMPLE η = 48.1
N49/N45	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.819 m η = 7.9	x: 0 m η = 23.7	η = 1.1	x: 0 m η = 17.5	x: 0 m η = 17.3	x: 0.614 m η = 1.5	x: 0.819 m η = 1.6	x: 0 m η = 17.6	x: 0 m η = 17.7	x: 0 m η = 3.1	x: 0 m η = 3.1	x: 0 m η = 23.8	x: 0 m η = 43.3	x: 0 m η = 42.7	CUMPLE η = 43.3
N3/N50	$w/t \le (w/t)_{Máx}$ Cumple	x: 1.41 m η = 21.3	x: 1.41 m η = 32.9	x: 1.41 m η = 1.8	x: 0 m η = 1.7	x: 1.41 m η = 18.3	x: 1.41 m η = 1.6	x: 0 m η = 0.1	x: 0 m η = 2.5	x: 1.41 m η = 19.1	x: 0 m η = 0.1	x: 1.41 m η = 3.7	x: 1.41 m η = 47.2	x: 1.41 m η = 54.6	x: 1.41 m η = 55.3	CUMPLE η = 55.3
N50/N51	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.7 m η = 12.4	x: 0.7 m η = 14.5	x: 0.7 m η = 0.6	x: 0 m η = 1.1	x: 0 m η = 35.3	x: 0.7 m η = 4.3	x: 1.4 m η = 0.2	x: 0 m η = 1.1	x: 0 m η = 35.6	x: 0 m η < 0.1	x: 0 m η = 12.9	x: 0 m η = 58.2	x: 0 m η = 50.3	x: 0 m η = 58.3	CUMPLE η = 58.3
N51/N52	$w/t \le (w/t)_{Máx}$ Cumple	x: 1.35 m η = 6.2	x: 0.225 m η = 3.4	x: 0.225 m η = 1.1	x: 1.35 m η = 10.9	x: 1.35 m η = 51.6	x: 0.225 m η = 6.0	x: 0 m η = 1.0	x: 1.35 m η = 11.0	x: 1.35 m η = 52.1	x: 1.35 m η = 1.2	x: 1.35 m η = 27.5	x: 1.35 m η = 74.7	x: 1.35 m η = 24.3	x: 1.35 m η = 67.5	CUMPLE η = 74.7
N52/N53	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.79 m η = 11.0	x: 0 m η = 5.2	x: 0.197 m η = 5.7	x: 0 m η = 1.4	x: 0 m η = 44.0	x: 0.197 m η = 8.8	x: 0 m η = 0.3	x: 0 m η = 2.9	x: 0 m η = 46.5	x: 0 m η = 0.1	x: 0 m η = 22.4	x: 0 m η = 66.0	x: 0 m η = 8.2	x: 0 m η = 59.4	CUMPLE η = 66.0
N50/N56	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.869 m η = 9.0	x: 0 m η = 18.8	x: 0.652 m η = 1.7	x: 0.869 m η = 3.3	x: 0 m η = 6.6	x: 0.652 m η = 0.5	x: 0 m η = 0.3	x: 0.869 m η = 3.3	x: 0 m η = 7.3	x: 0.869 m η = 0.1	x: 0 m η = 0.5	N.P.(1)	x: 0.869 m η = 22.4	x: 0.869 m η = 22.9	CUMPLE η = 22.9
N56/N51	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.983 m η = 12.0	x: 0 m η = 10.5	η = 0.5	x: 0 m η = 3.1	x: 0 m η = 26.8	η = 2.7	x: 0.983 m η = 0.3	x: 0 m η = 3.1	x: 0 m η = 27.1	x: 0 m η = 0.1	x: 0 m η = 7.4	x: 0 m η = 39.4	x: 0 m η = 13.4	x: 0 m η = 37.6	CUMPLE η = 39.4
N51/N55	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.856 m η = 5.8	x: 0.856 m η = 12.5	η = 0.6	x: 0 m η = 2.7	x: 0 m η = 2.0	η = 0.1	x: 0 m η = 0.2	x: 0 m η = 2.6	x: 0 m η = 2.3	x: 0 m η = 0.1	x: 0 m η = 0.1	N.P.(1)	x: 0 m η = 15.2	x: 0 m η = 15.5	CUMPLE η = 15.5
N55/N52	$w/t \le (w/t)_{Máx}$ Cumple	x: 1.114 m η = 7.7	x: 0 m η = 7.1	η = 4.7	x: 1.114 m η = 7.8	x: 1.114 m η = 27.7	η = 2.1	x: 0 m η = 0.6	x: 1.114 m η = 7.1	x: 1.114 m η = 29.7	x: 1.114 m η = 0.6	x: 1.114 m η = 8.9	x: 1.114 m η = 47.0	x: 1.114 m η = 39.9	x: 1.114 m η = 40.8	CUMPLE η = 47.0
N52/N57	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.8 m η = 1.6	x: 0 m η = 3.5	x: 0 m η = 0.8	x: 0.8 m η = 30.4	x: 0.8 m η = 11.3	η = 2.3	x: 0 m η = 4.9	x: 0.8 m η = 30.8	x: 0.8 m η = 11.7	x: 0.8 m η = 9.7	x: 0.8 m η = 1.4	x: 0.8 m η = 37.3	x: 0.8 m η = 36.0	x: 0.8 m η = 41.0	CUMPLE η = 41.0
N57/N54	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.273 m η = 4.1	x: 0 m η = 7.8	η = 7.5	x: 0.273 m η = 55.9	x: 0.273 m η = 10.9	η = 1.6	x: 0.273 m η = 33.1	x: 0.273 m η = 55.9	x: 0.273 m η = 14.2	x: 0.273 m η = 42.2	x: 0.273 m η = 2.0	x: 0.273 m η = 62.1	x: 0.273 m η = 61.5	x: 0.273 m η = 75.4	CUMPLE η = 75.4
N57/N53	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.457 m η = 9.7	x: 0.457 m η = 31.3	η = 2.2	x: 0 m η = 17.5	x: 0 m η = 13.2	η = 1.0	x: 0.915 m η = 1.4	x: 0 m η = 17.6	x: 0 m η = 14.2	x: 0 m η = 3.1	x: 0 m η = 2.0	x: 0 m η = 21.2	x: 0 m η = 48.7	x: 0 m η = 50.3	CUMPLE η = 50.3
N46/N58	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.617 m η = 4.1	x: 0 m η = 11.7	η = 7.0	x: 0 m η = 66.3	x: 0 m η = 6.0	η = 1.0	x: 0 m η = 14.7	x: 0 m η = 67.7	x: 0 m η = 9.1	x: 0 m η = 48.0	x: 0 m η = 0.8	x: 0 m η = 19.1	x: 0 m η = 83.6	x: 0 m η = 94.6	CUMPLE η = 94.6
N58/N59	$w/t \le (w/t)_{Máx}$ Cumple	x: 1.081 m η = 5.7	x: 0 m η = 11.9	x: 0.721 m η = 2.8	x: 0 m η = 20.7	x: 0 m η = 5.6	x: 0.721 m η = 0.9	x: 1.081 m η = 2.4	x: 0 m η = 21.7	x: 0 m η = 6.8	x: 0 m η = 4.8	x: 0 m η = 0.5	x: 0 m η = 11.6	x: 0 m η = 34.6	x: 0 m η = 34.7	CUMPLE η = 34.7
N59/N60	$w/t \le (w/t)_{Máx}$ Cumple	x: 0.544 m η = 6.8	x: 0.544 m η = 9.3	x: 0.907 m η = 2.2	x: 0 m η = 5.0	x: 1.088 m η = 3.4	η = 0.5	x: 0 m η = 0.7	x: 0 m η = 5.8	x: 1.088 m η = 4.2	x: 0 m η = 0.3	x: 1.088 m η = 0.2	x: 0 m η = 9.3	x: 0 m η = 15.6	x: 0 m η = 15.3	CUMPLE η = 15.6

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_z	V_y	M_xTr	M_yTr	M_yV_y	M_yV_z	MT	MP	TPTrMV	
N60/N61	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0 m η = 7.1	x: 0 m η = 7.1	η = 1.4	x: 0.18 m η = 1.1	x: 0 m η = 3.6	η = 0.5	x: 1.08 m η = 0.1	x: 0.18 m η = 1.7	x: 0 m η = 4.0	x: 0.18 m η < 0.1	x: 0 m η = 0.2	x: 0 m η = 10.3	x: 1.08 m η = 8.8	x: 0 m η = 8.5	CUMPLE η = 10.3
N61/N62	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.085 m η = 7.1	x: 1.085 m η = 5.0	η = 1.2	x: 1.085 m η = 1.3	x: 1.085 m η = 4.3	x: 0.723 m η = 0.6	x: 0 m η = 0.2	x: 1.085 m η = 1.8	x: 1.085 m η = 4.5	x: 1.085 m η < 0.1	x: 1.085 m η = 0.2	x: 1.085 m η = 11.3	x: 1.085 m η = 6.2	x: 1.085 m η = 10.1	CUMPLE η = 11.3
N62/N63	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.18 m η = 7.1	x: 0.18 m η = 3.3	η = 0.9	x: 0.902 m η = 1.2	x: 1.082 m η = 3.5	x: 0.361 m η = 0.3	x: 0 m η = 0.1	x: 0.902 m η = 1.6	x: 1.082 m η = 3.9	x: 0.902 m η < 0.1	x: 1.082 m η = 0.2	x: 1.082 m η = 11.5	x: 0 m η = 4.2	x: 1.082 m η = 9.8	CUMPLE η = 11.5
N63/N64	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.085 m η = 7.4	x: 0.904 m η = 1.9	η = 0.9	x: 0.723 m η = 1.2	x: 0 m η = 2.4	x: 6.181 m η = 0.4	x: 0 m η = 0.1	x: 0.723 m η = 1.5	x: 0 m η = 2.8	x: 0.723 m η < 0.1	x: 0 m η = 0.1	x: 1.085 m η = 11.7	x: 0 m η = 4.3	x: 1.085 m η = 10.1	CUMPLE η = 11.7
N64/N65	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.081 m η = 8.3	x: 0 m η = 2.1	η = 0.3	x: 0.901 m η = 1.4	x: 1.081 m η = 2.0	η = 0.2	x: 0 m η = 0.1	x: 0.901 m η = 1.5	x: 1.081 m η = 2.0	x: 0.901 m η < 0.1	x: 1.081 m η < 0.1	x: 1.081 m η = 11.9	x: 1.081 m η = 4.1	x: 1.081 m η = 10.6	CUMPLE η = 11.9
N66/N65	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.08 m η = 8.6	x: 0.36 m η = 1.7	x: 0 m η = 0.4	x: 0.54 m η = 1.4	x: 1.08 m η = 2.2	x: 0 m η = 0.2	x: 0 m η = 0.1	x: 0.54 m η = 1.4	x: 1.08 m η = 2.4	x: 0.54 m η < 0.1	x: 1.08 m η = 0.1	x: 0.9 m η = 11.8	x: 1.08 m η = 4.0	x: 0.9 m η = 10.8	CUMPLE η = 11.8
N67/N66	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.084 m η = 8.1	x: 0 m η = 0.8	x: 0.903 m η = 0.7	x: 0.722 m η = 1.3	x: 0 m η = 3.3	x: 0 m η = 0.4	x: 0 m η = 0.1	x: 0.722 m η = 1.5	x: 0 m η = 3.6	x: 0.722 m η < 0.1	x: 0 m η = 0.1	x: 1.084 m η = 12.2	x: 0 m η = 4.3	x: 1.084 m η = 10.7	CUMPLE η = 12.2
N68/N67	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.08 m η = 6.8	x: 0.18 m η = 0.8	η = 0.8	x: 0.9 m η = 1.3	x: 1.08 m η = 5.2	x: 0.18 m η = 0.6	x: 0 m η = 0.1	x: 0.9 m η = 1.6	x: 1.08 m η = 5.6	x: 0.9 m η < 0.1	x: 1.08 m η = 0.3	x: 1.08 m η = 13.3	x: 1.08 m η = 5.0	x: 1.08 m η = 11.7	CUMPLE η = 13.3
N69/N68	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.083 m η = 5.0	x: 1.083 m η = 2.1	η = 1.1	x: 1.083 m η = 1.3	x: 1.083 m η = 3.9	η = 0.7	x: 0 m η = 0.1	x: 1.083 m η = 1.8	x: 1.083 m η = 4.2	x: 1.083 m η < 0.1	x: 1.083 m η = 0.2	x: 1.083 m η = 11.1	x: 0 m η = 4.8	x: 1.083 m η = 9.6	CUMPLE η = 11.1
N70/N69	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.087 m η = 5.9	x: 0 m η = 5.5	η = 1.5	x: 0 m η = 1.3	x: 0 m η = 3.4	x: 0.724 m η = 0.5	x: 0 m η = 0.1	x: 0.724 m η = 1.6	x: 0 m η = 4.0	x: 0.724 m η < 0.1	x: 0 m η = 0.2	x: 0 m η = 10.4	x: 0 m η = 8.1	x: 0 m η = 8.2	CUMPLE η = 10.4
N71/N70	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.085 m η = 7.3	x: 1.085 m η = 10.0	x: 0.904 m η = 2.2	x: 0 m η = 3.7	x: 1.085 m η = 3.5	η = 0.5	x: 0 m η = 0.5	x: 0 m η = 4.5	x: 1.085 m η = 4.3	x: 0 m η = 0.2	x: 1.085 m η = 0.2	x: 1.085 m η = 10.9	x: 0 m η = 15.0	x: 0 m η = 14.7	CUMPLE η = 15.0
N72/N71	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.718 m η = 6.2	x: 0.718 m η = 12.3	x: 0.718 m η = 2.4	x: 0 m η = 13.6	x: 0 m η = 4.3	η = 0.7	x: 1.077 m η = 1.6	x: 0 m η = 14.6	x: 0 m η = 5.4	x: 0 m η = 2.1	x: 0 m η = 0.3	x: 0 m η = 10.7	x: 0 m η = 26.9	x: 0 m η = 25.6	CUMPLE η = 26.9
N54/N72	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.801 m η = 4.8	x: 0.801 m η = 13.5	x: 0.801 m η = 5.2	x: 0 m η = 51.3	x: 0 m η = 5.9	x: 0.801 m η = 0.8	x: 0 m η = 8.4	x: 0 m η = 52.6	x: 0 m η = 8.2	x: 0 m η = 28.4	x: 0 m η = 0.7	x: 0 m η = 18.5	x: 0 m η = 70.4	x: 0 m η = 77.2	CUMPLE η = 77.2
N74/N73	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.128 m η = 6.8	x: 0 m η = 16.7	η = 1.2	x: 1.128 m η = 1.8	x: 0 m η = 8.7	x: 0.752 m η = 1.2	x: 0 m η = 0.3	x: 1.128 m η = 2.4	x: 0 m η = 8.9	x: 1.128 m η = 0.1	x: 0 m η = 0.8	x: 0 m η = 5.2	x: 1.128 m η = 18.0	x: 0.752 m η = 17.8	CUMPLE η = 18.0
N75/N74	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.939 m η = 11.0	x: 0.939 m η = 18.5	x: 0.751 m η = 2.0	x: 0 m η = 1.8	x: 1.126 m η = 6.5	x: 0.751 m η = 0.9	x: 0 m η = 0.3	x: 1.126 m η = 2.2	x: 1.126 m η = 7.1	x: 1.126 m η < 0.1	x: 1.126 m η = 0.5	x: 0 m η = 15.8	x: 0 m η = 22.5	x: 0 m η = 21.6	CUMPLE η = 22.5
N76/N75	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0 m η = 6.6	x: 0 m η = 9.0	η = 1.9	x: 0 m η = 1.8	x: 0 m η = 2.2	x: 0.375 m η = 0.3	x: 0 m η = 0.3	x: 0 m η = 2.6	x: 0 m η = 3.0	x: 0 m η = 0.1	x: 0 m η = 0.1	x: 0 m η = 10.1	x: 1.126 m η = 12.8	x: 1.126 m η = 11.5	CUMPLE η = 12.8
N77/N76	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.12 m η = 10.4	x: 0 m η = 7.7	η = 1.9	x: 0 m η = 4.2	x: 1.12 m η = 3.7	η = 0.5	x: 0 m η = 0.6	x: 0 m η = 5.1	x: 1.12 m η = 4.0	x: 0 m η = 0.3	x: 1.12 m η = 0.2	x: 0 m η = 15.8	x: 0 m η = 10.1	x: 0 m η = 14.6	CUMPLE η = 15.8
N53/N77	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.187 m η = 11.2	x: 0 m η = 5.4	η = 4.3	x: 1.187 m η = 3.8	x: 0 m η = 10.7	x: 0.989 m η = 1.2	x: 1.187 m η = 0.5	x: 1.187 m η = 3.9	x: 0 m η = 12.5	x: 1.187 m η = 0.2	x: 0 m η = 1.6	x: 0 m η = 28.4	x: 0 m η = 18.4	x: 0 m η = 23.3	CUMPLE η = 28.4
N68/N73	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.467 m η = 6.6	x: 0.467 m η = 3.7	x: 0.234 m η = 0.4	x: 0 m η = 1.3	x: 0 m η = 1.3	x: 0.701 m η = 0.1	x: 0 m η = 0.2	x: 0 m η = 1.3	x: 0.934 m η = 1.4	x: 0 m η < 0.1	x: 0.934 m η < 0.1	N.P.[1]	x: 0.934 m η = 5.2	x: 0 m η = 8.2	CUMPLE η = 8.2
N69/N73	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.168 m η = 3.4	x: 0.168 m η = 12.0	η = 0.2	x: 0 m η = 1.2	x: 1.006 m η = 1.9	η = 0.1	x: 1.006 m η = 0.1	x: 0 m η = 1.3	x: 1.006 m η = 2.0	x: 0 m η < 0.1	x: 1.006 m η < 0.1	N.P.[1]	x: 1.006 m η = 14.6	x: 1.006 m η = 14.4	CUMPLE η = 14.6
N69/N74	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.94 m η = 8.1	x: 0.47 m η = 3.4	η = 0.4	x: 0 m η = 1.7	x: 0.94 m η = 5.4	x: 0.705 m η = 0.5	x: 0 m η = 0.2	x: 0 m η = 1.7	x: 0.94 m η = 5.6	x: 0 m η < 0.1	x: 0.94 m η = 0.3	x: 0.94 m η = 12.9	x: 0.94 m η = 8.8	x: 0.94 m η = 12.2	CUMPLE η = 12.9
N70/N74	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0 m η = 4.0	x: 0 m η = 15.2	η = 0.2	x: 0 m η = 1.9	x: 0 m η = 3.4	x: 0.507 m η = 0.3	x: 1.014 m η = 0.2	x: 0 m η = 2.0	x: 0 m η = 3.4	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 1.014 m η = 19.0	x: 1.014 m η = 18.3	CUMPLE η = 19.0
N70/N75	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.935 m η = 9.2	x: 0.701 m η = 4.0	x: 0.935 m η = 0.6	x: 0 m η = 2.2	x: 0 m η = 2.0	η = 0.2	x: 0 m η = 0.2	x: 0 m η = 2.2	x: 0 m η = 2.2	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 6.4	x: 0 m η = 12.3	CUMPLE η = 12.3
N71/N75	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.015 m η = 0.1	x: 0 m η = 17.8	η = 0.5	x: 0 m η = 1.0	x: 1.015 m η = 3.6	x: 0.338 m η = 0.2	x: 0 m η < 0.1	x: 0 m η = 1.1	x: 1.015 m η = 3.8	x: 0 m η < 0.1	x: 1.015 m η = 0.1	N.P.[1]	x: 1.015 m η = 20.8	x: 1.015 m η = 20.9	CUMPLE η = 20.9
N71/N76	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.932 m η = 12.0	N.P.[2]	η = 0.1	x: 0 m η = 0.9	x: 0 m η = 4.3	x: 0.932 m η = 0.4	x: 0.932 m η = 0.1	x: 0 m η = 0.9	x: 0 m η = 4.3	x: 0 m η < 0.1	x: 0 m η = 0.2	N.P.[3]	N.P.[3]	x: 0 m η = 14.6	CUMPLE η = 14.6
N72/N76	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 23.6	x: 0.678 m η = 0.3	x: 0 m η = 11.1	x: 1.017 m η = 3.5	x: 0.339 m η = 0.3	x: 1.017 m η = 0.9	x: 0 m η = 8.3	x: 1.017 m η = 3.7	x: 0 m η = 1.2	x: 1.017 m η = 0.1	N.P.[3]	x: 0 m η = 36.2	x: 0 m η = 37.5	CUMPLE η = 37.5
N72/N77	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.932 m η = 5.7	x: 0 m η = 2.1	η = 0.3	x: 0 m η = 12.9	x: 0 m η = 1.9	η = 0.1	x: 0 m η = 1.0	x: 0 m η = 13.0	x: 0 m η = 2.1	x: 0 m η = 1.7	x: 0 m η < 0.1	x: 0 m η = 24.5	x: 0 m η = 11.5	x: 0 m η = 21.9	CUMPLE η = 24.5
N57/N77	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 17.5	x: 0.51 m η = 2.6	x: 0 m η = 19.2	x: 1.02 m η = 4.1	η = 0.4	x: 0 m η = 1.4	x: 0 m η = 19.3	x: 1.02 m η = 5.2	x: 0 m η = 3.7	x: 1.02 m η = 0.3	N.P.[1]	x: 0 m η = 39.0	x: 0 m η = 41.6	CUMPLE η = 41.6
N78/N42	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.424 m η = 21.1	x: 0.424 m η = 16.6	x: 0.847 m η = 0.9	x: 0 m η = 8.8	x: 0 m η = 55.9	x: 0.847 m η = 6.5	x: 0 m η = 0.8	x: 0 m η = 8.8	x: 0 m η = 56.2	x: 0 m η = 0.8	x: 0 m η = 32.1	x: 0 m η = 81.5	x: 0 m η = 24.9	x: 0 m η = 78.0	CUMPLE η = 81.5
N2/N78	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.755 m η = 19.8	x: 0 m η = 41.4	x: 0.189 m η = 4.9	x: 0.755 m η = 10.6	x: 0 m η = 19.7	x: 0.189 m η = 1.8	x: 0 m η = 1.1	x: 0.755 m η = 12.7	x: 0 m η = 21.9	x: 0.755 m η = 1.6	x: 0 m η = 4.8	x: 0 m η = 12.2	x: 0.755 m η = 45.5	x: 0.755 m η = 45.5	CUMPLE η = 45.5
N78/N10	w / t ≤ (w / t)$_{Máx.}$ Cumple	η < 0.1	η < 0.1	η = 3.6	x: 0.3 m η = 22.9	x: 0.3 m η = 2.9	η = 1.2	x: 0.3 m η = 50.5	x: 0.3 m η = 24.4	x: 0.3 m η = 4.5	x: 0.3 m η = 80.3	x: 0.3 m η = 0.2	x: 0.3 m η = 60.8	x: 0.3 m η = 28.7	x: 0.3 m η = 36.0	CUMPLE η = 36.0
N42/N7	w / t ≤ (w / t)$_{Máx.}$ Cumple	η < 0.1	η < 0.1	η = 0.5	x: 0.3 m η = 25.8	x: 0.3 m η = 30.2	x: 0.15 m η = 12.4	x: 0.15 m η = 51.8	x: 0.3 m η = 26.0	x: 0.3 m η = 30.4	x: 0.3 m η = 85.5	x: 0.3 m η = 10.8	x: 0.3 m η = 95.5	x: 0.3 m η = 55.1	x: 0.3 m η = 61.2	CUMPLE η = 61.2
N48/N11	w / t ≤ (w / t)$_{Máx.}$ Cumple	η < 0.1	η < 0.1	η = 0.1	x: 0.3 m η = 58.3	x: 0 m η = 3.9	η = 1.7	x: 0.3 m η = 67.4	x: 0.3 m η = 58.4	x: 0 m η = 3.9	x: 0.3 m η = 96.2	x: 0 m η = 0.2	x: 0.3 m η = 20.8	x: 0.3 m η = 60.3	x: 0.3 m η = 91.6	CUMPLE η = 91.6
N43/N8	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 0.2	η = 0.2	η = 0.8	x: 0 m η = 50.6	x: 0.3 m η = 30.5	x: 0.15 m η = 13.0	x: 0.3 m η = 63.8	x: 0 m η = 50.9	x: 0.3 m η = 30.8	x: 0 m η = 68.6	x: 0.3 m η = 11.2	x: 0 m η = 25.6	x: 0 m η = 81.5	x: 0 m η = 69.2	CUMPLE η = 69.2
N47/N12	w / t ≤ (w / t)$_{Máx.}$ Cumple	η < 0.1	η < 0.1	η = 1.3	x: 0 m η = 39.7	x: 0 m η = 14.8	η = 4.9	x: 0.3 m η = 46.8	x: 0 m η = 40.3	x: 0 m η = 15.3	x: 0 m η = 18.7	x: 0 m η = 2.6	x: 0 m η = 90.5	x: 0 m η = 53.4	x: 0 m η = 35.7	CUMPLE η = 35.7
N44/N9	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.15 m η = 10.4	x: 0.15 m η = 11.0	x: 0.15 m η = 1.5	x: 0 m η = 10.4	x: 0.3 m η = 25.8	x: 0 m η = 8.3	x: 0.3 m η = 2.6	x: 0 m η = 11.0	x: 0.3 m η = 26.4	x: 0 m η = 1.3	x: 0.3 m η = 7.7	x: 0 m η = 54.4	x: 0 m η = 39.5	x: 0.3 m η = 43.3	CUMPLE η = 54.4
N46/N6	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.15 m η = 0.1	x: 0.15 m η = 0.1	η = 0.3	x: 0.3 m η = 36.4	x: 0.3 m η = 18.4	η = 6.2	x: 0.3 m η = 12.1	x: 0.3 m η = 36.5	x: 0.3 m η = 18.6	x: 0.3 m η = 14.8	x: 0.3 m η = 3.8	x: 0.3 m η = 48.3	x: 0.3 m η = 46.5	x: 0.3 m η = 45.5	CUMPLE η = 48.3
N45/N5	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.15 m η = 6.2	x: 0.15 m η = 6.8	η = 1.2	x: 0.3 m η = 74.1	x: 0.3 m η = 25.0	x: 0.15 m η = 8.4	x: 0.15 m η = 24.7	x: 0.3 m η = 74.4	x: 0.3 m η = 25.3	x: 0.3 m η = 81.4	x: 0.3 m η = 7.1	x: 0.3 m η = 30.6	x: 0.3 m η = 16.5	x: 0.3 m η = 19.0	CUMPLE η = 30.6

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2018))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N49/N13	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 0.4$	$\eta = 0.4$	x: 0.15 m $\eta = 0.3$	x: 0 m $\eta = 9.9$	x: 0.3 m $\eta = 25.0$	x: 0.15 m $\eta = 8.3$	x: 0.3 m $\eta = 3.3$	x: 0 m $\eta = 10.0$	x: 0.3 m $\eta = 25.1$	x: 0 m $\eta = 1.1$	x: 0.3 m $\eta = 7.0$	x: 0 m $\eta = 36.8$	x: 0.3 m $\eta = 21.6$	x: 0.3 m $\eta = 31.4$	CUMPLE $\eta = 36.8$
N58/N14	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	x: 0.15 m $\eta = 2.4$	x: 0.3 m $\eta = 26.3$	x: 0 m $\eta = 20.1$	$\eta = 6.7$	x: 0.3 m $\eta = 8.8$	x: 0.3 m $\eta = 27.3$	x: 0 m $\eta = 21.1$	x: 0.3 m $\eta = 8.2$	x: 0 m $\eta = 4.9$	x: 0.3 m $\eta = 60.4$	x: 0.3 m $\eta = 30.6$	x: 0.3 m $\eta = 41.2$	CUMPLE $\eta = 60.4$
N59/N15	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 0.2$	$\eta = 0.3$	$\eta = 0.7$	x: 0.3 m $\eta = 16.4$	x: 0 m $\eta = 24.4$	x: 0.15 m $\eta = 8.1$	x: 0.3 m $\eta = 5.4$	x: 0.3 m $\eta = 16.7$	x: 0 m $\eta = 24.7$	x: 0.3 m $\eta = 3.1$	x: 0 m $\eta = 6.7$	x: 0.3 m $\eta = 44.6$	x: 0.3 m $\eta = 41.5$	x: 0.3 m $\eta = 36.8$	CUMPLE $\eta = 44.6$
N60/N16	$w/t \le (w/t)_{Max}$ Cumple	x: 0.15 m $\eta < 0.1$	x: 0.15 m $\eta < 0.1$	$\eta = 0.8$	x: 0.3 m $\eta = 10.3$	x: 0 m $\eta = 22.1$	x: 0.15 m $\eta = 7.4$	x: 0.3 m $\eta = 3.4$	x: 0.3 m $\eta = 10.6$	x: 0 m $\eta = 22.5$	x: 0.3 m $\eta = 1.2$	x: 0 m $\eta = 5.6$	x: 0.3 m $\eta = 39.3$	x: 0 m $\eta = 14.5$	x: 0 m $\eta = 29.3$	CUMPLE $\eta = 39.3$
N61/N17	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 0.6$	x: 0 m $\eta = 8.1$	x: 0 m $\eta = 27.1$	$\eta = 9.1$	x: 0.3 m $\eta = 2.7$	x: 0 m $\eta = 8.3$	x: 0 m $\eta = 27.3$	x: 0 m $\eta = 0.8$	x: 0 m $\eta = 8.3$	x: 0.3 m $\eta = 32.0$	x: 0 m $\eta = 35.6$	x: 0 m $\eta = 35.3$	CUMPLE $\eta = 35.6$
N62/N18	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 0.4$	x: 0 m $\eta = 8.2$	x: 0.3 m $\eta = 18.2$	$\eta = 6.1$	x: 0.3 m $\eta = 2.7$	x: 0 m $\eta = 8.3$	x: 0.3 m $\eta = 18.3$	x: 0 m $\eta = 0.8$	x: 0.3 m $\eta = 3.7$	x: 0.3 m $\eta = 24.7$	x: 0 m $\eta = 26.5$	x: 0.3 m $\eta = 24.8$	CUMPLE $\eta = 26.5$
N63/N19	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 0.3$	$\eta = 0.4$	$\eta = 0.2$	x: 0.3 m $\eta = 4.8$	x: 0.3 m $\eta = 9.1$	$\eta = 3.1$	x: 0.3 m $\eta = 1.6$	x: 0.3 m $\eta = 4.9$	x: 0.3 m $\eta = 9.2$	x: 0.3 m $\eta = 0.3$	x: 0.3 m $\eta = 0.9$	x: 0.3 m $\eta = 17.7$	x: 0.3 m $\eta = 5.8$	x: 0.3 m $\eta = 12.9$	CUMPLE $\eta = 17.7$
N64/N20	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 0.1$	x: 0 m $\eta = 4.1$	x: 0.3 m $\eta = 9.7$	x: 0.3 m $\eta = 3.2$	x: 0.3 m $\eta = 1.3$	x: 0 m $\eta = 4.2$	x: 0.3 m $\eta = 9.7$	x: 0 m $\eta = 0.2$	x: 0.3 m $\eta = 1.0$	x: 0.3 m $\eta = 13.2$	x: 0 m $\eta = 12.5$	x: 0.3 m $\eta = 12.1$	CUMPLE $\eta = 13.2$
N65/N21	$w/t \le (w/t)_{Max}$ Cumple	x: 0.3 m $\eta < 0.1$	x: 0.3 m $\eta = 0.1$	$\eta = 0.1$	x: 0 m $\eta = 5.5$	x: 0 m $\eta = 10.6$	x: 0.3 m $\eta = 3.5$	x: 0.3 m $\eta = 1.7$	x: 0 m $\eta = 5.5$	x: 0 m $\eta = 10.6$	x: 0 m $\eta = 0.3$	x: 0 m $\eta = 1.3$	x: 0 m $\eta = 14.5$	x: 0 m $\eta = 11.9$	x: 0 m $\eta = 13.2$	CUMPLE $\eta = 14.5$
N66/N30	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta = 0.1$	$\eta = 0.2$	x: 0.3 m $\eta = 4.1$	x: 0 m $\eta = 10.1$	x: 0 m $\eta = 3.4$	x: 0.3 m $\eta = 1.4$	x: 0 m $\eta = 3.7$	x: 0 m $\eta = 10.1$	x: 0.3 m $\eta = 0.2$	x: 0 m $\eta = 1.1$	x: 0 m $\eta = 14.1$	x: 0 m $\eta = 13.1$	x: 0 m $\eta = 12.6$	CUMPLE $\eta = 14.1$
N67/N31	$w/t \le (w/t)_{Max}$ Cumple	x: 0 m $\eta = 0.6$	x: 0 m $\eta = 0.7$	x: 0 m $\eta = 0.2$	x: 0.3 m $\eta = 4.9$	x: 0.3 m $\eta = 9.5$	x: 0.3 m $\eta = 3.2$	x: 0.3 m $\eta = 1.6$	x: 0.3 m $\eta = 4.9$	x: 0.3 m $\eta = 9.6$	x: 0.3 m $\eta = 0.3$	x: 0.3 m $\eta = 1.0$	x: 0.3 m $\eta = 16.9$	x: 0.3 m $\eta = 11.9$	x: 0.3 m $\eta = 12.3$	CUMPLE $\eta = 16.9$
N68/N32	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 0.4$	x: 0.3 m $\eta = 6.1$	x: 0 m $\eta = 25.9$	$\eta = 8.7$	x: 0.3 m $\eta = 2.0$	x: 0.3 m $\eta = 6.2$	x: 0 m $\eta = 26.0$	x: 0.3 m $\eta = 0.4$	x: 0 m $\eta = 7.5$	x: 0.3 m $\eta = 40.2$	x: 0.3 m $\eta = 22.4$	x: 0.3 m $\eta = 33.1$	CUMPLE $\eta = 40.2$
N73/N33	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 0.4$	$\eta = 0.4$	$\eta = 0.2$	x: 0 m $\eta = 8.2$	x: 0.3 m $\eta = 23.8$	$\eta = 7.9$	x: 0.3 m $\eta = 2.4$	x: 0 m $\eta = 8.3$	x: 0.3 m $\eta = 23.9$	x: 0 m $\eta = 0.7$	x: 0.3 m $\eta = 6.3$	x: 0 m $\eta = 37.7$	x: 0 m $\eta = 32.2$	x: 0 m $\eta = 31.4$	CUMPLE $\eta = 37.7$
N69/N34	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 0.6$	x: 0.3 m $\eta = 7.7$	x: 0 m $\eta = 28.1$	$\eta = 9.4$	x: 0.3 m $\eta = 2.6$	x: 0.3 m $\eta = 8.0$	x: 0 m $\eta = 28.3$	x: 0.3 m $\eta = 0.7$	x: 0 m $\eta = 8.9$	x: 0.3 m $\eta = 43.3$	x: 0.3 m $\eta = 21.9$	x: 0.3 m $\eta = 35.9$	CUMPLE $\eta = 43.3$
N74/N35	$w/t \le (w/t)_{Max}$ Cumple	x: 0.3 m $\eta = 1.3$	x: 0.3 m $\eta = 1.4$	$\eta = 0.5$	x: 0 m $\eta = 3.9$	x: 0.3 m $\eta = 10.5$	x: 0.15 m $\eta = 3.5$	x: 0.3 m $\eta = 1.3$	x: 0 m $\eta = 4.2$	x: 0.3 m $\eta = 10.7$	x: 0 m $\eta = 0.2$	x: 0.3 m $\eta = 1.3$	x: 0 m $\eta = 16.4$	x: 0.3 m $\eta = 13.7$	x: 0.3 m $\eta = 14.7$	CUMPLE $\eta = 16.4$
N70/N36	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 0.9$	x: 0.3 m $\eta = 10.0$	x: 0 m $\eta = 22.3$	x: 0.3 m $\eta = 7.4$	x: 0.3 m $\eta = 3.4$	x: 0.3 m $\eta = 10.4$	x: 0 m $\eta = 22.6$	x: 0.3 m $\eta = 1.2$	x: 0 m $\eta = 5.7$	x: 0.3 m $\eta = 39.8$	x: 0.3 m $\eta = 15.9$	x: 0.3 m $\eta = 29.9$	CUMPLE $\eta = 39.8$
N75/N37	$w/t \le (w/t)_{Max}$ Cumple	x: 0.3 m $\eta = 0.4$	x: 0.3 m $\eta = 0.5$	x: 0.3 m $\eta = 0.8$	x: 0 m $\eta = 3.8$	x: 0 m $\eta = 14.0$	$\eta = 4.7$	x: 0.3 m $\eta = 1.2$	x: 0 m $\eta = 4.2$	x: 0 m $\eta = 14.2$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 2.2$	x: 0.3 m $\eta = 18.1$	x: 0 m $\eta = 16.3$	x: 0 m $\eta = 17.8$	CUMPLE $\eta = 18.1$
N71/N40	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 0.8$	x: 0.3 m $\eta = 15.4$	x: 0 m $\eta = 22.8$	$\eta = 7.6$	x: 0.3 m $\eta = 5.1$	x: 0.3 m $\eta = 15.7$	x: 0 m $\eta = 23.2$	x: 0.3 m $\eta = 2.7$	x: 0 m $\eta = 6.0$	x: 0.3 m $\eta = 48.1$	x: 0.3 m $\eta = 20.1$	x: 0.3 m $\eta = 34.0$	CUMPLE $\eta = 48.1$
N76/N38	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 0.5$	$\eta = 0.6$	$\eta = 0.8$	x: 0 m $\eta = 9.0$	x: 0 m $\eta = 8.8$	$\eta = 2.9$	x: 0.3 m $\eta = 2.6$	x: 0 m $\eta = 9.3$	x: 0 m $\eta = 9.0$	x: 0 m $\eta = 0.9$	x: 0 m $\eta = 0.9$	x: 0 m $\eta = 16.0$	x: 0 m $\eta = 14.2$	x: 0 m $\eta = 12.9$	CUMPLE $\eta = 16.0$
N72/N41	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 2.1$	x: 0.3 m $\eta = 22.2$	x: 0 m $\eta = 21.3$	$\eta = 7.1$	x: 0.3 m $\eta = 7.4$	x: 0.3 m $\eta = 23.0$	x: 0 m $\eta = 22.2$	x: 0.3 m $\eta = 5.8$	x: 0 m $\eta = 5.4$	x: 0.3 m $\eta = 53.7$	x: 0.3 m $\eta = 24.3$	x: 0.3 m $\eta = 36.7$	CUMPLE $\eta = 53.7$
N77/N39	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 0.3$	$\eta = 0.3$	$\eta = 0.7$	x: 0.3 m $\eta = 2.9$	x: 0.3 m $\eta = 21.5$	x: 0 m $\eta = 7.1$	x: 0.3 m $\eta = 1.0$	x: 0.3 m $\eta = 3.0$	x: 0.3 m $\eta = 21.6$	x: 0.3 m $\eta = 0.1$	x: 0.3 m $\eta = 5.2$	x: 0.3 m $\eta = 29.7$	x: 0.3 m $\eta = 23.3$	x: 0.3 m $\eta = 27.1$	CUMPLE $\eta = 29.7$
N54/N23	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta = 0.1$	$\eta = 0.3$	x: 0.3 m $\eta = 35.1$	x: 0.3 m $\eta = 17.8$	$\eta = 5.9$	x: 0.3 m $\eta = 11.7$	x: 0.3 m $\eta = 35.1$	x: 0.3 m $\eta = 17.9$	x: 0.3 m $\eta = 13.7$	x: 0.3 m $\eta = 3.5$	x: 0.3 m $\eta = 49.5$	x: 0.3 m $\eta = 46.8$	x: 0.3 m $\eta = 44.7$	CUMPLE $\eta = 49.5$
N57/N29	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 0.1$	$\eta < 0.1$	$\eta = 0.8$	x: 0.3 m $\eta = 10.0$	x: 0.3 m $\eta = 22.7$	$\eta = 7.5$	x: 0.3 m $\eta = 3.2$	x: 0.3 m $\eta = 10.3$	x: 0.3 m $\eta = 22.7$	x: 0.3 m $\eta = 1.2$	x: 0.3 m $\eta = 5.7$	x: 0.3 m $\eta = 34.3$	x: 0.3 m $\eta = 26.4$	x: 0.3 m $\eta = 29.0$	CUMPLE $\eta = 34.3$
N53/N22	$w/t \le (w/t)_{Max}$ Cumple	x: 0.15 m $\eta = 5.9$	x: 0.15 m $\eta = 6.5$	x: 0.15 m $\eta = 0.8$	x: 0.3 m $\eta = 73.5$	x: 0.3 m $\eta = 25.0$	x: 0 m $\eta = 8.3$	x: 0.15 m $\eta = 24.5$	x: 0.3 m $\eta = 73.7$	x: 0.3 m $\eta = 25.3$	x: 0.3 m $\eta = 60.3$	x: 0.3 m $\eta = 7.1$	x: 0.3 m $\eta = 29.3$	x: 0.3 m $\eta = 15.2$	x: 0.3 m $\eta = 16.5$	CUMPLE $\eta = 29.3$
N52/N28	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 10.1$	$\eta = 10.7$	$\eta = 1.2$	x: 0 m $\eta = 10.7$	x: 0.3 m $\eta = 28.0$	$\eta = 9.0$	x: 0.3 m $\eta = 2.8$	x: 0 m $\eta = 11.1$	x: 0.3 m $\eta = 28.4$	x: 0 m $\eta = 1.3$	x: 0.3 m $\eta = 8.9$	x: 0 m $\eta = 56.4$	x: 0 m $\eta = 41.3$	x: 0.3 m $\eta = 45.8$	CUMPLE $\eta = 56.4$
N55/N25	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 1.4$	x: 0 m $\eta = 34.4$	x: 0 m $\eta = 14.9$	$\eta = 4.9$	x: 0.3 m $\eta = 45.0$	x: 0 m $\eta = 35.1$	x: 0 m $\eta = 15.5$	x: 0 m $\eta = 22.6$	x: 0 m $\eta = 2.6$	x: 0 m $\eta = 83.7$	x: 0 m $\eta = 48.2$	x: 0 m $\eta = 83.0$	CUMPLE $\eta = 83.0$
N51/N27	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 0.1$	$\eta = 0.1$	$\eta = 0.9$	x: 0 m $\eta = 43.8$	x: 0.3 m $\eta = 29.4$	$\eta = 12.5$	x: 0.3 m $\eta = 60.9$	x: 0 m $\eta = 44.2$	x: 0.3 m $\eta = 29.8$	x: 0 m $\eta = 45.0$	x: 0.3 m $\eta = 10.4$	x: 0 m $\eta = 15.5$	x: 0 m $\eta = 73.5$	x: 0 m $\eta = 36.3$	CUMPLE $\eta = 36.3$
N56/N24	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 0.1$	x: 0.3 m $\eta = 52.5$	x: 0 m $\eta = 3.9$	$\eta = 1.7$	x: 0.3 m $\eta = 64.9$	x: 0.3 m $\eta = 52.6$	x: 0 m $\eta = 3.9$	x: 0.3 m $\eta = 74.9$	x: 0 m $\eta = 0.2$	x: 0.3 m $\eta = 95.4$	x: 0.3 m $\eta = 54.3$	x: 0.3 m $\eta = 63.4$	CUMPLE $\eta = 63.4$
N50/N26	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 0.1$	$\eta = 0.1$	$\eta = 0.5$	x: 0.3 m $\eta = 20.5$	x: 0.3 m $\eta = 29.3$	$\eta = 12.0$	x: 0.3 m $\eta = 49.5$	x: 0.3 m $\eta = 20.7$	x: 0.3 m $\eta = 29.5$	x: 0.3 m $\eta = 70.3$	x: 0.3 m $\eta = 10.1$	x: 0.3 m $\eta = 86.0$	x: 0.3 m $\eta = 50.3$	x: 0.3 m $\eta = 40.2$	CUMPLE $\eta = 40.2$
N73/N79	$w/t \le (w/t)_{Max}$ Cumple	x: 0.745 m $\eta = 2.7$	x: 0 m $\eta = 18.8$	$\eta = 0.8$	x: 1.118 m $\eta = 1.7$	x: 1.118 m $\eta = 4.5$	x: 0.186 m $\eta = 0.5$	x: 0 m $\eta = 0.2$	x: 1.118 m $\eta = 2.1$	x: 1.118 m $\eta = 4.8$	x: 1.118 m $\eta < 0.1$	x: 1.118 m $\eta = 0.2$	N.P.[1]	x: 1.118 m $\eta = 22.2$	x: 1.118 m $\eta = 21.2$	CUMPLE $\eta = 22.2$
N33/N80	$w/t \le (w/t)_{Max}$ Cumple	x: 1.118 m $\eta = 1.8$	x: 0 m $\eta = 12.1$	$\eta = 0.8$	x: 0.932 m $\eta = 1.1$	x: 1.118 m $\eta = 4.6$	x: 0.186 m $\eta = 0.5$	x: 0 m $\eta = 0.1$	x: 0.932 m $\eta = 1.5$	x: 1.118 m $\eta = 4.8$	x: 0.932 m $\eta < 0.1$	x: 1.118 m $\eta = 0.2$	N.P.[1]	x: 1.118 m $\eta = 14.7$	x: 1.118 m $\eta = 13.8$	CUMPLE $\eta = 14.7$
N68/N79	$w/t \le (w/t)_{Max}$ Cumple	x: 0.671 m $\eta = 3.7$	x: 0.168 m $\eta = 9.7$	x: 0.335 m $\eta = 0.6$	x: 0 m $\eta = 1.3$	x: 1.006 m $\eta = 1.8$	x: 0.335 m $\eta = 0.1$	x: 1.006 m $\eta = 0.1$	x: 0 m $\eta = 1.3$	x: 1.006 m $\eta = 2.0$	x: 0 m $\eta < 0.1$	x: 1.006 m $\eta < 0.1$	N.P.[1]	x: 1.006 m $\eta = 11.1$	x: 1.006 m $\eta = 10.9$	CUMPLE $\eta = 11.1$
N67/N79	$w/t \le (w/t)_{Max}$ Cumple	x: 0.476 m $\eta = 5.5$	x: 0.476 m $\eta = 4.0$	x: 0.476 m $\eta = 0.4$	x: 0 m $\eta = 0.9$	x: 0.953 m $\eta = 1.3$	x: 0.953 m $\eta = 0.1$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 1.0$	x: 0.953 m $\eta = 1.5$	x: 0 m $\eta < 0.1$	x: 0.953 m $\eta < 0.1$	N.P.[1]	x: 0.953 m $\eta = 5.9$	x: 0.953 m $\eta = 6.9$	CUMPLE $\eta = 6.9$
N32/N80	$w/t \le (w/t)_{Max}$ Cumple	x: 0.503 m $\eta = 2.8$	x: 0.503 m $\eta = 7.1$	x: 0.503 m $\eta = 0.4$	x: 0 m $\eta = 0.9$	x: 1.006 m $\eta = 2.8$	x: 0.503 m $\eta = 0.2$	x: 1.006 m $\eta = 0.1$	x: 0 m $\eta = 1.0$	x: 1.006 m $\eta = 2.9$	x: 0 m $\eta < 0.1$	x: 1.006 m $\eta = 0.1$	N.P.[1]	x: 1.006 m $\eta = 8.2$	x: 1.006 m $\eta = 8.1$	CUMPLE $\eta = 8.2$
N31/N80	$w/t \le (w/t)_{Max}$ Cumple	x: 0.953 m $\eta = 4.5$	x: 0 m $\eta = 2.7$	x: 0.476 m $\eta = 0.2$	x: 0 m $\eta = 0.8$	x: 0 m $\eta = 1.3$	$\eta = 0.1$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 0.8$	x: 0.953 m $\eta = 1.1$	x: 0 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.[1]	x: 0.953 m $\eta = 4.2$	x: 0.953 m $\eta = 5.7$	CUMPLE $\eta = 5.7$
N79/N81	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m $\eta = 21.8$	$\eta = 0.7$	x: 1.119 m $\eta = 1.4$	x: 0 m $\eta = 2.8$	x: 0.186 m $\eta = 0.2$	x: 0 m $\eta = 0.1$	x: 1.119 m $\eta = 1.6$	x: 0 m $\eta = 3.1$	x: 1.119 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	N.P.[1]	x: 1.119 m $\eta = 24.7$	x: 1.119 m $\eta = 23.9$	CUMPLE $\eta = 24.7$
N81/N82	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m $\eta = 23.5$	x: 0 m $\eta = 0.5$	x: 1.122 m $\eta = 1.7$	x: 0 m $\eta = 4.0$	$\eta = 0.6$	x: 0 m $\eta = 0.1$	x: 1.122 m $\eta = 1.9$	x: 0 m $\eta = 4.0$	x: 1.122 m $\eta < 0.1$	x: 0 m $\eta = 0.2$	N.P.[1]	x: 1.122 m $\eta = 26.2$	x: 1.122 m $\eta = 25.7$	CUMPLE $\eta = 26.2$
N80/N83	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m $\eta = 14.5$	x: 1.119 m $\eta = 0.7$	x: 0.746 m $\eta = 1.1$	x: 0 m $\eta = 2.9$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 0.1$	x: 0.746 m $\eta = 1.4$	x: 0 m $\eta = 3.2$	x: 0.746 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	N.P.[1]	x: 1.119 m $\eta = 17.0$	x: 1.119 m $\eta = 16.3$	CUMPLE $\eta = 17.0$

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_yTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N83/N84	$w / t \leq (w / t)_{Max.}$ Cumple	N.P.[4]	x: 0 m η = 15.9	x: 0.935 m η = 0.7	x: 0.748 m η = 1.2	x: 0 m η = 4.1	x: 0.935 m η = 0.6	x: 0 m η = 0.1	x: 0.748 m η = 1.3	x: 0 m η = 4.4	x: 0.748 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 0.374 m η = 18.1	x: 0.561 m η = 17.6	CUMPLE η = 18.1
N79/N80	$w / t \leq (w / t)_{Max.}$ Cumple	η = 0.4	η = 0.4	η = 0.2	x: 0 m η = 5.9	x: 0.3 m η = 7.4	x: 0 m η = 2.4	x: 0.3 m η = 1.6	x: 0 m η = 6.0	x: 0.3 m η = 7.5	x: 0 m η = 0.4	x: 0.3 m η = 0.6	x: 0 m η = 14.0	x: 0 m η = 13.6	x: 0 m η = 11.9	CUMPLE η = 14.0
N81/N83	$w / t \leq (w / t)_{Max.}$ Cumple	η = 0.2	η = 0.3	η = 0.2	x: 0 m η = 3.9	x: 0 m η = 11.2	η = 3.7	x: 0.3 m η = 1.3	x: 0 m η = 2.8	x: 0 m η = 11.3	x: 0 m η = 0.2	x: 0 m η = 1.4	x: 0.3 m η = 16.4	x: 0 m η = 13.9	x: 0 m η = 14.2	CUMPLE η = 16.4
N82/N84	$w / t \leq (w / t)_{Max.}$ Cumple	η = 0.5	η = 0.5	η = 0.2	x: 0 m η = 5.7	x: 0 m η = 15.7	x: 0.3 m η = 5.2	x: 0.3 m η = 0.9	x: 0 m η = 5.8	x: 0 m η = 15.8	x: 0 m η = 0.3	x: 0 m η = 2.8	x: 0 m η = 25.4	x: 0 m η = 21.7	x: 0 m η = 20.9	CUMPLE η = 25.4
N67/N81	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.17 m η = 3.5	x: 0 m η = 7.5	η = 0.7	x: 0 m η = 1.1	x: 0 m η = 2.0	η = 0.2	x: 1.017 m η = 0.1	x: 0 m η = 1.2	x: 0 m η = 2.3	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 8.8	x: 0 m η = 8.6	CUMPLE η = 8.8
N66/N81	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.731 m η = 4.4	x: 0.731 m η = 4.0	η = 0.2	x: 0 m η = 0.8	x: 0.974 m η = 1.7	x: 0.974 m η = 0.2	x: 0.974 m η = 0.1	x: 0 m η = 0.9	x: 0.974 m η = 1.8	x: 0 m η < 0.1	x: 0.974 m η < 0.1	N.P.[1]	x: 0.974 m η = 6.4	x: 0.974 m η = 6.1	CUMPLE η = 6.4
N66/N82	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.34 m η = 3.1	x: 0.34 m η = 5.3	η = 0.6	x: 0 m η = 0.7	x: 1.021 m η = 5.0	x: 0.34 m η = 0.4	x: 1.021 m η = 0.1	x: 0 m η = 0.8	x: 1.021 m η = 5.2	x: 0 m η < 0.1	x: 1.021 m η = 0.3	N.P.[1]	x: 0 m η = 6.6	x: 1.021 m η = 7.2	CUMPLE η = 7.2
N65/N82	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.985 m η = 3.0	x: 0 m η = 4.1	η = 0.1	x: 0 m η = 0.9	x: 0.985 m η = 6.7	η = 0.5	x: 0.985 m η = 0.1	x: 0 m η = 1.0	x: 0.985 m η = 6.7	x: 0 m η < 0.1	x: 0.985 m η = 0.5	x: 0.985 m η = 8.2	x: 0.985 m η = 9.0	x: 0.985 m η = 9.9	CUMPLE η = 9.9
N31/N83	$w / t \leq (w / t)_{Max.}$ Cumple	x: 1.017 m η = 3.2	x: 0 m η = 5.9	x: 0.678 m η = 0.4	x: 0 m η = 0.7	x: 1.017 m η = 1.7	η = 0.1	x: 1.017 m η = 0.1	x: 0 m η = 0.8	x: 1.017 m η = 1.8	x: 0 m η < 0.1	x: 1.017 m η < 0.1	N.P.[1]	x: 0 m η = 7.0	x: 0 m η = 6.8	CUMPLE η = 7.0
N30/N83	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.974 m η = 4.2	x: 0 m η = 3.4	η = 0.2	x: 0 m η = 0.6	x: 0.974 m η = 1.7	x: 0 m η = 0.2	x: 0 m η = 0.1	x: 0 m η = 0.7	x: 0.974 m η = 1.7	x: 0 m η < 0.1	x: 0.974 m η < 0.1	N.P.[1]	x: 0.974 m η = 5.6	x: 0.974 m η = 5.8	CUMPLE η = 5.8
N30/N84	$w / t \leq (w / t)_{Max.}$ Cumple	x: 1.021 m η = 3.5	x: 0 m η = 4.9	x: 0.681 m η = 0.2	x: 0.17 m η = 0.5	x: 0 m η = 2.5	x: 0.34 m η = 0.2	x: 1.021 m η = 0.1	x: 0 m η = 0.6	x: 0 m η = 2.5	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 1.021 m η = 6.5	x: 1.021 m η = 6.3	CUMPLE η = 6.5
N21/N84	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.985 m η = 3.9	x: 0 m η = 4.2	x: 0.492 m η = 0.6	x: 0.985 m η = 0.6	x: 0.985 m η = 2.6	x: 0.246 m η = 0.2	x: 0.985 m η = 0.1	x: 0.985 m η = 0.6	x: 0.985 m η = 2.8	x: 0.985 m η < 0.1	x: 0.985 m η = 0.1	N.P.[1]	x: 0 m η = 6.7	x: 0 m η = 6.6	CUMPLE η = 6.7
N65/N85	$w / t \leq (w / t)_{Max.}$ Cumple	x: 1.026 m η = 3.3	x: 0 m η = 3.2	x: 0.513 m η = 0.3	x: 0.171 m η = 0.6	x: 1.026 m η = 5.9	η = 0.5	x: 1.026 m η = 0.1	x: 0.171 m η = 0.6	x: 1.026 m η = 6.0	x: 0.171 m η < 0.1	x: 1.026 m η = 0.4	x: 1.026 m η = 8.3	x: 1.026 m η = 6.5	x: 1.026 m η = 7.6	CUMPLE η = 8.3
N64/N85	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.336 m η = 2.3	x: 0.336 m η = 4.9	η = 0.2	x: 0 m η = 1.0	x: 1.007 m η = 5.9	η = 0.6	x: 1.007 m η = 0.1	x: 0 m η = 1.0	x: 1.007 m η = 5.9	x: 0 m η < 0.1	x: 1.007 m η = 0.4	x: 1.007 m η = 8.1	x: 0 m η = 7.9	x: 0 m η = 8.6	CUMPLE η = 8.6
N82/N85	$w / t \leq (w / t)_{Max.}$ Cumple	N.P.[4]	x: 0 m η = 23.8	η = 1.3	x: 0.747 m η = 1.2	x: 1.12 m η = 5.9	x: 1.12 m η = 0.8	x: 0 m η = 0.1	x: 0.747 m η = 1.3	x: 1.12 m η = 6.5	x: 0.56 m η < 0.1	x: 1.12 m η = 0.4	N.P.[1]	x: 1.12 m η = 26.1	x: 0.933 m η = 25.5	CUMPLE η = 26.1
N86/N85	$w / t \leq (w / t)_{Max.}$ Cumple	N.P.[4]	x: 0 m η = 22.8	η = 0.8	x: 1.122 m η = 1.5	x: 1.122 m η = 7.5	η = 1.1	x: 0 m η = 0.1	x: 1.122 m η = 1.8	x: 1.122 m η = 7.7	x: 1.122 m η < 0.1	x: 1.122 m η = 0.6	N.P.[1]	x: 0.561 m η = 25.4	x: 1.122 m η = 24.8	CUMPLE η = 25.4
N87/N86	$w / t \leq (w / t)_{Max.}$ Cumple	N.P.[4]	x: 0 m η = 21.1	η = 0.5	x: 1.131 m η = 1.2	x: 0 m η = 3.2	x: 1.131 m η = 0.3	x: 0 m η = 0.1	x: 1.131 m η = 1.4	x: 0 m η = 3.3	x: 0.943 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 1.131 m η = 24.1	x: 1.131 m η = 23.3	CUMPLE η = 24.1
N88/N87	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.94 m η = 0.5	x: 0 m η = 18.2	x: 0.564 m η = 1.1	x: 1.128 m η = 1.7	x: 0 m η = 4.0	x: 1.128 m η = 0.2	x: 0 m η = 0.2	x: 1.128 m η = 2.2	x: 0 m η = 4.2	x: 1.128 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 1.128 m η = 21.3	x: 1.128 m η = 20.4	CUMPLE η = 21.3
N89/N88	$w / t \leq (w / t)_{Max.}$ Cumple	x: 1.138 m η = 2.7	x: 0 m η = 14.0	η = 1.2	x: 1.138 m η = 1.4	x: 0 m η = 14.0	x: 0.569 m η = 2.2	x: 0 m η = 0.2	x: 1.138 m η = 2.0	x: 0 m η = 14.1	x: 1.138 m η < 0.1	x: 0 m η = 2.0	x: 0 m η = 8.3	x: 0 m η = 20.8	x: 0 m η = 23.6	CUMPLE η = 23.6
N90/N89	$w / t \leq (w / t)_{Max.}$ Cumple	x: 1.148 m η = 4.2	x: 1.148 m η = 10.7	x: 0.574 m η = 2.6	x: 1.148 m η = 1.5	x: 1.148 m η = 10.2	x: 0.574 m η = 1.4	x: 0 m η = 0.2	x: 1.148 m η = 2.1	x: 1.148 m η = 11.0	x: 1.148 m η < 0.1	x: 1.148 m η = 1.2	x: 1.148 m η = 7.2	x: 1.148 m η = 17.4	x: 1.148 m η = 16.7	CUMPLE η = 17.4
N91/N90	$w / t \leq (w / t)_{Max.}$ Cumple	x: 1.129 m η = 6.7	x: 0 m η = 9.4	η = 1.9	x: 0 m η = 2.4	x: 0 m η = 2.4	η = 0.1	x: 0 m η = 0.4	x: 0 m η = 3.3	x: 0 m η = 3.2	x: 0 m η = 0.1	x: 0 m η = 0.1	x: 0 m η = 10.2	x: 1.129 m η = 11.3	x: 1.129 m η = 10.7	CUMPLE η = 11.3
N92/N91	$w / t \leq (w / t)_{Max.}$ Cumple	x: 1.12 m η = 10.4	x: 0 m η = 7.6	η = 1.8	x: 0 m η = 4.4	x: 1.12 m η = 5.2	η = 0.8	x: 0 m η = 0.6	x: 0 m η = 5.2	x: 1.12 m η = 5.7	x: 0 m η = 0.3	x: 1.12 m η = 0.3	x: 0 m η = 15.5	x: 1.12 m η = 8.9	x: 0 m η = 14.5	CUMPLE η = 15.5
N45/N92	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.677 m η = 8.5	x: 0.677 m η = 4.5	η = 4.5	x: 0.902 m η = 3.3	x: 0 m η = 11.3	x: 0.451 m η = 1.5	x: 0.902 m η = 0.7	x: 0.902 m η = 3.6	x: 0 m η = 13.0	x: 0.902 m η = 0.1	x: 0 m η = 1.7	x: 0 m η = 26.6	x: 0 m η = 17.6	x: 0 m η = 20.9	CUMPLE η = 26.6
N64/N86	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.689 m η = 3.8	x: 0.689 m η = 2.5	x: 0 m η = 0.2	x: 0 m η = 0.5	x: 1.034 m η = 1.9	η = 0.1	x: 1.034 m η = 0.1	x: 0 m η = 0.6	x: 1.034 m η = 2.0	x: 0 m η < 0.1	x: 1.034 m η < 0.1	N.P.[1]	x: 1.034 m η = 4.4	x: 1.034 m η = 5.1	CUMPLE η = 5.1
N63/N86	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.341 m η = 2.4	x: 0.341 m η = 5.6	x: 0.683 m η = 0.7	x: 0 m η = 1.1	x: 1.024 m η = 1.6	η = 0.1	x: 1.024 m η = 0.1	x: 0 m η = 1.2	x: 0 m η = 1.8	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 1.024 m η = 6.5	x: 1.024 m η = 6.5	CUMPLE η = 6.5
N63/N87	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.507 m η = 3.9	x: 0.507 m η = 2.1	η = 0.1	x: 0 m η = 0.8	x: 0 m η = 2.1	x: 0.507 m η = 0.2	x: 0 m η = 0.1	x: 0 m η = 0.6	x: 0 m η = 2.2	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 3.0	x: 0 m η = 5.9	CUMPLE η = 5.9
N62/N87	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.167 m η = 1.3	x: 0 m η = 8.1	x: 0.502 m η = 0.5	x: 0 m η = 1.3	x: 1.003 m η = 4.1	x: 0.502 m η = 0.3	x: 1.003 m η = 0.1	x: 0 m η = 1.4	x: 1.003 m η = 4.3	x: 0 m η < 0.1	x: 1.003 m η = 0.2	N.P.[1]	x: 1.003 m η = 10.7	x: 1.003 m η = 10.4	CUMPLE η = 10.7
N62/N88	$w / t \leq (w / t)_{Max.}$ Cumple	x: 1.011 m η = 6.5	x: 0.843 m η = 0.2	η = 0.2	x: 0 m η = 0.7	x: 1.011 m η = 6.1	η = 0.5	x: 0 m η = 0.1	x: 0 m η = 0.7	x: 1.011 m η = 6.2	x: 0 m η < 0.1	x: 1.011 m η = 0.4	x: 1.011 m η = 12.0	x: 0 m η = 0.9	x: 1.011 m η = 11.3	CUMPLE η = 12.0
N61/N88	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0 m η = 0.8	x: 0 m η = 10.5	x: 0.337 m η = 0.7	x: 0 m η = 1.4	x: 1.012 m η = 5.8	x: 0.337 m η = 0.5	x: 1.012 m η = 0.1	x: 0 m η = 1.5	x: 1.012 m η = 6.1	x: 0 m η < 0.1	x: 1.012 m η = 0.4	N.P.[1]	x: 1.012 m η = 13.7	x: 1.012 m η = 13.3	CUMPLE η = 13.7
N61/N89	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.999 m η = 7.8	N.P.[2]	x: 0.5 m η = 0.4	x: 0 m η = 0.7	x: 0 m η = 6.0	x: 0.5 m η = 0.6	x: 0 m η = 0.1	x: 0 m η = 0.8	x: 0 m η = 6.2	x: 0 m η < 0.1	x: 0 m η = 0.4	x: 0.999 m η = 12.4	N.P.[3]	x: 0.999 m η = 11.4	CUMPLE η = 12.4
N60/N89	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.745 m η = 0.8	x: 0 m η = 13.2	x: 0.497 m η = 0.5	x: 0 m η = 2.1	x: 0 m η = 5.6	x: 0.497 m η = 0.5	x: 0.993 m η = 0.2	x: 0 m η = 2.2	x: 0 m η = 5.8	x: 0 m η < 0.1	x: 0 m η = 0.3	x: 0 m η = 8.0	x: 0.993 m η = 16.7	x: 0.993 m η = 16.2	CUMPLE η = 16.7
N60/N90	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.968 m η = 8.9	x: 0.242 m η = 1.5	η = 0.5	x: 0 m η = 1.8	x: 0.968 m η = 2.5	η = 0.1	x: 0 m η = 0.2	x: 0 m η = 1.6	x: 0.968 m η = 2.7	x: 0 m η < 0.1	x: 0.968 m η = 0.1	N.P.[1]	x: 0.968 m η = 4.5	x: 0 m η = 11.7	CUMPLE η = 11.7
N59/N90	$w / t \leq (w / t)_{Max.}$ Cumple	N.P.[4]	x: 0 m η = 16.3	x: 0.941 m η = 0.8	x: 0 m η = 2.1	x: 0.941 m η = 3.1	x: 0 m η = 0.2	x: 0 m η = 0.1	x: 0 m η = 2.1	x: 0.941 m η = 3.5	x: 0 m η < 0.1	x: 0.941 m η = 0.1	N.P.[1]	x: 0.941 m η = 19.1	x: 0.941 m η = 19.5	CUMPLE η = 19.5
N59/N91	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.971 m η = 13.6	N.P.[2]	η = 0.2	x: 0 m η = 2.3	x: 0 m η = 3.1	x: 0.243 m η = 0.2	x: 0.971 m η = 0.2	x: 0 m η = 2.0	x: 0 m η = 3.2	x: 0 m η = 0.1	x: 0 m η = 0.1	N.P.[1]	N.P.[3]	x: 0 m η = 17.4	CUMPLE η = 17.4
N58/N91	$w / t \leq (w / t)_{Max.}$ Cumple	N.P.[4]	x: 0 m η = 22.8	x: 0.71 m η = 0.5	x: 0 m η = 17.2	x: 0.947 m η = 3.0	x: 0 m η = 0.2	x: 0.947 m η = 1.4	x: 0 m η = 12.9	x: 0.947 m η = 3.2	x: 0 m η = 3.0	x: 0.947 m η = 0.1	N.P.[1]	x: 0 m η = 42.4	x: 0 m η = 44.3	CUMPLE η = 44.3
N58/N92	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.736 m η = 5.7	x: 0.736 m η = 7.7	x: 0.981 m η = 0.4	x: 0 m η = 17.4	x: 0 m η = 3.9	η = 0.2	x: 0 m η = 1.3	x: 0 m η = 17.4	x: 0 m η = 4.1	x: 0 m η = 3.1	x: 0 m η = 0.2	x: 0 m η = 25.1	x: 0 m η = 21.7	x: 0 m η = 24.2	CUMPLE η = 25.1
N49/N92	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.974 m η = 1.9	x: 0 m η = 8.6	η = 3.1	x: 0 m η = 16.7	x: 0.974 m η = 7.3	η = 0.7	x: 0 m η = 1.3	x: 0 m η = 14.2	x: 0.974 m η = 8.7	x: 0 m η = 2.8	x: 0.974 m η = 0.8	x: 0 m η = 19.3	x: 0 m η = 25.3	x: 0 m η = 29.5	CUMPLE η = 29.5
N21/N93	$w / t \leq (w / t)_{Max.}$ Cumple	x: 1.026 m η = 3.9	x: 0 m η = 3.8	x: 0.513 m η = 0.5	x: 0 m η = 0.4	x: 1.026 m η = 4.6	x: 0.855 m η = 0.5	x: 1.026 m η = 0.1	x: 0 m η = 0.4	x: 1.026 m η = 4.8	x: 0 m η < 0.1	x: 1.026 m η = 0.2	N.P.[1]	x: 0 m η = 6.0	x: 1.026 m η = 6.1	CUMPLE η = 6.1



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N20/N93	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.007 m η = 3.0	x: 0 m η = 4.6	x: 0.336 m η = 0.2	x: 1.007 m η = 0.6	x: 0 m η = 4.8	x: 0.336 m η = 0.5	x: 1.007 m η = 0.1	x: 1.007 m η = 0.7	x: 0 m η = 4.9	x: 1.007 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 0 m η = 6.2	x: 0 m η = 6.6	CUMPLE η = 6.6
N20/N94	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.034 m η = 3.7	x: 0 m η = 2.3	x: 1.034 m η = 0.4	x: 0 m η = 0.4	x: 0 m η = 1.5	η = 0.1	x: 0 m η = 0.1	x: 0 m η = 0.5	x: 1.034 m η = 1.5	x: 0 m η < 0.1	x: 1.034 m η < 0.1	N.P.[1]	x: 1.034 m η = 4.0	x: 0 m η = 5.0	CUMPLE η = 5.0
N84/N93	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 16.2	η = 0.4	x: 0.56 m η = 1.2	x: 1.12 m η = 6.2	x: 1.12 m η = 0.8	x: 0 m η = 0.1	x: 0.56 m η = 1.3	x: 1.12 m η = 6.3	x: 0.56 m η < 0.1	x: 1.12 m η = 0.4	N.P.[1]	x: 0.933 m η = 18.3	x: 0.747 m η = 18.0	CUMPLE η = 18.3
N94/N93	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 15.3	η = 0.9	x: 0.935 m η = 1.1	x: 1.122 m η = 7.5	η = 1.1	x: 0 m η = 0.1	x: 0.935 m η = 1.3	x: 1.122 m η = 7.7	x: 0.748 m η < 0.1	x: 1.122 m η = 0.6	N.P.[1]	x: 0 m η = 17.8	x: 0 m η = 17.2	CUMPLE η = 17.8
N19/N94	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.024 m η = 2.5	x: 0 m η = 4.6	x: 0.683 m η = 0.6	x: 0 m η = 0.7	x: 1.024 m η = 1.9	η = 0.2	x: 1.024 m η = 0.1	x: 0 m η = 0.8	x: 1.024 m η = 2.0	x: 0 m η < 0.1	x: 1.024 m η < 0.1	N.P.[1]	x: 1.024 m η = 5.6	x: 1.024 m η = 5.5	CUMPLE η = 5.6
N95/N94	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 13.9	x: 0.943 m η = 0.9	x: 0.566 m η = 1.0	x: 0 m η = 3.2	x: 1.131 m η = 0.3	x: 1.131 m η = 0.1	x: 0.566 m η = 1.3	x: 0 m η = 3.6	x: 0.377 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 1.131 m η = 16.6	x: 1.131 m η = 15.9	CUMPLE η = 16.6
N19/N95	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.013 m η = 3.8	x: 0 m η = 1.4	x: 0.675 m η = 0.1	x: 1.013 m η = 0.5	x: 0 m η = 2.0	x: 0.507 m η = 0.2	x: 0 m η = 0.1	x: 0 m η = 0.6	x: 0 m η = 2.1	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 2.1	x: 0 m η = 5.3	CUMPLE η = 5.3
N18/N95	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.167 m η = 1.4	x: 0.167 m η = 5.1	x: 0.502 m η = 0.6	x: 0 m η = 0.9	x: 1.003 m η = 3.9	x: 0.502 m η = 0.3	x: 1.003 m η = 0.1	x: 0 m η = 1.0	x: 1.003 m η = 4.2	x: 0 m η < 0.1	x: 1.003 m η = 0.2	N.P.[1]	x: 1.003 m η = 7.9	x: 1.003 m η = 8.2	CUMPLE η = 8.2
N18/N96	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.011 m η = 5.8	x: 0.169 m η = 0.3	x: 0.506 m η = 0.7	x: 1.011 m η = 0.7	x: 0 m η = 2.9	x: 0.506 m η = 0.3	x: 0 m η = 0.1	x: 0 m η = 0.8	x: 0 m η = 3.2	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 1.011 m η = 3.6	x: 0 m η = 7.7	CUMPLE η = 7.7
N96/N95	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.128 m η = 1.1	x: 0 m η = 11.6	η = 0.9	x: 1.128 m η = 1.1	x: 0 m η = 3.8	x: 0.376 m η = 0.2	x: 0 m η = 0.1	x: 1.128 m η = 1.5	x: 0 m η = 4.2	x: 0.94 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 0.564 m η = 14.0	x: 0.94 m η = 13.0	CUMPLE η = 14.0
N17/N96	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.012 m η = 0.9	x: 0 m η = 6.9	η = 0.2	x: 0 m η = 0.9	x: 0 m η = 3.0	x: 0.844 m η = 0.3	x: 1.012 m η = 0.1	x: 0 m η = 1.0	x: 0 m η = 3.1	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 1.012 m η = 10.0	x: 1.012 m η = 9.8	CUMPLE η = 10.0
N97/N96	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.138 m η = 3.0	x: 0 m η = 9.2	η = 1.2	x: 1.138 m η = 0.8	x: 0 m η = 13.8	x: 0.948 m η = 2.2	x: 0 m η = 0.1	x: 1.138 m η = 1.3	x: 0 m η = 14.2	x: 1.138 m η < 0.1	x: 0 m η = 2.1	x: 0 m η = 8.4	x: 0 m η = 17.8	x: 0 m η = 20.8	CUMPLE η = 20.8
N17/N97	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.999 m η = 6.7	N.P.[2]	η = 0.3	x: 0 m η = 0.7	x: 0 m η = 6.0	x: 0.749 m η = 0.6	x: 0 m η = 0.1	x: 0 m η = 0.7	x: 0 m η = 6.2	x: 0 m η < 0.1	x: 0 m η = 0.4	x: 0.999 m η = 12.1	N.P.[3]	x: 0.999 m η = 11.4	CUMPLE η = 12.1
N16/N97	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.248 m η = 0.8	x: 0 m η = 9.0	x: 0.497 m η = 0.4	x: 0 m η = 1.6	x: 0 m η = 5.8	x: 0.497 m η = 0.6	x: 0.993 m η = 0.2	x: 0 m η = 1.7	x: 0 m η = 5.9	x: 0 m η < 0.1	x: 0 m η = 0.4	N.P.[1]	x: 0.993 m η = 12.5	x: 0.993 m η = 12.1	CUMPLE η = 12.5
N16/N98	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.968 m η = 7.3	N.P.[2]	x: 0.968 m η = 0.7	x: 0 m η = 1.9	x: 0 m η = 1.5	η = 0.1	x: 0 m η = 0.2	x: 0 m η = 1.6	x: 0 m η = 1.8	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	N.P.[3]	x: 0 m η = 10.1	CUMPLE η = 10.1
N98/N97	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.148 m η = 5.1	x: 0 m η = 8.9	η = 1.8	x: 0.383 m η = 0.8	x: 1.148 m η = 10.1	η = 1.3	x: 0 m η = 0.1	x: 0.766 m η = 1.2	x: 1.148 m η = 10.5	x: 0.766 m η < 0.1	x: 1.148 m η = 1.1	x: 1.148 m η = 8.4	x: 1.148 m η = 13.9	x: 1.148 m η = 14.6	CUMPLE η = 14.6
N15/N98	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 10.4	x: 0.941 m η = 0.6	x: 0 m η = 2.1	x: 0.941 m η = 4.5	x: 0.706 m η = 0.3	x: 0 m η = 0.1	x: 0 m η = 2.1	x: 0.941 m η = 4.7	x: 0 m η < 0.1	x: 0.941 m η = 0.2	N.P.[1]	x: 0.941 m η = 13.0	x: 0.941 m η = 13.6	CUMPLE η = 13.6
N99/N98	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.129 m η = 6.9	x: 0 m η = 7.6	η = 1.9	x: 0 m η = 1.6	x: 0 m η = 2.5	η = 0.1	x: 0 m η = 0.2	x: 0 m η = 2.2	x: 0 m η = 3.3	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 10.2	x: 0 m η = 9.6	x: 0 m η = 9.0	CUMPLE η = 10.2
N15/N99	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.971 m η = 10.4	N.P.[2]	x: 0.485 m η = 0.1	x: 0 m η = 2.0	x: 0 m η = 3.7	η = 0.3	x: 0.971 m η = 0.2	x: 0 m η = 2.0	x: 0 m η = 3.7	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	N.P.[3]	x: 0 m η = 13.9	CUMPLE η = 13.9
N14/N99	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 15.0	x: 0.237 m η = 0.8	x: 0 m η = 14.9	x: 0.947 m η = 4.4	x: 0 m η = 0.3	x: 0.947 m η = 1.2	x: 0 m η = 12.3	x: 0.947 m η = 4.8	x: 0 m η = 2.2	x: 0.947 m η = 0.2	N.P.[1]	x: 0 m η = 31.7	x: 0 m η = 33.7	CUMPLE η = 33.7
N100/N99	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.12 m η = 10.3	x: 0 m η = 6.5	η = 1.8	x: 0 m η = 3.0	x: 1.12 m η = 5.3	η = 0.8	x: 0 m η = 0.3	x: 0 m η = 3.8	x: 1.12 m η = 5.6	x: 0 m η = 0.1	x: 1.12 m η = 0.3	x: 0 m η = 15.2	x: 0 m η = 8.4	x: 0 m η = 13.9	CUMPLE η = 15.2
N14/N100	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.981 m η = 5.2	x: 0 m η = 8.6	x: 0.981 m η = 0.5	x: 0 m η = 15.3	x: 0 m η = 3.9	η = 0.2	x: 0 m η = 1.2	x: 0 m η = 15.4	x: 0 m η = 4.1	x: 0 m η = 2.4	x: 0 m η = 0.2	x: 0 m η = 14.6	x: 0 m η = 22.3	x: 0 m η = 24.4	CUMPLE η = 24.4
N13/N100	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.974 m η = 3.0	x: 0 m η = 5.4	η = 3.2	x: 0 m η = 15.2	x: 0.974 m η = 7.3	η = 0.8	x: 0 m η = 1.2	x: 0 m η = 13.8	x: 0 m η = 8.7	x: 0 m η = 2.3	x: 0.974 m η = 0.8	x: 0 m η = 20.9	x: 0 m η = 18.5	x: 0 m η = 20.4	CUMPLE η = 20.9
N5/N100	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.677 m η = 7.7	x: 0 m η = 3.4	x: 0.902 m η = 4.5	x: 0.902 m η = 3.5	x: 0 m η = 10.7	x: 0.902 m η = 1.4	x: 0.902 m η = 0.7	x: 0.902 m η = 4.2	x: 0 m η = 12.7	x: 0.902 m η = 0.2	x: 0 m η = 1.6	x: 0 m η = 21.7	x: 0 m η = 5.5	x: 0 m η = 16.4	CUMPLE η = 21.7
N85/N93	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 1.1	η = 1.2	η = 0.1	x: 0.3 m η = 6.1	x: 0.3 m η = 13.3	x: 0 m η = 4.5	x: 0.3 m η = 1.6	x: 0.3 m η = 6.1	x: 0.3 m η = 13.4	x: 0.3 m η = 0.4	x: 0.3 m η = 2.0	x: 0.3 m η = 16.7	x: 0.3 m η = 15.6	x: 0.3 m η = 17.3	CUMPLE η = 17.3
N86/N94	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0 m η = 0.4	x: 0 m η = 0.5	x: 0 m η = 0.2	x: 0 m η = 4.2	x: 0 m η = 18.7	η = 6.2	x: 0.3 m η = 1.3	x: 0 m η = 4.3	x: 0 m η = 18.8	x: 0 m η = 0.2	x: 0 m η = 3.9	x: 0.3 m η = 26.6	x: 0 m η = 21.0	x: 0 m η = 23.8	CUMPLE η = 26.6
N87/N95	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.15 m η = 0.2	x: 0.15 m η = 0.2	η = 0.2	x: 0.3 m η = 3.9	x: 0.3 m η = 3.6	x: 0.3 m η = 1.2	x: 0.3 m η = 1.2	x: 0.3 m η = 4.0	x: 0.3 m η = 3.7	x: 0.3 m η = 0.2	x: 0.3 m η = 0.2	N.P.[1]	x: 0.3 m η = 7.6	x: 0.3 m η = 6.6	CUMPLE η = 7.6
N88/N96	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.15 m η = 1.3	x: 0.15 m η = 1.5	η = 0.4	x: 0.3 m η = 8.5	x: 0 m η = 27.0	x: 0.15 m η = 8.8	x: 0.3 m η = 1.7	x: 0.3 m η = 8.6	x: 0 m η = 27.1	x: 0.3 m η = 0.8	x: 0 m η = 8.1	x: 0.3 m η = 41.9	x: 0.3 m η = 35.8	x: 0 m η = 35.2	CUMPLE η = 41.9
N89/N97	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 2.1	η = 2.3	η = 0.3	x: 0 m η = 4.4	x: 0 m η = 16.7	η = 5.5	x: 0.3 m η = 1.4	x: 0 m η = 4.6	x: 0 m η = 16.8	x: 0 m η = 0.2	x: 0 m η = 3.1	x: 0 m η = 25.1	x: 0 m η = 21.8	x: 0 m η = 23.0	CUMPLE η = 25.1
N90/N98	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 0.7	η = 0.8	η = 0.8	x: 0 m η = 3.8	x: 0 m η = 12.3	η = 4.0	x: 0.3 m η = 1.3	x: 0 m η = 4.1	x: 0 m η = 12.5	x: 0 m η = 0.2	x: 0 m η = 1.7	x: 0.3 m η = 19.3	x: 0 m η = 14.6	x: 0 m η = 16.1	CUMPLE η = 19.3
N91/N99	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.3 m η = 0.6	x: 0.3 m η = 0.7	η = 0.8	x: 0 m η = 8.8	x: 0.3 m η = 9.7	x: 0.3 m η = 3.1	x: 0.3 m η = 2.5	x: 0 m η = 9.1	x: 0.3 m η = 9.8	x: 0 m η = 0.9	x: 0.3 m η = 1.1	x: 0 m η = 21.1	x: 0 m η = 17.9	x: 0 m η = 15.4	CUMPLE η = 21.1
N92/N100	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 0.1	η = 0.1	η = 0.7	x: 0.3 m η = 6.9	x: 0.3 m η = 24.7	x: 0.15 m η = 8.2	x: 0.3 m η = 2.2	x: 0.3 m η = 7.2	x: 0.3 m η = 24.9	x: 0.3 m η = 0.6	x: 0.3 m η = 6.9	x: 0.3 m η = 40.0	x: 0.3 m η = 30.9	x: 0.3 m η = 32.0	CUMPLE η = 40.0
N101/N102	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.41 m η = 22.0	x: 1.41 m η = 35.7	η = 1.8	x: 0 m η = 1.9	x: 1.41 m η = 18.7	η = 1.7	x: 0 m η = 0.1	x: 0 m η = 2.7	x: 1.41 m η = 19.5	x: 0 m η = 0.1	x: 1.41 m η = 3.8	x: 1.41 m η = 48.6	x: 1.41 m η = 58.4	x: 1.41 m η = 59.0	CUMPLE η = 59.0
N102/N103	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.4 m η = 13.8	x: 0 m η = 13.8	x: 0 m η = 0.6	x: 1.167 m η = 1.5	x: 0 m η = 38.1	x: 1.4 m η = 4.8	x: 0 m η = 0.1	x: 1.4 m η = 1.2	x: 0 m η = 38.4	x: 1.167 m η < 0.1	x: 0 m η = 15.0	x: 0 m η = 63.2	x: 0 m η = 52.6	x: 0 m η = 61.5	CUMPLE η = 63.2
N103/N104	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.35 m η = 13.3	x: 0 m η = 3.0	η = 1.1	x: 1.35 m η = 4.3	x: 1.35 m η = 54.3	x: 0.45 m η = 6.3	x: 0 m η = 0.3	x: 1.35 m η = 4.4	x: 1.35 m η = 54.8	x: 1.35 m η = 0.2	x: 1.35 m η = 30.4	x: 1.35 m η = 76.0	x: 1.35 m η = 11.1	x: 1.35 m η = 74.3	CUMPLE η = 76.0
N104/N105	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.79 m η = 16.5	x: 0 m η = 5.0	η = 6.9	x: 0 m η = 10.8	x: 0 m η = 51.9	x: 0.592 m η = 10.3	x: 0.79 m η = 2.2	x: 0 m η = 10.8	x: 0 m η = 55.0	x: 0 m η = 1.2	x: 0 m η = 31.3	x: 0 m η = 84.3	x: 0 m η = 60.9	x: 0 m η = 73.0	CUMPLE η = 84.3
N104/N106	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.073 m η = 2.0	x: 0 m η = 4.1	η = 2.1	x: 1.073 m η = 9.6	x: 1.073 m η = 15.4	η = 2.1	x: 1.073 m η = 1.4	x: 1.073 m η = 9.7	x: 1.073 m η = 16.4	x: 1.073 m η = 1.0	x: 1.073 m η = 2.7	x: 1.073 m η = 28.9	x: 1.073 m η = 23.4	x: 1.073 m η = 23.5	CUMPLE η = 28.9
N101/N109	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.378 m η = 19.6	x: 0.378 m η = 51.1	x: 0.378 m η = 5.1	x: 0.755 m η = 11.2	x: 0 m η = 20.2	x: 0.378 m η = 1.8	x: 0.755 m η = 1.1	x: 0.755 m η = 13.4	x: 0 m η = 22.4	x: 0.755 m η = 1.8	x: 0 m η = 5.1	x: 0 m η = 13.9	x: 0.755 m η = 59.5	x: 0.755 m η = 58.2	CUMPLE η = 59.5

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))														Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N109/N102	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.424 m η = 25.9	x: 0.424 m η = 16.5	x: 0.424 m η = 0.7	x: 0 m η = 9.4	x: 0 m η = 57.2	x: 0.424 m η = 6.6	x: 0 m η = 0.8	x: 0 m η = 9.4	x: 0 m η = 57.5	x: 0 m η = 0.9	x: 0 m η = 33.5	x: 0 m η = 86.7	x: 0 m η = 24.9	x: 0 m η = 82.9	CUMPLE η = 86.7
N102/N108	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.869 m η = 8.2	x: 0 m η = 22.1	η = 1.6	x: 0 m η = 3.8	x: 0 m η = 8.0	η = 0.6	x: 0 m η = 0.4	x: 0.869 m η = 3.5	x: 0 m η = 8.6	x: 0 m η = 0.1	x: 0 m η = 0.8	N.P.[1]	x: 0.869 m η = 26.0	x: 0.869 m η = 26.5	CUMPLE η = 26.5
N108/N103	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.983 m η = 14.0	x: 0 m η = 9.5	η = 0.4	x: 0 m η = 2.6	x: 0 m η = 29.2	η = 2.9	x: 0.983 m η = 0.2	x: 0 m η = 2.6	x: 0 m η = 29.3	x: 0 m η = 0.1	x: 0 m η = 8.7	x: 0 m η = 43.8	x: 0 m η = 12.9	x: 0 m η = 42.3	CUMPLE η = 43.8
N103/N107	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.685 m η = 5.3	x: 0.685 m η = 15.0	x: 0.514 m η = 0.8	x: 0 m η = 3.1	x: 1.028 m η = 1.5	x: 1.028 m η < 0.1	x: 0 m η = 0.3	x: 0 m η = 2.5	x: 1.028 m η = 1.8	x: 0 m η = 0.1	x: 1.028 m η < 0.1	N.P.[1]	x: 0 m η = 17.5	x: 0 m η = 18.0	CUMPLE η = 18.0
N107/N104	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 8.3	x: 0 m η = 6.5	x: 0.743 m η = 5.0	x: 0.928 m η = 1.5	x: 1.114 m η = 29.4	x: 0 m η = 2.2	x: 0 m η = 0.1	x: 1.114 m η = 3.2	x: 1.114 m η = 31.5	x: 1.114 m η = 0.1	x: 1.114 m η = 10.0	x: 1.114 m η = 49.7	x: 1.114 m η = 39.5	x: 1.114 m η = 44.1	CUMPLE η = 49.7
N106/N105	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.096 m η = 10.0	x: 0 m η = 58.1	x: 1.096 m η = 4.1	x: 0 m η = 3.8	x: 0 m η = 9.5	x: 1.096 m η = 0.5	x: 0 m η = 0.3	x: 0 m η = 4.1	x: 0 m η = 11.2	x: 0 m η = 0.2	x: 0 m η = 1.3	N.P.[1]	x: 0 m η = 63.8	x: 0 m η = 62.9	CUMPLE η = 63.8
N114/N110	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.41 m η = 21.1	x: 1.41 m η = 33.8	η = 1.8	x: 0 m η = 1.8	x: 1.41 m η = 17.6	η = 1.6	x: 0 m η = 0.1	x: 0 m η = 2.6	x: 1.41 m η = 18.4	x: 0 m η = 0.1	x: 1.41 m η = 3.4	x: 1.41 m η = 46.2	x: 1.41 m η = 55.1	x: 1.41 m η = 55.8	CUMPLE η = 55.8
N110/N111	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.4 m η = 13.8	x: 0 m η = 13.5	x: 1.4 m η = 0.6	x: 0.7 m η = 1.5	x: 0 m η = 37.0	x: 1.4 m η = 4.6	x: 0 m η = 0.1	x: 1.4 m η = 1.2	x: 0 m η = 37.3	x: 0.7 m η < 0.1	x: 0 m η = 14.1	x: 0 m η = 61.7	x: 0 m η = 51.1	x: 0 m η = 60.0	CUMPLE η = 61.7
N111/N112	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.35 m η = 13.3	x: 0 m η = 3.3	η = 1.0	x: 1.35 m η = 4.3	x: 1.35 m η = 52.6	x: 0.45 m η = 6.1	x: 0 m η = 0.3	x: 1.35 m η = 4.3	x: 1.35 m η = 53.0	x: 1.35 m η = 0.2	x: 1.35 m η = 28.5	x: 1.35 m η = 75.0	x: 1.35 m η = 5.6	x: 1.35 m η = 71.6	CUMPLE η = 75.0
N112/N113	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.79 m η = 16.3	x: 0 m η = 5.0	x: 0.395 m η = 6.6	x: 0 m η = 10.1	x: 0 m η = 50.0	x: 0.395 m η = 9.9	x: 0.79 m η = 1.9	x: 0 m η = 10.1	x: 0 m η = 52.9	x: 0 m η = 1.1	x: 0 m η = 28.9	x: 0 m η = 81.0	x: 0 m η = 9.6	x: 0 m η = 70.4	CUMPLE η = 81.0
N114/N118	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.566 m η = 20.8	x: 0.378 m η = 51.4	x: 0.378 m η = 4.8	x: 0.755 m η = 11.0	x: 0 m η = 19.4	x: 0.378 m η = 1.8	x: 0.755 m η = 1.1	x: 0.755 m η = 13.1	x: 0 m η = 21.5	x: 0.755 m η = 1.7	x: 0 m η = 4.6	x: 0 m η = 14.8	x: 0.755 m η = 59.9	x: 0.755 m η = 58.6	CUMPLE η = 59.9
N118/N110	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.424 m η = 26.0	x: 0.424 m η = 17.5	x: 0.424 m η = 0.8	x: 0 m η = 9.4	x: 0 m η = 54.5	x: 0.424 m η = 6.3	x: 0 m η = 0.8	x: 0 m η = 9.4	x: 0 m η = 54.8	x: 0 m η = 0.9	x: 0 m η = 30.5	x: 0 m η = 84.1	x: 0 m η = 26.0	x: 0 m η = 80.0	CUMPLE η = 84.1
N110/N117	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.869 m η = 8.7	x: 0 m η = 22.2	η = 1.6	x: 0 m η = 3.7	x: 0 m η = 7.8	η = 0.6	x: 0 m η = 0.4	x: 0.869 m η = 3.6	x: 0 m η = 8.5	x: 0 m η = 0.1	x: 0 m η = 0.7	N.P.[1]	x: 0.869 m η = 26.2	x: 0.869 m η = 26.6	CUMPLE η = 26.6
N117/N111	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.983 m η = 14.0	x: 0 m η = 10.0	x: 0.492 m η = 0.4	x: 0 m η = 2.6	x: 0 m η = 28.3	x: 0.492 m η = 2.9	x: 0.983 m η = 0.2	x: 0 m η = 2.7	x: 0 m η = 28.5	x: 0 m η = 0.1	x: 0 m η = 8.2	x: 0 m η = 42.0	x: 0 m η = 13.7	x: 0 m η = 40.4	CUMPLE η = 42.0
N111/N116	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.685 m η = 5.4	x: 0.685 m η = 14.9	x: 0.514 m η = 0.8	x: 0 m η = 3.0	x: 1.028 m η = 1.6	x: 0.514 m η < 0.1	x: 0 m η = 0.3	x: 0 m η = 2.4	x: 1.028 m η = 2.0	x: 0 m η = 0.1	x: 1.028 m η < 0.1	N.P.[1]	x: 0 m η = 17.6	x: 0 m η = 17.8	CUMPLE η = 17.8
N116/N112	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 8.1	x: 0 m η = 6.5	x: 0.743 m η = 4.8	x: 1.114 m η = 1.6	x: 1.114 m η = 28.7	x: 0.743 m η = 2.2	x: 0 m η = 0.1	x: 1.114 m η = 3.1	x: 1.114 m η = 30.8	x: 1.114 m η = 0.1	x: 1.114 m η = 9.5	x: 1.114 m η = 46.1	x: 1.114 m η = 38.2	x: 1.114 m η = 42.8	CUMPLE η = 46.1
N112/N115	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.073 m η = 2.0	x: 0 m η = 3.9	x: 0.715 m η = 2.4	x: 1.073 m η = 8.4	x: 1.073 m η = 14.5	x: 0.358 m η = 2.0	x: 1.073 m η = 1.2	x: 1.073 m η = 8.4	x: 1.073 m η = 15.6	x: 1.073 m η = 0.7	x: 1.073 m η = 2.5	x: 1.073 m η = 27.7	x: 1.073 m η = 21.9	x: 1.073 m η = 22.0	CUMPLE η = 27.7
N115/N113	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.365 m η = 11.0	x: 0 m η = 60.8	η = 4.2	x: 0 m η = 3.5	x: 0 m η = 10.0	x: 1.096 m η = 0.6	x: 0 m η = 0.4	x: 0 m η = 4.2	x: 0 m η = 11.8	x: 0 m η = 0.2	x: 0 m η = 1.4	N.P.[1]	x: 0 m η = 66.1	x: 0 m η = 65.2	CUMPLE η = 66.1
N106/N119	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.617 m η = 5.0	x: 0 m η = 26.6	x: 0.617 m η = 4.6	x: 0 m η = 17.4	x: 0 m η = 6.8	η = 0.9	x: 0 m η = 3.3	x: 0 m η = 17.4	x: 0 m η = 8.9	x: 0 m η = 3.1	x: 0 m η = 0.8	x: 0.617 m η = 4.7	x: 0 m η = 44.3	x: 0 m η = 48.3	CUMPLE η = 48.3
N119/N120	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.081 m η = 7.1	x: 0 m η = 18.7	x: 0.54 m η = 2.0	x: 1.081 m η = 1.7	x: 0 m η = 4.8	η = 0.8	x: 1.081 m η = 0.3	x: 1.081 m η = 1.7	x: 0 m η = 5.7	x: 1.081 m η < 0.1	x: 0 m η = 0.3	N.P.[1]	x: 1.081 m η = 20.5	x: 1.081 m η = 20.8	CUMPLE η = 20.8
N120/N121	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.363 m η = 8.6	x: 0.363 m η = 14.6	η = 1.9	x: 0 m η = 2.0	x: 1.088 m η = 1.4	x: 0.907 m η = 0.2	x: 0 m η = 0.3	x: 0 m η = 2.1	x: 1.088 m η = 2.2	x: 0 m η < 0.1	x: 1.088 m η = 0.1	x: 1.088 m η = 4.8	x: 0 m η = 17.0	x: 0 m η = 17.1	CUMPLE η = 17.1
N121/N122	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.72 m η = 9.0	x: 0.72 m η = 10.2	x: 1.08 m η = 1.0	x: 1.08 m η = 1.0	x: 0 m η = 3.5	x: 1.08 m η = 0.5	x: 0 m η = 0.2	x: 1.08 m η = 1.1	x: 0 m η = 3.9	x: 1.08 m η < 0.1	x: 0 m η = 0.2	x: 1.08 m η = 7.7	x: 0 m η = 11.2	x: 0 m η = 11.4	CUMPLE η = 11.4
N122/N123	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.085 m η = 9.6	x: 1.085 m η = 7.2	x: 1.085 m η = 0.3	x: 1.085 m η = 1.6	x: 1.085 m η = 3.0	η = 0.4	x: 0 m η = 0.2	x: 1.085 m η = 1.6	x: 1.085 m η = 3.1	x: 1.085 m η < 0.1	x: 1.085 m η = 0.1	x: 1.085 m η = 9.6	x: 0 m η = 8.0	x: 0.723 m η = 10.9	CUMPLE η = 10.9
N123/N124	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.082 m η = 10.3	x: 0 m η = 4.4	η = 0.7	x: 1.082 m η = 1.7	x: 1.082 m η = 2.9	η = 0.3	x: 0 m η = 0.1	x: 1.082 m η = 1.7	x: 1.082 m η = 3.3	x: 1.082 m η < 0.1	x: 1.082 m η = 0.1	x: 1.082 m η = 12.6	x: 0 m η = 5.4	x: 1.082 m η = 12.4	CUMPLE η = 12.6
N124/N125	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.085 m η = 12.8	x: 0.904 m η = 1.7	x: 0.362 m η = 1.0	x: 0.904 m η = 1.7	x: 0 m η = 1.9	η = 0.2	x: 0 m η = 0.1	x: 0.904 m η = 1.7	x: 0 m η = 2.3	x: 0.904 m η < 0.1	x: 0 m η = 0.1	x: 1.085 m η = 15.2	x: 0 m η = 3.4	x: 0.904 m η = 14.9	CUMPLE η = 15.2
N125/N126	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.081 m η = 14.6	x: 0 m η = 0.2	η = 0.5	x: 1.081 m η = 2.0	x: 0 m η = 1.6	η = 0.3	x: 0 m η = 0.1	x: 0.901 m η = 1.2	x: 0 m η = 1.6	x: 1.081 m η < 0.1	x: 0 m η < 0.1	x: 1.081 m η = 17.4	x: 0 m η = 1.4	x: 1.081 m η = 17.1	CUMPLE η = 17.4
N127/N126	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.08 m η = 15.2	N.P.[2]	x: 0.36 m η = 0.5	x: 0.72 m η = 2.0	x: 0 m η = 1.9	x: 1.08 m η = 0.2	x: 0 m η = 0.1	x: 0.72 m η = 1.3	x: 0 m η = 2.0	x: 0.72 m η < 0.1	x: 0 m η < 0.1	x: 0.72 m η = 17.9	N.P.[3]	x: 0.72 m η = 17.7	CUMPLE η = 17.9
N128/N127	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.084 m η = 14.3	N.P.[2]	η = 0.9	x: 0.722 m η = 1.9	x: 0 m η = 2.2	η = 0.1	x: 0 m η = 0.1	x: 0.722 m η = 2.0	x: 0 m η = 2.5	x: 0.722 m η < 0.1	x: 0 m η = 0.1	x: 1.084 m η = 16.9	N.P.[3]	x: 0.722 m η = 16.7	CUMPLE η = 16.9
N129/N128	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.08 m η = 12.0	x: 0.18 m η = 2.1	η = 0.9	x: 1.08 m η = 1.9	x: 1.08 m η = 4.7	x: 0.54 m η = 0.6	x: 0 m η = 0.1	x: 1.08 m η = 1.9	x: 1.08 m η = 5.1	x: 1.08 m η < 0.1	x: 1.08 m η = 0.3	x: 1.08 m η = 14.5	x: 0 m η = 3.6	x: 1.08 m η = 14.4	CUMPLE η = 14.5
N130/N129	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.083 m η = 9.0	x: 1.083 m η = 4.9	η = 0.6	x: 1.083 m η = 1.8	x: 0 m η = 3.5	η = 0.6	x: 0 m η = 0.2	x: 1.083 m η = 1.9	x: 0 m η = 3.8	x: 1.083 m η < 0.1	x: 0 m η = 0.1	x: 1.083 m η = 11.7	x: 0 m η = 5.9	x: 1.083 m η = 10.5	CUMPLE η = 11.7
N131/N130	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.087 m η = 8.4	x: 1.087 m η = 8.0	x: 0.724 m η = 1.2	x: 1.087 m η = 1.3	x: 0 m η = 3.3	η = 0.4	x: 0 m η = 0.2	x: 1.087 m η = 1.4	x: 0 m η = 3.8	x: 1.087 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 9.5	x: 1.087 m η = 9.1	x: 1.087 m η = 10.0	CUMPLE η = 10.0
N132/N131	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.723 m η = 7.7	x: 0.723 m η = 11.9	x: 0 m η = 1.7	x: 0 m η = 1.7	x: 0 m η = 2.0	x: 0.904 m η = 0.3	x: 0 m η = 0.3	x: 0 m η = 1.8	x: 0 m η = 2.7	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 5.6	x: 0 m η = 14.6	x: 0 m η = 14.2	CUMPLE η = 14.6
N133/N132	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.077 m η = 6.9	x: 0 m η = 16.4	x: 0 m η = 1.7	x: 1.077 m η = 1.3	x: 0 m η = 3.5	η = 0.6	x: 1.077 m η = 0.2	x: 1.077 m η = 1.4	x: 0 m η = 4.3	x: 1.077 m η < 0.1	x: 0 m η = 0.2	x: 0 m η = 3.2	x: 1.077 m η = 18.4	x: 1.077 m η = 18.2	CUMPLE η = 18.4
N115/N133	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.801 m η = 5.6	x: 0 m η = 23.8	x: 0.801 m η = 3.8	x: 0 m η = 14.6	x: 0 m η = 6.2	x: 0.801 m η = 0.8	x: 0 m η = 2.1	x: 0 m η = 10.2	x: 0 m η = 7.9	x: 0 m η = 2.2	x: 0 m η = 0.6	x: 0 m η = 8.4	x: 0 m η = 38.8	x: 0 m η = 42.1	CUMPLE η = 42.1
N135/N134	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.128 m η = 3.5	x: 0 m η = 17.3	η = 0.6	x: 1.128 m η = 2.3	x: 0 m η = 8.8	x: 0.752 m η = 1.3	x: 0 m η = 0.3	x: 1.128 m η = 2.3	x: 0 m η = 9.1	x: 1.128 m η = 0.1	x: 0 m η = 0.8	N.P.[1]	x: 1.128 m η = 20.0	x: 1.128 m η = 20.1	CUMPLE η = 20.1
N136/N135	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.126 m η = 7.0	x: 0 m η = 12.7	x: 0.751 m η = 1.3	x: 1.126 m η = 1.8	x: 1.126 m η = 6.6	x: 0.375 m η = 0.9	x: 0 m η = 0.3	x: 1.126 m η = 1.8	x: 1.126 m η = 7.2	x: 1.126 m η < 0.1	x: 1.126 m η = 0.5	x: 0 m η = 10.8	x: 1.126 m η = 16.2	x: 1.126 m η = 16.1	CUMPLE η = 16.2
N137/N136	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.188 m η = 10.5	x: 0.188 m η = 10.6	x: 1.126 m η = 1.2	x: 0 m η = 1.2	x: 0 m η = 2.2	x: 0.188 m η = 0.2	x: 0 m η = 0.3	x: 0 m η = 1.2	x: 0 m η = 2.7	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 8.4	x: 1.126 m η = 12.3	x: 0 m η = 12.6	CUMPLE η = 12.6
N138/N137	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.373 m η = 14.9	x: 0.373 m η = 8.6	η = 0.1	x: 0 m η = 8.1	x: 1.12 m η = 3.4	x: 0 m η = 0.4	x: 0 m η = 1.0	x: 0 m η = 8.1	x: 1.12 m η = 3.4	x: 0 m η = 0.7	x: 1.12 m η = 0.1	x: 0 m η = 23.9	x: 0.373 m η = 9.9	x: 0 m η = 23.1	CUMPLE η = 23.9

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N113/N138	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.187 m η = 21.5	x: 0.396 m η = 6.8	x: 0.791 m η = 4.4	x: 1.187 m η = 7.0	x: 0 m η = 13.5	x: 0.791 m η = 1.7	x: 1.187 m η = 1.0	x: 1.187 m η = 7.0	x: 0 m η = 15.5	x: 1.187 m η = 0.5	x: 0 m η = 2.4	x: 0 m η = 39.6	x: 0 m η = 18.8	x: 0 m η = 31.5	CUMPLE η = 39.6
N129/N134	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.934 m η = 9.2	x: 0.701 m η = 0.1	η = 0.2	x: 0.934 m η = 1.0	x: 0.934 m η = 1.3	η = 0.1	x: 0 m η = 0.1	x: 0 m η = 1.0	x: 0.934 m η = 1.3	x: 0.934 m η < 0.1	x: 0.934 m η < 0.1	N.P.(1)	x: 0.701 m η = 0.9	x: 0.934 m η = 10.6	CUMPLE η = 10.6
N130/N134	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.006 m η < 0.1	x: 0 m η = 17.0	η = 0.5	x: 0 m η = 1.9	x: 1.006 m η = 1.4	x: 0.335 m η = 0.1	x: 1.006 m η = 0.2	x: 0 m η = 1.0	x: 1.006 m η = 1.6	x: 0 m η < 0.1	x: 1.006 m η < 0.1	N.P.(1)	x: 0 m η = 19.3	x: 0 m η = 19.4	CUMPLE η = 19.4
N130/N135	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.94 m η = 12.1	N.P.(2)	η = 0.7	x: 0.94 m η = 1.5	x: 0.94 m η = 4.8	x: 0.235 m η = 0.5	x: 0 m η = 0.2	x: 0 m η = 1.5	x: 0.94 m η = 5.1	x: 0.94 m η < 0.1	x: 0.94 m η = 0.3	N.P.(1)	N.P.(3)	x: 0.94 m η = 14.1	CUMPLE η = 14.1
N131/N135	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.845 m η = 0.2	x: 0 m η = 21.7	x: 0.845 m η = 0.3	x: 0 m η = 2.2	x: 0 m η = 3.5	x: 0.845 m η = 0.3	x: 1.014 m η = 0.2	x: 0 m η = 1.2	x: 0 m η = 3.7	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.(1)	x: 0 m η = 24.2	x: 0 m η = 24.4	CUMPLE η = 24.4
N131/N136	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.935 m η = 14.0	x: 0.234 m η = 0.4	x: 0.234 m η = 1.0	x: 0 m η = 2.2	x: 0 m η = 2.1	x: 0.701 m η = 0.2	x: 0 m η = 0.2	x: 0 m η = 1.8	x: 0 m η = 2.5	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.(1)	x: 0 m η = 3.3	x: 0 m η = 16.8	CUMPLE η = 16.8
N132/N136	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 26.6	x: 0 m η = 0.1	x: 1.015 m η = 1.5	x: 1.015 m η = 4.8	x: 0 m η = 0.3	x: 1.015 m η = 0.2	x: 1.015 m η = 0.9	x: 1.015 m η = 4.9	x: 1.015 m η < 0.1	x: 1.015 m η = 0.2	N.P.(1)	x: 1.015 m η = 28.6	x: 1.015 m η = 28.5	CUMPLE η = 28.6
N132/N137	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.932 m η = 16.1	N.P.(2)	x: 0.233 m η = 0.5	x: 0 m η = 2.9	x: 0.932 m η = 5.1	x: 0.466 m η = 0.5	x: 0 m η = 0.3	x: 0 m η = 1.9	x: 0.932 m η = 5.3	x: 0 m η = 0.1	x: 0.932 m η = 0.3	N.P.(1)	N.P.(3)	x: 0 m η = 19.7	CUMPLE η = 19.7
N133/N137	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 30.9	x: 0.678 m η = 0.6	x: 0 m η = 4.1	x: 1.017 m η = 5.7	x: 0.678 m η = 0.4	x: 1.017 m η = 0.4	x: 1.017 m η = 2.3	x: 1.017 m η = 6.0	x: 0 m η = 0.2	x: 1.017 m η = 0.4	N.P.(1)	x: 0 m η = 35.6	x: 0 m η = 36.0	CUMPLE η = 36.0
N133/N138	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.932 m η = 16.2	N.P.(2)	η = 0.3	x: 0 m η = 4.0	x: 0.932 m η = 4.3	x: 0.466 m η = 0.3	x: 0 m η = 0.2	x: 0 m η = 2.2	x: 0.932 m η = 4.4	x: 0 m η = 0.2	x: 0.932 m η = 0.2	N.P.(1)	N.P.(3)	x: 0 m η = 21.1	CUMPLE η = 21.1
N115/N138	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 31.4	x: 0 m η = 3.0	x: 0 m η = 5.1	x: 0 m η = 8.6	x: 0.871 m η = 0.7	x: 0.871 m η = 0.5	x: 0 m η = 5.0	x: 0 m η = 9.9	x: 0 m η = 0.3	x: 0 m η = 1.0	N.P.(1)	x: 0 m η = 37.3	x: 0 m η = 37.7	CUMPLE η = 37.7
N143/N139	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.41 m η = 25.0	x: 1.41 m η = 39.4	x: 1.41 m η = 1.8	x: 0 m η = 2.0	x: 1.41 m η = 18.8	x: 1.41 m η = 1.7	x: 0 m η = 0.2	x: 0 m η = 2.8	x: 1.41 m η = 19.6	x: 0 m η = 0.1	x: 1.41 m η = 3.9	x: 1.41 m η = 51.6	x: 1.41 m η = 62.3	x: 1.41 m η = 62.9	CUMPLE η = 62.9
N139/N140	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 13.8	x: 0 m η = 13.7	x: 0 m η = 0.6	x: 1.167 m η = 1.5	x: 0 m η = 38.2	x: 0 m η = 4.7	x: 0 m η = 0.1	x: 0 m η = 1.1	x: 0 m η = 38.5	x: 1.167 m η < 0.1	x: 0 m η = 15.0	x: 0 m η = 63.1	x: 0 m η = 52.4	x: 0 m η = 61.5	CUMPLE η = 63.1
N140/N141	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.35 m η = 13.4	x: 0 m η = 3.1	η = 1.2	x: 1.35 m η = 4.4	x: 1.35 m η = 55.6	η = 6.4	x: 0 m η = 0.3	x: 1.35 m η = 4.5	x: 1.35 m η = 56.2	x: 1.35 m η = 0.2	x: 1.35 m η = 32.0	x: 1.35 m η = 82.0	x: 1.35 m η = 57.4	x: 1.35 m η = 77.7	CUMPLE η = 82.0
N141/N142	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.79 m η = 16.7	x: 0 m η = 4.9	η = 6.8	x: 0 m η = 10.5	x: 0 m η = 50.9	η = 10.3	x: 0.79 m η = 2.2	x: 0 m η = 10.6	x: 0 m η = 53.9	x: 0 m η = 1.2	x: 0 m η = 30.1	x: 0 m η = 87.7	x: 0 m η = 59.2	x: 0 m η = 74.5	CUMPLE η = 87.7
N141/N144	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.536 m η = 2.5	x: 0.536 m η = 4.6	x: 0.536 m η = 2.3	x: 1.073 m η = 9.7	x: 1.073 m η = 15.3	x: 0.536 m η = 2.1	x: 1.073 m η = 1.4	x: 1.073 m η = 9.7	x: 1.073 m η = 16.3	x: 1.073 m η = 1.0	x: 1.073 m η = 2.7	x: 1.073 m η = 27.3	x: 1.073 m η = 25.6	x: 1.073 m η = 24.2	CUMPLE η = 27.3
N139/N145	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.217 m η = 8.5	x: 0.217 m η = 22.5	x: 0.652 m η = 1.6	x: 0 m η = 3.8	x: 0 m η = 8.0	x: 0.652 m η = 0.6	x: 0 m η = 0.4	x: 0 m η = 4.1	x: 0 m η = 8.7	x: 0 m η = 0.2	x: 0 m η = 0.8	x: 0 m η = 13.3	x: 0.869 m η = 26.6	x: 0.869 m η = 27.0	CUMPLE η = 27.0
N145/N140	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.983 m η = 14.2	x: 0 m η = 9.8	η = 0.4	x: 0 m η = 2.5	x: 0 m η = 29.2	η = 2.9	x: 0.983 m η = 0.2	x: 0 m η = 2.5	x: 0 m η = 29.4	x: 0 m η = 0.1	x: 0 m η = 8.7	x: 0 m η = 46.4	x: 0 m η = 33.2	x: 0 m η = 45.4	CUMPLE η = 46.4
N140/N146	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.685 m η = 5.7	x: 0.685 m η = 15.6	x: 0.514 m η = 0.8	x: 0 m η = 3.1	x: 1.028 m η = 1.6	x: 0.171 m η < 0.1	x: 0 m η = 0.3	x: 0 m η = 2.5	x: 1.028 m η = 1.9	x: 0 m η = 0.1	x: 1.028 m η < 0.1	N.P.(1)	x: 0 m η = 18.3	x: 0 m η = 18.4	CUMPLE η = 18.4
N146/N141	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.557 m η = 9.0	x: 0.557 m η = 7.5	x: 0.928 m η = 5.1	x: 0.928 m η = 1.6	x: 1.114 m η = 30.1	x: 0.557 m η = 2.3	x: 0 m η = 0.1	x: 0 m η = 3.2	x: 1.114 m η = 32.3	x: 0 m η = 0.1	x: 1.114 m η = 10.5	x: 1.114 m η = 51.7	x: 1.114 m η = 41.8	x: 1.114 m η = 46.1	CUMPLE η = 51.7
N144/N142	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.914 m η = 9.6	x: 0 m η = 57.2	x: 0.914 m η = 3.9	x: 0 m η = 3.8	x: 0 m η = 9.4	x: 0.914 m η = 0.5	x: 0 m η = 0.3	x: 0 m η = 3.1	x: 0 m η = 11.0	x: 0 m η = 0.1	x: 0 m η = 1.2	N.P.(1)	x: 0 m η = 62.6	x: 0 m η = 62.0	CUMPLE η = 62.6
N151/N147	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.41 m η = 25.0	x: 1.41 m η = 38.6	x: 1.41 m η = 1.8	x: 0 m η = 1.9	x: 1.41 m η = 17.7	x: 1.41 m η = 1.6	x: 0 m η = 0.2	x: 0 m η = 2.7	x: 1.41 m η = 18.5	x: 0 m η = 0.1	x: 1.41 m η = 3.4	x: 1.41 m η = 50.1	x: 1.41 m η = 60.1	x: 1.41 m η = 60.7	CUMPLE η = 60.7
N147/N148	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 13.3	x: 0 m η = 12.9	x: 0 m η = 0.6	x: 0.7 m η = 1.5	x: 0 m η = 37.1	x: 0 m η = 4.6	x: 0 m η = 0.1	x: 0 m η = 1.1	x: 0 m η = 37.4	x: 0.467 m η < 0.1	x: 0 m η = 14.2	x: 0 m η = 61.3	x: 0 m η = 50.6	x: 0 m η = 59.7	CUMPLE η = 61.3
N148/N149	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.35 m η = 13.3	x: 0 m η = 4.3	η = 1.0	x: 1.35 m η = 4.4	x: 1.35 m η = 53.8	x: 1.125 m η = 6.2	x: 0 m η = 0.3	x: 1.35 m η = 4.5	x: 1.35 m η = 54.3	x: 1.35 m η = 0.2	x: 1.35 m η = 29.8	x: 1.35 m η = 80.5	x: 1.35 m η = 56.2	x: 1.35 m η = 76.0	CUMPLE η = 80.5
N149/N150	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.79 m η = 16.5	x: 0 m η = 5.2	x: 0.395 m η = 6.4	x: 0 m η = 9.8	x: 0 m η = 49.1	x: 0.395 m η = 9.9	x: 0.79 m η = 1.8	x: 0 m η = 9.9	x: 0 m η = 51.9	x: 0 m η = 1.0	x: 0 m η = 27.9	x: 0 m η = 85.3	x: 0 m η = 57.0	x: 0 m η = 72.4	CUMPLE η = 85.3
N156/N147	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.847 m η = 26.3	x: 0 m η = 17.7	η = 0.8	x: 0 m η = 9.5	x: 0 m η = 54.7	η = 6.3	x: 0 m η = 0.9	x: 0 m η = 9.6	x: 0 m η = 55.0	x: 0 m η = 0.9	x: 0 m η = 30.7	x: 0 m η = 84.8	x: 0 m η = 26.6	x: 0 m η = 78.9	CUMPLE η = 84.8
N148/N153	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.685 m η = 6.3	x: 0.685 m η = 16.1	x: 0.171 m η = 0.8	x: 0 m η = 3.0	x: 1.028 m η = 1.7	x: 0.171 m η = 0.1	x: 0 m η = 0.3	x: 0 m η = 2.5	x: 1.028 m η = 2.1	x: 0 m η = 0.1	x: 1.028 m η < 0.1	N.P.(1)	x: 0 m η = 18.9	x: 0 m η = 18.9	CUMPLE η = 18.9
N153/N149	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.186 m η = 9.2	x: 0.186 m η = 8.2	x: 0.557 m η = 4.9	x: 1.114 m η = 1.7	x: 1.114 m η = 29.2	x: 0.557 m η = 2.2	x: 0 m η = 0.1	x: 1.114 m η = 3.0	x: 1.114 m η = 31.3	x: 1.114 m η = 0.1	x: 1.114 m η = 9.9	x: 1.114 m η = 50.8	x: 1.114 m η = 41.3	x: 1.114 m η = 45.3	CUMPLE η = 50.8
N149/N152	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.536 m η = 2.1	x: 0.536 m η = 4.0	x: 0.536 m η = 2.6	x: 1.073 m η = 8.4	x: 1.073 m η = 14.3	x: 0.536 m η = 1.9	x: 1.073 m η = 1.2	x: 1.073 m η = 8.4	x: 1.073 m η = 15.4	x: 1.073 m η = 0.7	x: 1.073 m η = 2.4	x: 1.073 m η = 25.3	x: 1.073 m η = 23.7	x: 1.073 m η = 22.2	CUMPLE η = 25.3
N152/N150	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.096 m η = 10.8	x: 0 m η = 59.9	x: 0.914 m η = 4.0	x: 0 m η = 3.5	x: 0 m η = 10.0	x: 0.914 m η = 0.6	x: 0 m η = 0.4	x: 0 m η = 3.0	x: 0 m η = 11.7	x: 0 m η = 0.1	x: 0 m η = 1.4	N.P.(1)	x: 0 m η = 64.9	x: 0 m η = 64.2	CUMPLE η = 64.9
N144/N156	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.617 m η = 5.3	x: 0 m η = 26.2	η = 4.8	x: 0 m η = 17.4	x: 0 m η = 6.8	η = 1.0	x: 0 m η = 3.3	x: 0 m η = 17.4	x: 0 m η = 8.9	x: 0 m η = 3.1	x: 0 m η = 0.8	N.P.(1)	x: 0 m η = 43.9	x: 0 m η = 48.0	CUMPLE η = 48.0
N156/N157	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.081 m η = 7.3	x: 0 m η = 18.6	x: 0.18 m η = 2.0	x: 1.081 m η = 1.7	x: 0 m η = 4.9	x: 0.18 m η = 0.8	x: 1.081 m η = 0.3	x: 1.081 m η = 1.7	x: 0 m η = 5.8	x: 1.081 m η < 0.1	x: 0 m η = 0.3	x: 0 m η = 3.1	x: 1.081 m η = 20.5	x: 1.081 m η = 20.7	CUMPLE η = 20.7
N157/N158	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.088 m η = 8.8	x: 0 m η = 14.6	η = 1.8	x: 0 m η = 2.0	x: 1.088 m η = 1.2	x: 0.363 m η = 0.2	x: 0 m η = 0.3	x: 0 m η = 2.0	x: 1.088 m η = 2.0	x: 0 m η < 0.1	x: 1.088 m η < 0.1	N.P.(1)	x: 0 m η = 17.0	x: 0 m η = 17.2	CUMPLE η = 17.2
N158/N159	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.08 m η = 9.4	x: 0 m η = 10.4	x: 0.72 m η = 0.8	x: 1.08 m η = 1.0	x: 0 m η = 3.2	x: 0.72 m η = 0.5	x: 0 m η = 0.2	x: 1.08 m η = 1.1	x: 0 m η = 3.6	x: 1.08 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 5.6	x: 0 m η = 11.5	x: 0 m η = 11.6	CUMPLE η = 11.6
N159/N160	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.085 m η = 10.0	x: 1.085 m η = 7.4	x: 0.904 m η = 0.3	x: 1.085 m η = 1.6	x: 1.085 m η = 3.1	η = 0.4	x: 0 m η = 0.2	x: 1.085 m η = 1.6	x: 1.085 m η = 3.2	x: 1.085 m η < 0.1	x: 1.085 m η = 0.1	x: 1.085 m η = 9.7	x: 0 m η = 8.2	x: 0.723 m η = 11.2	CUMPLE η = 11.2
N160/N161	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.082 m η = 10.6	x: 0 m η = 4.7	x: 0 m η = 0.9	x: 1.082 m η = 1.7	x: 1.082 m η = 3.1	η = 0.3	x: 0 m η = 0.1	x: 1.082 m η = 1.7	x: 1.082 m η = 3.5	x: 1.082 m η < 0.1	x: 1.082 m η = 0.1	x: 1.082 m η = 12.9	x: 0 m η = 5.7	x: 1.082 m η = 12.7	CUMPLE η = 12.9
N161/N162	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.085 m η = 13.2	x: 1.085 m η = 2.2	x: 0.362 m η = 1.0	x: 0.904 m η = 1.7	x: 0 m η = 1.8	x: 0.904 m η = 0.2	x: 0 m η = 0.1	x: 0.542 m η = 1.2	x: 0 m η = 2.3	x: 0.904 m η < 0.1	x: 0 m η = 0.1	x: 1.085 m η = 15.5	x: 0 m η = 3.8	x: 0.904 m η = 15.3	CUMPLE η = 15.5
N162/N163	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.081 m η = 15.0	N.P.(2)	x: 0 m η = 0.4	x: 0.901 m η = 2.0	x: 0 m η = 1.6	x: 1.081 m η = 0.3	x: 0 m η = 0.1	x: 0.54 m η = 1.0	x: 0 m η = 1.6	x: 0.901 m η < 0.1	x: 0 m η < 0.1	x: 1.081 m η = 17.7	N.P.(3)	x: 0.901 m η = 17.5	CUMPLE η = 17.7

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N164/N163	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.08 m η = 15.6	N.P.[2]	x: 0.36 m η = 0.5	x: 0.54 m η = 2.0	x: 0 m η = 1.9	x: 1.08 m η = 0.2	x: 0 m η = 0.1	x: 0.54 m η = 1.0	x: 0 m η = 2.0	x: 0.54 m η < 0.1	x: 0 m η < 0.1	x: 0.72 m η = 18.3	N.P.[3]	x: 0.54 m η = 18.1	CUMPLE η = 18.3
N165/N164	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.084 m η = 14.7	N.P.[2]	x: 0.722 m η = 0.8	x: 0.722 m η = 1.9	x: 0 m η = 2.2	x: 1.084 m η = 0.2	x: 0 m η = 0.2	x: 0 m η = 1.6	x: 0 m η = 2.5	x: 0.722 m η < 0.1	x: 0 m η = 0.1	x: 0.903 m η = 17.2	N.P.[3]	x: 0.722 m η = 17.1	CUMPLE η = 17.2
N166/N165	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.08 m η = 12.4	x: 0 m η = 1.9	x: 0.36 m η = 0.8	x: 1.08 m η = 1.9	x: 1.08 m η = 4.7	η = 0.6	x: 0 m η = 0.1	x: 1.08 m η = 1.9	x: 1.08 m η = 5.1	x: 0.9 m η < 0.1	x: 1.08 m η = 0.3	x: 1.08 m η = 15.4	x: 1.08 m η = 5.9	x: 1.08 m η = 14.7	CUMPLE η = 15.4
N167/N166	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.902 m η = 9.0	x: 0.902 m η = 4.8	η = 0.6	x: 1.083 m η = 1.8	x: 1.083 m η = 3.6	x: 1.083 m η = 0.6	x: 0 m η = 0.2	x: 1.083 m η = 1.9	x: 1.083 m η = 3.8	x: 1.083 m η < 0.1	x: 1.083 m η = 0.2	x: 1.083 m η = 11.0	x: 1.083 m η = 5.8	x: 0 m η = 10.8	CUMPLE η = 11.0
N168/N167	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.087 m η = 8.7	x: 0 m η = 8.2	x: 0.543 m η = 1.1	x: 1.087 m η = 1.3	x: 0 m η = 3.2	x: 0.906 m η = 0.4	x: 0 m η = 0.2	x: 1.087 m η = 1.4	x: 0 m η = 3.7	x: 1.087 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 6.5	x: 0 m η = 9.3	x: 1.087 m η = 10.1	CUMPLE η = 10.1
N169/N168	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.085 m η = 8.0	x: 0 m η = 11.9	x: 0.542 m η = 1.7	x: 0 m η = 1.7	x: 0 m η = 1.9	x: 0.723 m η = 0.3	x: 0 m η = 0.3	x: 0 m η = 1.7	x: 0 m η = 2.7	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 14.4	x: 0 m η = 14.2	CUMPLE η = 14.4
N170/N169	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.077 m η = 6.8	x: 0 m η = 16.0	x: 0.18 m η = 1.8	x: 1.077 m η = 1.3	x: 0 m η = 3.6	x: 0.18 m η = 0.6	x: 1.077 m η = 0.2	x: 1.077 m η = 1.3	x: 0 m η = 4.3	x: 1.077 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 1.077 m η = 17.9	x: 1.077 m η = 17.7	CUMPLE η = 17.9
N152/N170	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.801 m η = 5.3	x: 0 m η = 23.4	x: 0.801 m η = 3.9	x: 0 m η = 14.6	x: 0 m η = 6.1	x: 0.801 m η = 0.8	x: 0 m η = 2.1	x: 0 m η = 10.4	x: 0 m η = 7.8	x: 0 m η = 2.2	x: 0 m η = 0.6	x: 0 m η = 13.6	x: 0 m η = 38.4	x: 0 m η = 41.7	CUMPLE η = 41.7
N172/N171	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.128 m η = 0.8	x: 0 m η = 16.7	η = 0.2	x: 1.128 m η = 2.3	x: 0 m η = 8.9	x: 1.128 m η = 1.3	x: 0 m η = 0.3	x: 1.128 m η = 2.3	x: 0 m η = 9.0	x: 1.128 m η = 0.1	x: 0 m η = 0.8	x: 1.128 m η = 2.9	x: 1.128 m η = 19.3	x: 1.128 m η = 19.5	CUMPLE η = 19.5
N173/N172	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.126 m η = 5.1	x: 0 m η = 10.3	x: 0.188 m η = 2.1	x: 1.126 m η = 1.8	x: 1.126 m η = 6.6	x: 0.188 m η = 0.9	x: 0 m η = 0.3	x: 1.126 m η = 1.9	x: 1.126 m η = 7.5	x: 1.126 m η < 0.1	x: 1.126 m η = 0.6	x: 0 m η = 8.9	x: 1.126 m η = 13.3	x: 1.126 m η = 13.6	CUMPLE η = 13.6
N174/N173	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.126 m η = 9.6	x: 0 m η = 9.4	η = 1.4	x: 0 m η = 1.2	x: 0 m η = 2.1	x: 0.188 m η = 0.2	x: 0 m η = 0.3	x: 0 m η = 1.2	x: 0 m η = 2.7	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 7.6	x: 1.126 m η = 11.2	x: 0 m η = 11.8	CUMPLE η = 11.8
N175/N174	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.12 m η = 14.7	x: 0 m η = 8.1	x: 0.373 m η = 0.5	x: 0 m η = 8.0	x: 1.12 m η = 3.3	x: 0.187 m η = 0.4	x: 0 m η = 1.0	x: 0 m η = 8.1	x: 1.12 m η = 3.5	x: 0 m η = 0.7	x: 1.12 m η = 0.1	x: 0 m η = 24.0	x: 0 m η = 9.7	x: 0 m η = 23.4	CUMPLE η = 24.0
N150/N175	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.187 m η = 21.9	x: 0.594 m η = 6.9	x: 0.594 m η = 5.1	x: 1.187 m η = 6.9	x: 0 m η = 13.3	x: 0.594 m η = 1.6	x: 1.187 m η = 1.0	x: 1.187 m η = 6.9	x: 0 m η = 15.5	x: 1.187 m η = 0.5	x: 0 m η = 2.4	x: 0 m η = 32.4	x: 0 m η = 9.1	x: 1.187 m η = 30.5	CUMPLE η = 32.4
N166/N171	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.934 m η = 9.2	x: 0.701 m η = 2.1	x: 0 m η = 0.6	x: 0.934 m η = 1.0	x: 0.934 m η = 2.1	x: 0 m η = 0.2	x: 0 m η = 0.1	x: 0 m η = 1.0	x: 0.934 m η = 2.3	x: 0.934 m η < 0.1	x: 0.934 m η = 0.1	N.P.[1]	x: 0 m η = 3.4	x: 0.934 m η = 10.5	CUMPLE η = 10.5
N167/N171	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.006 m η = 1.6	x: 0 m η = 16.9	η = 0.1	x: 0 m η = 1.9	x: 1.006 m η = 1.2	η = 0.1	x: 1.006 m η = 0.2	x: 1.006 m η = 1.0	x: 1.006 m η = 1.2	x: 0 m η < 0.1	x: 1.006 m η < 0.1	N.P.[1]	x: 0 m η = 19.0	x: 0 m η = 19.3	CUMPLE η = 19.3
N167/N172	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.94 m η = 12.2	N.P.[2]	η = 0.4	x: 0.94 m η = 1.5	x: 0.94 m η = 6.5	η = 0.6	x: 0 m η = 0.2	x: 0 m η = 1.3	x: 0.94 m η = 6.6	x: 0.94 m η < 0.1	x: 0.94 m η = 0.4	x: 0.94 m η = 14.5	N.P.[3]	x: 0.94 m η = 14.3	CUMPLE η = 14.5
N168/N172	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.014 m η = 0.2	x: 0 m η = 21.5	η = 0.1	x: 0 m η = 2.1	x: 0 m η = 4.0	η = 0.4	x: 1.014 m η = 0.2	x: 1.014 m η = 1.3	x: 0 m η = 4.0	x: 0 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 0 m η = 24.1	x: 0 m η = 24.2	CUMPLE η = 24.2
N168/N173	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.935 m η = 14.0	N.P.[2]	η = 0.4	x: 0 m η = 2.2	x: 0.935 m η = 2.7	η = 0.1	x: 0 m η = 0.2	x: 0 m η = 1.5	x: 0.935 m η = 2.9	x: 0 m η = 0.1	x: 0.935 m η = 0.1	N.P.[1]	N.P.[3]	x: 0 m η = 16.7	CUMPLE η = 16.7
N169/N173	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 26.5	x: 0.846 m η = 0.8	x: 1.015 m η = 1.5	x: 1.015 m η = 1.9	x: 0.169 m η = 0.1	x: 1.015 m η = 0.2	x: 1.015 m η = 1.1	x: 1.015 m η = 2.2	x: 1.015 m η < 0.1	x: 1.015 m η < 0.1	N.P.[1]	x: 1.015 m η = 28.3	x: 1.015 m η = 28.3	CUMPLE η = 28.3
N169/N174	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.932 m η = 16.1	N.P.[2]	x: 0.233 m η = 0.2	x: 0 m η = 2.9	x: 0 m η = 3.5	x: 0.233 m η = 0.3	x: 0 m η = 0.3	x: 0 m η = 1.7	x: 0 m η = 3.5	x: 0 m η = 0.1	x: 0 m η = 0.1	N.P.[1]	N.P.[3]	x: 0 m η = 19.6	CUMPLE η = 19.6
N170/N174	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 30.9	η = 0.1	x: 0 m η = 4.0	x: 1.017 m η = 2.2	η = 0.2	x: 1.017 m η = 0.4	x: 1.017 m η = 2.4	x: 1.017 m η = 2.2	x: 0 m η = 0.2	x: 1.017 m η = 0.1	N.P.[1]	x: 0 m η = 35.6	x: 0 m η = 35.9	CUMPLE η = 35.9
N170/N175	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.932 m η = 16.2	N.P.[2]	x: 0.233 m η = 0.2	x: 0 m η = 4.0	x: 0.932 m η = 1.5	x: 0.233 m η = 0.1	x: 0 m η = 0.2	x: 0 m η = 2.2	x: 0.932 m η = 1.6	x: 0 m η = 0.2	x: 0.932 m η < 0.1	N.P.[1]	N.P.[3]	x: 0 m η = 21.2	CUMPLE η = 21.2
N152/N175	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 31.7	x: 0.435 m η = 2.6	x: 0 m η = 5.0	x: 0 m η = 9.9	x: 0.435 m η = 0.9	x: 0.871 m η = 0.5	x: 0 m η = 4.9	x: 0 m η = 11.0	x: 0 m η = 0.3	x: 0 m η = 1.2	N.P.[1]	x: 0 m η = 37.5	x: 0 m η = 38.0	CUMPLE η = 38.0
N151/N155	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.189 m η = 21.4	x: 0.189 m η = 52.2	x: 0.755 m η = 4.8	x: 0.755 m η = 10.4	x: 0 m η = 19.4	x: 0.189 m η = 1.8	x: 0.755 m η = 1.1	x: 0.755 m η = 12.5	x: 0 m η = 21.5	x: 0.755 m η = 1.6	x: 0 m η = 4.6	x: 0 m η = 11.5	x: 0.755 m η = 57.4	x: 0.755 m η = 57.2	CUMPLE η = 57.4
N176/N139	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.847 m η = 25.8	x: 0 m η = 16.3	x: 0.847 m η = 0.7	x: 0 m η = 9.4	x: 0 m η = 57.2	x: 0.847 m η = 6.6	x: 0 m η = 0.8	x: 0 m η = 9.4	x: 0 m η = 57.5	x: 0 m η = 0.9	x: 0 m η = 33.5	x: 0 m η = 83.3	x: 0 m η = 24.8	x: 0 m η = 79.1	CUMPLE η = 83.3
N143/N176	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.189 m η = 19.5	x: 0.189 m η = 51.1	x: 0.189 m η = 5.1	x: 0.755 m η = 11.0	x: 0 m η = 20.2	x: 0.189 m η = 1.8	x: 0.755 m η = 1.2	x: 0.755 m η = 13.3	x: 0 m η = 22.5	x: 0.755 m η = 1.8	x: 0 m η = 5.1	N.P.[1]	x: 0.755 m η = 56.6	x: 0.755 m η = 56.0	CUMPLE η = 56.6
N176/N109	$w/t \leq (w/t)_{Máx.}$ Cumple	η < 0.1	η < 0.1	η = 3.5	x: 0 m η = 25.9	x: 0.3 m η = 2.5	η = 1.0	x: 0 m η = 51.8	x: 0 m η = 27.4	x: 0.3 m η = 4.0	x: 0 m η = 89.2	x: 0.3 m η = 0.2	x: 0 m η = 64.3	x: 0.3 m η = 31.3	x: 0 m η = 47.8	CUMPLE η = 47.8
N139/N102	$w/t \leq (w/t)_{Máx.}$ Cumple	η < 0.1	η < 0.1	η = 0.5	x: 0.3 m η = 28.1	x: 0.3 m η = 30.6	x: 0.15 m η = 12.6	x: 0 m η = 52.7	x: 0.3 m η = 28.3	x: 0.3 m η = 30.8	x: 0.3 m η = 92.3	x: 0.3 m η = 11.0	x: 0.3 m η = 98.8	x: 0.3 m η = 59.0	x: 0.3 m η = 70.6	CUMPLE η = 70.6
N145/N108	$w/t \leq (w/t)_{Máx.}$ Cumple	η < 0.1	η < 0.1	η < 0.1	x: 0.3 m η = 61.6	x: 0.3 m η = 4.0	x: 0.15 m η = 1.7	x: 0.15 m η = 68.8	x: 0.3 m η = 61.6	x: 0.3 m η = 4.0	x: 0 m η = 38.6	x: 0.3 m η = 0.2	x: 0.3 m η = 27.1	x: 0.3 m η = 65.7	x: 0.3 m η = 48.2	CUMPLE η = 48.2
N141/N104	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.5	η = 1.4	η = 1.0	x: 0 m η = 17.6	x: 0 m η = 27.1	η = 9.1	x: 0.3 m η = 5.7	x: 0 m η = 18.1	x: 0 m η = 27.6	x: 0 m η = 3.6	x: 0 m η = 8.4	x: 0 m η = 56.0	x: 0 m η = 46.5	x: 0 m η = 41.4	CUMPLE η = 56.0
N144/N106	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.15 m η = 0.3	x: 0.15 m η = 0.3	x: 0.15 m η = 0.6	x: 0.3 m η = 33.1	x: 0.3 m η = 14.5	x: 0.15 m η = 4.8	x: 0 m η = 11.0	x: 0.3 m η = 33.4	x: 0.3 m η = 14.8	x: 0.3 m η = 12.4	x: 0.3 m η = 2.4	x: 0.3 m η = 60.3	x: 0.3 m η = 47.9	x: 0.3 m η = 45.3	CUMPLE η = 60.3
N142/N105	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 2.5	η = 1.0	x: 0.15 m η = 0.7	x: 0.3 m η = 80.0	x: 0.3 m η = 29.3	x: 0.3 m η = 9.8	x: 0.15 m η = 26.6	x: 0.3 m η = 80.3	x: 0.3 m η = 29.7	x: 0.3 m η = 71.5	x: 0.3 m η = 9.8	x: 0.3 m η = 39.6	x: 0.3 m η = 10.9	x: 0.3 m η = 17.9	CUMPLE η = 39.6
N156/N119	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.1	η = 0.1	η = 0.7	x: 0.3 m η = 19.2	x: 0 m η = 14.8	x: 0.3 m η = 4.9	x: 0 m η = 6.3	x: 0.3 m η = 19.5	x: 0 m η = 15.1	x: 0.3 m η = 4.2	x: 0 m η = 2.5	x: 0.3 m η = 42.6	x: 0.3 m η = 34.4	x: 0.3 m η = 30.1	CUMPLE η = 42.6
N157/N120	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.2	η = 0.2	η = 0.7	x: 0.3 m η = 11.9	x: 0 m η = 18.8	x: 0.15 m η = 6.2	x: 0 m η = 3.9	x: 0.3 m η = 12.2	x: 0 m η = 19.1	x: 0.3 m η = 1.6	x: 0 m η = 4.0	x: 0.3 m η = 38.9	x: 0.3 m η = 30.9	x: 0.3 m η = 27.6	CUMPLE η = 38.9
N158/N121	$w/t \leq (w/t)_{Máx.}$ Cumple	η < 0.1	η < 0.1	η = 0.5	x: 0.3 m η = 3.8	x: 0 m η = 17.4	x: 0 m η = 5.6	x: 0 m η = 1.2	x: 0.3 m η = 4.0	x: 0 m η = 17.6	x: 0.3 m η = 0.2	x: 0 m η = 3.4	x: 0.3 m η = 26.1	x: 0.3 m η = 21.4	x: 0 m η = 22.2	CUMPLE η = 26.1
N159/N122	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.2	η = 0.2	x: 0.15 m η = 0.3	x: 0 m η = 3.0	x: 0 m η = 22.6	η = 7.6	x: 0 m η = 0.9	x: 0 m η = 3.1	x: 0 m η = 22.7	x: 0 m η = 0.1	x: 0 m η = 5.8	x: 0 m η = 32.0	x: 0 m η = 26.0	x: 0 m η = 28.7	CUMPLE η = 32.0
N160/N123	$w/t \leq (w/t)_{Máx.}$ Cumple	η < 0.1	η = 0.1	η = 0.3	x: 0 m η = 4.4	x: 0.3 m η = 16.3	η = 5.4	x: 0 m η = 1.4	x: 0 m η = 4.5	x: 0.3 m η = 16.4	x: 0 m η = 0.2	x: 0.3 m η = 3.0	x: 0 m η = 25.9	x: 0 m η = 20.3	x: 0.3 m η = 21.0	CUMPLE η = 25.9
N161/N124	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.3	η = 0.3	η = 0.4	x: 0.3 m η = 1.5	x: 0 m η = 5.9	η = 2.0	x: 0 m η = 0.5	x: 0.3 m η = 1.7	x: 0 m η = 5.9	x: 0.3 m η < 0.1	x: 0 m η = 0.4	x: 0.3 m η = 7.3	x: 0.3 m η = 6.4	x: 0 m η = 7.5	CUMPLE η = 7.5

Listados

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N162/N125	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 0.4$	x: 0 m $\eta = 2.0$	x: 0.3 m $\eta = 10.9$	$\eta = 3.7$	x: 0 m $\eta = 0.6$	x: 0 m $\eta = 2.1$	x: 0.3 m $\eta = 10.9$	x: 0 m $\eta < 0.1$	x: 0.3 m $\eta = 1.3$	x: 0.3 m $\eta = 13.7$	x: 0.3 m $\eta = 11.0$	x: 0.3 m $\eta = 13.7$	CUMPLE $\eta = 13.7$
N163/N126	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 0.1$	x: 0 m $\eta = 1.3$	x: 0 m $\eta = 12.7$	x: 0 m $\eta = 4.3$	x: 0 m $\eta = 0.4$	x: 0 m $\eta = 1.3$	x: 0 m $\eta = 12.7$	x: 0 m $\eta < 0.1$	x: 0 m $\eta = 1.8$	x: 0 m $\eta = 17.2$	x: 0 m $\eta = 8.5$	x: 0 m $\eta = 15.9$	CUMPLE $\eta = 17.2$
N164/N127	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 0.3$	x: 0 m $\eta = 2.6$	x: 0.3 m $\eta = 9.6$	x: 0.3 m $\eta = 3.2$	x: 0 m $\eta = 0.9$	x: 0 m $\eta = 2.7$	x: 0.3 m $\eta = 9.6$	x: 0 m $\eta = 0.1$	x: 0.3 m $\eta = 1.0$	x: 0.3 m $\eta = 15.2$	x: 0.3 m $\eta = 12.1$	x: 0.3 m $\eta = 12.3$	CUMPLE $\eta = 15.2$
N165/N128	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 0.5$	$\eta = 0.6$	x: 0 m $\eta = 0.4$	x: 0.3 m $\eta = 4.6$	x: 0 m $\eta = 11.2$	x: 0.3 m $\eta = 3.7$	x: 0 m $\eta = 1.6$	x: 0.3 m $\eta = 4.7$	x: 0 m $\eta = 11.4$	x: 0.3 m $\eta = 0.2$	x: 0 m $\eta = 1.4$	x: 0.3 m $\eta = 17.3$	x: 0.3 m $\eta = 14.3$	x: 0.3 m $\eta = 14.8$	CUMPLE $\eta = 17.3$
N166/N129	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 0.1$	$\eta = 0.1$	$\eta = 0.4$	x: 0.3 m $\eta = 5.4$	x: 0 m $\eta = 25.2$	x: 0.3 m $\eta = 8.4$	x: 0 m $\eta = 1.7$	x: 0.3 m $\eta = 5.5$	x: 0 m $\eta = 25.4$	x: 0.3 m $\eta = 0.3$	x: 0 m $\eta = 7.2$	x: 0.3 m $\eta = 38.2$	x: 0.3 m $\eta = 30.8$	x: 0.3 m $\eta = 32.1$	CUMPLE $\eta = 38.2$
N171/N134	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 1.2$	$\eta = 1.3$	$\eta = 0.3$	x: 0 m $\eta = 9.5$	x: 0.3 m $\eta = 25.3$	x: 0 m $\eta = 8.2$	x: 0.3 m $\eta = 2.2$	x: 0 m $\eta = 9.6$	x: 0.3 m $\eta = 25.4$	x: 0 m $\eta = 1.0$	x: 0.3 m $\eta = 7.1$	x: 0 m $\eta = 42.4$	x: 0 m $\eta = 35.0$	x: 0 m $\eta = 33.5$	CUMPLE $\eta = 42.4$
N167/N130	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 0.4$	x: 0.3 m $\eta = 4.5$	x: 0 m $\eta = 25.9$	$\eta = 8.6$	x: 0 m $\eta = 1.4$	x: 0.3 m $\eta = 4.7$	x: 0 m $\eta = 26.0$	x: 0.3 m $\eta = 0.2$	x: 0 m $\eta = 7.5$	x: 0.3 m $\eta = 38.0$	x: 0.3 m $\eta = 30.6$	x: 0.3 m $\eta = 32.7$	CUMPLE $\eta = 38.0$
N172/N135	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 1.4$	$\eta = 1.9$	$\eta = 0.4$	x: 0.3 m $\eta = 2.9$	x: 0.3 m $\eta = 11.2$	x: 0 m $\eta = 3.7$	x: 0.3 m $\eta = 0.7$	x: 0.3 m $\eta = 3.1$	x: 0.3 m $\eta = 11.4$	x: 0.3 m $\eta = 0.1$	x: 0.3 m $\eta = 1.4$	x: 0.3 m $\eta = 18.7$	x: 0.3 m $\eta = 15.8$	x: 0.3 m $\eta = 16.2$	CUMPLE $\eta = 18.7$
N168/N131	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 0.5$	x: 0.3 m $\eta = 6.1$	x: 0 m $\eta = 18.6$	x: 0 m $\eta = 6.2$	x: 0 m $\eta = 1.9$	x: 0.3 m $\eta = 6.3$	x: 0 m $\eta = 18.8$	x: 0.3 m $\eta = 0.4$	x: 0 m $\eta = 3.9$	x: 0.3 m $\eta = 30.7$	x: 0.3 m $\eta = 24.8$	x: 0 m $\eta = 24.1$	CUMPLE $\eta = 30.7$
N173/N136	$w/t \le (w/t)_{Max}$ Cumple	x: 0.3 m $\eta = 1.4$	x: 0.3 m $\eta = 1.6$	x: 0.3 m $\eta = 0.6$	x: 0 m $\eta = 4.6$	x: 0 m $\eta = 10.4$	x: 0.3 m $\eta = 3.2$	x: 0.3 m $\eta = 1.0$	x: 0 m $\eta = 4.9$	x: 0 m $\eta = 10.6$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 1.2$	x: 0 m $\eta = 19.7$	x: 0 m $\eta = 16.6$	x: 0 m $\eta = 15.4$	CUMPLE $\eta = 19.7$
N169/N132	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 0.1$	$\eta = 0.1$	$\eta = 0.6$	x: 0.3 m $\eta = 11.8$	x: 0 m $\eta = 17.3$	x: 0.3 m $\eta = 5.7$	x: 0 m $\eta = 3.8$	x: 0.3 m $\eta = 12.0$	x: 0 m $\eta = 17.5$	x: 0.3 m $\eta = 1.6$	x: 0 m $\eta = 3.4$	x: 0.3 m $\eta = 36.2$	x: 0.3 m $\eta = 29.3$	x: 0.3 m $\eta = 25.8$	CUMPLE $\eta = 36.2$
N174/N137	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 1.5$	$\eta = 1.8$	x: 0 m $\eta = 0.6$	x: 0 m $\eta = 10.3$	x: 0.3 m $\eta = 5.9$	x: 0.3 m $\eta = 1.9$	x: 0.3 m $\eta = 2.2$	x: 0 m $\eta = 10.5$	x: 0.3 m $\eta = 5.9$	x: 0 m $\eta = 1.1$	x: 0.3 m $\eta = 0.4$	x: 0 m $\eta = 17.5$	x: 0 m $\eta = 15.3$	x: 0 m $\eta = 15.0$	CUMPLE $\eta = 17.5$
N170/N133	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 0.1$	$\eta = 0.1$	$\eta = 0.6$	x: 0.3 m $\eta = 17.9$	x: 0 m $\eta = 13.3$	x: 0.3 m $\eta = 4.4$	x: 0 m $\eta = 5.9$	x: 0.3 m $\eta = 18.1$	x: 0 m $\eta = 13.5$	x: 0.3 m $\eta = 3.6$	x: 0 m $\eta = 2.0$	x: 0.3 m $\eta = 38.9$	x: 0.3 m $\eta = 31.4$	x: 0.3 m $\eta = 27.6$	CUMPLE $\eta = 38.9$
N175/N138	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 1.1$	$\eta = 1.2$	x: 0 m $\eta = 0.2$	x: 0.3 m $\eta = 3.7$	x: 0.3 m $\eta = 25.5$	x: 0 m $\eta = 8.2$	x: 0 m $\eta = 0.6$	x: 0.3 m $\eta = 3.8$	x: 0.3 m $\eta = 25.6$	x: 0.3 m $\eta = 0.1$	x: 0.3 m $\eta = 7.2$	x: 0.3 m $\eta = 37.2$	x: 0.3 m $\eta = 30.1$	x: 0.3 m $\eta = 33.2$	CUMPLE $\eta = 37.2$
N152/N115	$w/t \le (w/t)_{Max}$ Cumple	x: 0.15 m $\eta = 0.1$	x: 0.15 m $\eta = 0.1$	$\eta = 0.4$	x: 0.3 m $\eta = 33.7$	x: 0.3 m $\eta = 16.7$	$\eta = 5.5$	x: 0 m $\eta = 11.2$	x: 0.3 m $\eta = 33.8$	x: 0.3 m $\eta = 16.9$	x: 0.3 m $\eta = 12.7$	x: 0.3 m $\eta = 3.2$	x: 0.3 m $\eta = 63.5$	x: 0.3 m $\eta = 50.4$	x: 0.3 m $\eta = 47.0$	CUMPLE $\eta = 63.5$
N150/N113	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 2.5$	$\eta = 0.2$	$\eta = 0.7$	x: 0.3 m $\eta = 78.3$	x: 0.3 m $\eta = 28.9$	$\eta = 9.5$	x: 0.15 m $\eta = 26.0$	x: 0.3 m $\eta = 78.5$	x: 0.3 m $\eta = 29.2$	x: 0.3 m $\eta = 68.4$	x: 0.3 m $\eta = 9.4$	x: 0.3 m $\eta = 35.5$	x: 0 m $\eta = 5.7$	x: 0.3 m $\eta = 10.4$	CUMPLE $\eta = 35.5$
N149/N112	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 0.4$	$\eta = 1.1$	x: 0.15 m $\eta = 0.9$	x: 0 m $\eta = 15.1$	x: 0 m $\eta = 27.2$	x: 0.15 m $\eta = 9.1$	x: 0.3 m $\eta = 4.8$	x: 0 m $\eta = 15.5$	x: 0 m $\eta = 27.6$	x: 0 m $\eta = 2.6$	x: 0 m $\eta = 8.4$	x: 0 m $\eta = 53.5$	x: 0 m $\eta = 42.6$	x: 0 m $\eta = 38.6$	CUMPLE $\eta = 53.5$
N153/N116	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 1.4$	x: 0 m $\eta = 34.6$	x: 0 m $\eta = 16.7$	$\eta = 5.6$	x: 0 m $\eta = 45.0$	x: 0 m $\eta = 35.2$	x: 0 m $\eta = 17.3$	x: 0 m $\eta = 23.1$	x: 0 m $\eta = 3.3$	x: 0 m $\eta = 90.7$	x: 0 m $\eta = 52.3$	x: 0 m $\eta = 86.3$	CUMPLE $\eta = 86.3$
N147/N110	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	x: 0.15 m $\eta = 0.4$	x: 0.3 m $\eta = 23.0$	x: 0.3 m $\eta = 29.3$	x: 0.15 m $\eta = 12.0$	x: 0.3 m $\eta = 50.6$	x: 0.3 m $\eta = 23.2$	x: 0.3 m $\eta = 29.5$	x: 0.3 m $\eta = 77.3$	x: 0.3 m $\eta = 10.1$	x: 0.3 m $\eta = 90.8$	x: 0.3 m $\eta = 52.5$	x: 0.3 m $\eta = 49.5$	CUMPLE $\eta = 49.5$
N155/N118	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 3.4$	x: 0 m $\eta = 20.5$	x: 0.3 m $\eta = 2.5$	$\eta = 1.0$	x: 0 m $\eta = 49.5$	x: 0 m $\eta = 21.9$	x: 0.3 m $\eta = 4.0$	x: 0 m $\eta = 73.2$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 57.4$	x: 0.3 m $\eta = 25.9$	x: 0 m $\eta = 26.8$	CUMPLE $\eta = 26.8$
N171/N177	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m $\eta = 23.7$	$\eta = 0.6$	x: 1.118 m $\eta = 2.3$	x: 1.118 m $\eta = 4.7$	x: 0.186 m $\eta = 0.6$	x: 0 m $\eta = 0.2$	x: 1.118 m $\eta = 1.5$	x: 1.118 m $\eta = 4.9$	x: 1.118 m $\eta = 0.1$	x: 1.118 m $\eta = 0.2$	N.P.[1]	x: 1.118 m $\eta = 26.1$	x: 1.118 m $\eta = 26.5$	CUMPLE $\eta = 26.5$
N134/N178	$w/t \le (w/t)_{Max}$ Cumple	x: 1.118 m $\eta = 0.9$	x: 0 m $\eta = 24.2$	$\eta = 0.6$	x: 1.118 m $\eta = 2.3$	x: 1.118 m $\eta = 4.6$	x: 0 m $\eta = 0.5$	x: 0 m $\eta = 0.2$	x: 1.118 m $\eta = 2.3$	x: 1.118 m $\eta = 4.8$	x: 1.118 m $\eta = 0.1$	x: 1.118 m $\eta = 0.2$	x: 1.118 m $\eta = 4.1$	x: 1.118 m $\eta = 26.7$	x: 1.118 m $\eta = 27.0$	CUMPLE $\eta = 27.0$
N166/N177	$w/t \le (w/t)_{Max}$ Cumple	x: 1.006 m $\eta = 3.3$	x: 0 m $\eta = 10.7$	x: 0.503 m $\eta = 0.7$	x: 0 m $\eta = 1.8$	x: 1.006 m $\eta = 1.1$	x: 0.335 m $\eta = 0.1$	x: 1.006 m $\eta = 0.2$	x: 1.006 m $\eta = 1.6$	x: 1.006 m $\eta = 1.4$	x: 0 m $\eta < 0.1$	x: 1.006 m $\eta < 0.1$	N.P.[1]	x: 1.006 m $\eta = 13.0$	x: 0 m $\eta = 12.9$	CUMPLE $\eta = 13.0$
N165/N177	$w/t \le (w/t)_{Max}$ Cumple	x: 0.953 m $\eta = 10.4$	x: 0 m $\eta = 9.3$	$\eta = 0.5$	x: 0 m $\eta = 1.7$	x: 0.953 m $\eta = 2.7$	x: 0.715 m $\eta = 0.3$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 1.8$	x: 0.953 m $\eta = 2.8$	x: 0 m $\eta < 0.1$	x: 0.953 m $\eta = 0.1$	N.P.[1]	x: 0 m $\eta = 13.7$	x: 0 m $\eta = 14.2$	CUMPLE $\eta = 14.2$
N129/N178	$w/t \le (w/t)_{Max}$ Cumple	x: 1.006 m $\eta = 1.8$	x: 0 m $\eta = 10.8$	x: 0.335 m $\eta = 0.2$	x: 0 m $\eta = 1.8$	x: 1.006 m $\eta = 3.8$	x: 1.006 m $\eta = 0.3$	x: 1.006 m $\eta = 0.2$	x: 0 m $\eta = 0.9$	x: 1.006 m $\eta = 3.9$	x: 0 m $\eta < 0.1$	x: 1.006 m $\eta = 0.2$	N.P.[1]	x: 0 m $\eta = 12.7$	x: 0 m $\eta = 13.0$	CUMPLE $\eta = 13.0$
N128/N178	$w/t \le (w/t)_{Max}$ Cumple	x: 0.953 m $\eta = 6.1$	x: 0 m $\eta = 2.3$	x: 0.476 m $\eta = 0.2$	x: 0 m $\eta = 0.9$	x: 0.953 m $\eta = 3.3$	$\eta = 0.3$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 0.9$	x: 0.953 m $\eta = 3.4$	x: 0 m $\eta < 0.1$	x: 0.953 m $\eta = 0.1$	N.P.[1]	x: 0.953 m $\eta = 6.2$	x: 0.953 m $\eta = 9.3$	CUMPLE $\eta = 9.3$
N177/N179	$w/t \le (w/t)_{Max}$ Cumple	x: 0.559 m $\eta = 6.0$	x: 0 m $\eta = 28.1$	$\eta = 1.5$	x: 1.119 m $\eta = 2.0$	x: 0 m $\eta = 2.8$	$\eta = 0.3$	x: 0 m $\eta = 0.2$	x: 1.119 m $\eta = 2.1$	x: 0 m $\eta = 3.4$	x: 1.119 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 10.4$	x: 1.119 m $\eta = 30.4$	x: 1.119 m $\eta = 30.6$	CUMPLE $\eta = 30.6$
N179/N180	$w/t \le (w/t)_{Max}$ Cumple	x: 0.748 m $\eta = 0.7$	x: 0 m $\eta = 30.4$	x: 0.935 m $\eta = 2.4$	x: 1.122 m $\eta = 2.1$	x: 0 m $\eta = 3.3$	x: 0.935 m $\eta = 0.5$	x: 0 m $\eta = 0.1$	x: 1.122 m $\eta = 2.2$	x: 0 m $\eta = 4.3$	x: 1.122 m $\eta = 0.1$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 3.8$	x: 1.122 m $\eta = 33.2$	x: 1.122 m $\eta = 33.0$	CUMPLE $\eta = 33.2$
N178/N181	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m $\eta = 28.6$	x: 1.119 m $\eta = 0.8$	x: 1.119 m $\eta = 2.0$	x: 0 m $\eta = 3.0$	$\eta = 0.3$	x: 0 m $\eta = 0.1$	x: 0.932 m $\eta = 1.2$	x: 0 m $\eta = 3.3$	x: 1.119 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	N.P.[1]	x: 1.119 m $\eta = 30.8$	x: 1.119 m $\eta = 31.1$	CUMPLE $\eta = 31.1$
N181/N182	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m $\eta = 30.9$	$\eta = 1.3$	x: 1.122 m $\eta = 2.1$	x: 0 m $\eta = 3.3$	$\eta = 0.4$	x: 0 m $\eta = 0.1$	x: 1.122 m $\eta = 2.1$	x: 0 m $\eta = 3.8$	x: 1.122 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	N.P.[1]	x: 1.122 m $\eta = 33.4$	x: 1.122 m $\eta = 33.5$	CUMPLE $\eta = 33.5$
N177/N178	$w/t \le (w/t)_{Max}$ Cumple	x: 0.3 m $\eta = 1.2$	x: 0.3 m $\eta = 1.4$	x: 0.3 m $\eta = 0.4$	x: 0 m $\eta = 7.1$	x: 0.3 m $\eta = 16.1$	x: 0.3 m $\eta = 5.4$	x: 0.3 m $\eta = 1.5$	x: 0 m $\eta = 7.3$	x: 0.3 m $\eta = 16.2$	x: 0 m $\eta = 0.5$	x: 0.3 m $\eta = 2.9$	x: 0.3 m $\eta = 23.3$	x: 0 m $\eta = 19.0$	x: 0.3 m $\eta = 20.4$	CUMPLE $\eta = 23.3$
N179/N181	$w/t \le (w/t)_{Max}$ Cumple	x: 0.3 m $\eta = 0.5$	x: 0.3 m $\eta = 0.7$	x: 0.15 m $\eta = 0.4$	x: 0.3 m $\eta = 2.9$	x: 0 m $\eta = 11.9$	x: 0 m $\eta = 4.0$	x: 0.3 m $\eta = 0.9$	x: 0.3 m $\eta = 3.1$	x: 0 m $\eta = 11.9$	x: 0.3 m $\eta = 0.1$	x: 0 m $\eta = 1.6$	x: 0.3 m $\eta = 17.7$	x: 0 m $\eta = 14.8$	x: 0 m $\eta = 15.4$	CUMPLE $\eta = 17.7$
N180/N182	$w/t \le (w/t)_{Max}$ Cumple	x: 0 m $\eta = 5.2$	x: 0 m $\eta = 6.3$	$\eta = 0.2$	x: 0 m $\eta = 16.5$	x: 0.3 m $\eta = 17.8$	x: 0.3 m $\eta = 5.9$	x: 0.3 m $\eta = 5.0$	x: 0 m $\eta = 16.6$	x: 0.3 m $\eta = 17.8$	x: 0 m $\eta = 3.0$	x: 0.3 m $\eta = 3.5$	x: 0 m $\eta = 41.0$	x: 0 m $\eta = 36.5$	x: 0 m $\eta = 32.9$	CUMPLE $\eta = 41.0$
N165/N179	$w/t \le (w/t)_{Max}$ Cumple	x: 0.339 m $\eta = 7.5$	x: 0 m $\eta = 13.6$	x: 0.848 m $\eta = 0.6$	x: 0 m $\eta = 1.5$	x: 0 m $\eta = 1.8$	x: 0.17 m $\eta = 0.2$	x: 1.017 m $\eta = 0.1$	x: 1.017 m $\eta = 0.9$	x: 0 m $\eta = 1.8$	x: 0 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.[1]	x: 1.017 m $\eta = 16.3$	x: 0 m $\eta = 16.1$	CUMPLE $\eta = 16.3$
N164/N179	$w/t \le (w/t)_{Max}$ Cumple	x: 0.731 m $\eta = 7.5$	x: 0 m $\eta = 7.5$	$\eta = 0.2$	x: 0 m $\eta = 1.7$	x: 0.974 m $\eta = 2.6$	x: 0.974 m $\eta = 0.3$	x: 0.974 m $\eta = 0.2$	x: 0 m $\eta = 1.7$	x: 0.974 m $\eta = 2.6$	x: 0 m $\eta < 0.1$	x: 0.974 m $\eta = 0.1$	N.P.[1]	x: 0 m $\eta = 11.7$	x: 0.974 m $\eta = 11.1$	CUMPLE $\eta = 11.7$
N164/N180	$w/t \le (w/t)_{Max}$ Cumple	x: 0.17 m $\eta = 6.0$	x: 0.17 m $\eta = 9.1$	$\eta = 0.2$	x: 0 m $\eta = 1.1$	x: 1.021 m $\eta = 2.6$	x: 1.021 m $\eta = 0.2$	x: 1.021 m $\eta = 0.1$	x: 0 m $\eta = 1.1$	x: 1.021 m $\eta = 2.7$	x: 0 m $\eta < 0.1$	x: 1.021 m $\eta = 0.1$	N.P.[1]	x: 1.021 m $\eta = 12.3$	x: 1.021 m $\eta = 12.2$	CUMPLE $\eta = 12.3$
N163/N180	$w/t \le (w/t)_{Max}$ Cumple	x: 0.985 m $\eta = 5.4$	x: 0 m $\eta = 7.2$	x: 0.985 m $\eta = 0.8$	x: 0 m $\eta = 1.3$	x: 0.985 m $\eta = 2.7$	x: 0.985 m $\eta = 0.3$	x: 0.985 m $\eta = 0.2$	x: 0 m $\eta = 1.4$	x: 0.985 m $\eta = 2.7$	x: 0 m $\eta < 0.1$	x: 0.985 m $\eta = 0.1$	N.P.[1]	x: 0 m $\eta = 10.6$	x: 0 m $\eta = 10.2$	CUMPLE $\eta = 10.6$
N126/N181	$w/t \le (w/t)_{Max}$ Cumple	x: 0.678 m $\eta = 3.8$	x: 0.678 m $\eta = 8.4$	x: 1.017 m $\eta = 0.3$	x: 0 m $\eta = 1.5$	x: 1.017 m $\eta = 1.9$	$\eta = 0.2$	x: 1.017 m $\eta = 0.1$	x: 0 m $\eta = 0.9$	x: 1.017 m $\eta = 1.9$	x: 0 m $\eta < 0.1$	x: 1.017 m $\eta < 0.1$	N.P.[1]	x: 0 m $\eta = 10.9$	x: 0 m $\eta = 10.7$	CUMPLE $\eta = 10.9$

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))														Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N127/N181	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.731 m η = 5.4	x: 0 m η = 4.6	η = 0.2	x: 0 m η = 1.0	x: 0.974 m η = 2.7	η = 0.3	x: 0.974 m η = 0.1	x: 0 m η = 1.0	x: 0.974 m η = 2.7	x: 0 m η < 0.1	x: 0.974 m η = 0.1	N.P.(1)	x: 0 m η = 8.1	x: 0.974 m η = 8.6	CUMPLE η = 8.6
N127/N182	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.851 m η = 4.8	x: 0.34 m η = 7.4	x: 0 m η = 0.3	x: 0 m η = 1.1	x: 1.021 m η = 1.6	η = 0.1	x: 1.021 m η = 0.1	x: 0 m η = 1.0	x: 1.021 m η = 1.7	x: 0 m η < 0.1	x: 1.021 m η < 0.1	N.P.(1)	x: 1.021 m η = 9.8	x: 1.021 m η = 9.4	CUMPLE η = 9.8
N126/N182	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.985 m η = 4.8	x: 0 m η = 6.4	x: 0.985 m η = 0.7	x: 0 m η = 1.2	x: 0 m η = 2.0	x: 0.246 m η = 0.2	x: 0.985 m η = 0.1	x: 0 m η = 1.1	x: 0 m η = 2.0	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 9.5	x: 0 m η = 9.2	CUMPLE η = 9.5
N163/N183	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.026 m η = 5.8	x: 0 m η = 5.9	η = 0.4	x: 0.171 m η = 0.7	x: 1.026 m η = 5.3	x: 0.513 m η = 0.5	x: 1.026 m η = 0.1	x: 0.171 m η = 0.7	x: 1.026 m η = 5.4	x: 0.171 m η < 0.1	x: 1.026 m η = 0.3	x: 1.026 m η = 8.0	x: 1.026 m η = 7.2	x: 1.026 m η = 7.6	CUMPLE η = 8.0
N162/N183	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.504 m η = 3.9	x: 0.504 m η = 7.6	η = 0.1	x: 0 m η = 1.3	x: 0 m η = 5.0	x: 0.671 m η = 0.5	x: 1.007 m η = 0.1	x: 0 m η = 1.4	x: 0 m η = 5.0	x: 0 m η < 0.1	x: 0 m η = 0.3	N.P.(1)	x: 1.007 m η = 9.5	x: 1.007 m η = 9.2	CUMPLE η = 9.5
N180/N183	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 30.6	x: 1.12 m η = 1.4	x: 0.373 m η = 1.8	x: 1.12 m η = 6.1	x: 0.933 m η = 0.9	x: 1.12 m η = 0.1	x: 0.747 m η = 1.3	x: 1.12 m η = 6.7	x: 0.373 m η < 0.1	x: 1.12 m η = 0.4	N.P.(1)	x: 0.187 m η = 32.8	x: 0.373 m η = 32.9	CUMPLE η = 32.9
N184/N183	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 28.9	η = 1.6	x: 1.122 m η = 2.1	x: 1.122 m η = 7.8	x: 0.374 m η = 1.2	x: 0 m η = 0.2	x: 1.122 m η = 2.2	x: 1.122 m η = 8.5	x: 1.122 m η < 0.1	x: 1.122 m η = 0.7	N.P.(1)	x: 1.122 m η = 31.5	x: 1.122 m η = 31.5	CUMPLE η = 31.5
N185/N184	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 25.9	x: 0 m η = 0.6	x: 1.131 m η = 1.7	x: 0 m η = 3.7	x: 1.131 m η = 0.3	x: 0 m η = 0.1	x: 1.131 m η = 1.8	x: 0 m η = 3.9	x: 1.131 m η < 0.1	x: 0 m η = 0.2	N.P.(1)	x: 1.131 m η = 28.0	x: 1.131 m η = 28.0	CUMPLE η = 28.0
N186/N185	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.128 m η = 0.7	x: 0 m η = 21.1	x: 1.128 m η = 0.5	x: 1.128 m η = 2.2	x: 1.128 m η = 3.0	η = 0.1	x: 0 m η = 0.2	x: 0.752 m η = 1.1	x: 1.128 m η = 3.2	x: 1.128 m η = 0.1	x: 1.128 m η = 0.1	N.P.(1)	x: 1.128 m η = 23.6	x: 1.128 m η = 23.9	CUMPLE η = 23.9
N187/N186	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.138 m η = 3.9	x: 0 m η = 14.1	x: 1.138 m η = 0.6	x: 1.138 m η = 1.7	x: 0 m η = 12.6	η = 1.9	x: 0 m η = 0.3	x: 1.138 m η = 1.7	x: 0 m η = 12.9	x: 1.138 m η < 0.1	x: 0 m η = 1.7	x: 0 m η = 7.7	x: 0 m η = 16.1	x: 0 m η = 20.5	CUMPLE η = 20.5
N188/N187	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.148 m η = 7.5	x: 0 m η = 11.8	η = 2.9	x: 0 m η = 1.8	x: 1.148 m η = 9.9	x: 0.383 m η = 1.4	x: 0 m η = 0.4	x: 0 m η = 1.9	x: 1.148 m η = 11.1	x: 1.148 m η < 0.1	x: 1.148 m η = 1.3	x: 0 m η = 11.2	x: 1.148 m η = 14.8	x: 1.148 m η = 14.5	CUMPLE η = 14.8
N189/N188	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.129 m η = 11.9	x: 0 m η = 10.4	η = 1.3	x: 0 m η = 1.4	x: 0 m η = 2.3	η = 0.1	x: 0 m η = 0.3	x: 0 m η = 1.5	x: 0 m η = 2.9	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 8.4	x: 0.753 m η = 11.7	x: 0 m η = 13.7	CUMPLE η = 13.7
N190/N189	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.12 m η = 16.3	x: 0 m η = 7.9	x: 0.187 m η = 1.0	x: 0 m η = 9.2	x: 1.12 m η = 4.3	x: 0.187 m η = 0.6	x: 0 m η = 1.0	x: 0 m η = 9.3	x: 1.12 m η = 4.8	x: 0 m η = 0.9	x: 1.12 m η = 0.2	x: 0 m η = 28.5	x: 1.12 m η = 9.5	x: 0 m η = 27.8	CUMPLE η = 28.5
N142/N190	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.902 m η = 21.4	x: 0.451 m η = 6.0	x: 0.451 m η = 6.0	x: 0.902 m η = 8.3	x: 0 m η = 14.6	x: 0.451 m η = 2.1	x: 0.902 m η = 1.6	x: 0.902 m η = 8.3	x: 0 m η = 17.3	x: 0.902 m η = 0.7	x: 0 m η = 3.0	x: 0 m η = 35.1	x: 0 m η = 10.0	x: 0.902 m η = 31.7	CUMPLE η = 35.1
N162/N184	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.034 m η = 5.7	x: 0 m η = 3.7	η = 0.2	x: 0 m η = 0.6	x: 1.034 m η = 2.6	x: 0 m η = 0.1	x: 0 m η = 0.1	x: 0 m η = 0.7	x: 1.034 m η = 2.7	x: 0 m η < 0.1	x: 1.034 m η = 0.1	N.P.(1)	x: 1.034 m η = 5.5	x: 1.034 m η = 7.7	CUMPLE η = 7.7
N161/N184	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.024 m η = 3.2	x: 0 m η = 8.2	x: 0.512 m η = 0.9	x: 0 m η = 1.6	x: 0 m η = 1.4	η = 0.1	x: 1.024 m η = 0.1	x: 1.024 m η = 1.0	x: 0 m η = 1.8	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 9.3	x: 0 m η = 9.5	CUMPLE η = 9.5
N161/N185	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.013 m η = 6.7	x: 0 m η = 2.5	η = 0.3	x: 0 m η = 0.7	x: 0 m η = 1.7	η = 0.1	x: 0 m η = 0.1	x: 0 m η = 0.8	x: 0 m η = 1.9	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 3.2	x: 1.013 m η = 7.5	CUMPLE η = 7.5
N160/N185	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.334 m η = 1.8	x: 0 m η = 12.4	x: 0.167 m η = 0.6	x: 0 m η = 1.9	x: 1.003 m η = 2.5	x: 0.167 m η = 0.2	x: 1.003 m η = 0.2	x: 1.003 m η = 1.1	x: 1.003 m η = 2.8	x: 0 m η < 0.1	x: 1.003 m η = 0.1	N.P.(1)	x: 0 m η = 14.3	x: 0 m η = 14.7	CUMPLE η = 14.7
N160/N186	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.011 m η = 10.6	N.P.(2)	x: 0.169 m η = 0.4	x: 1.011 m η = 1.1	x: 1.011 m η = 3.5	x: 0.169 m η = 0.3	x: 0 m η = 0.1	x: 0 m η = 1.0	x: 1.011 m η = 3.7	x: 1.011 m η < 0.1	x: 1.011 m η = 0.1	N.P.(1)	N.P.(3)	x: 1.011 m η = 12.0	CUMPLE η = 12.0
N159/N186	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.169 m η = 0.9	x: 0 m η = 16.6	η = 0.6	x: 0 m η = 2.2	x: 1.012 m η = 2.1	η = 0.2	x: 1.012 m η = 0.2	x: 1.012 m η = 1.2	x: 1.012 m η = 2.3	x: 0 m η < 0.1	x: 1.012 m η = 0.1	N.P.(1)	x: 0 m η = 18.9	x: 0 m η = 19.3	CUMPLE η = 19.3
N159/N187	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.999 m η = 12.6	N.P.(2)	x: 0 m η = 0.4	x: 0 m η = 1.3	x: 0.999 m η = 7.2	x: 0 m η = 0.7	x: 0 m η = 0.2	x: 0 m η = 1.2	x: 0.999 m η = 7.4	x: 0 m η < 0.1	x: 0.999 m η = 0.6	x: 0 m η = 16.2	N.P.(3)	x: 0.999 m η = 14.8	CUMPLE η = 16.2
N158/N187	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.993 m η = 0.1	x: 0 m η = 20.9	x: 0.993 m η = 0.3	x: 0 m η = 2.3	x: 0 m η = 6.5	x: 0.993 m η = 0.6	x: 0.993 m η = 0.2	x: 0.993 m η = 1.3	x: 0 m η = 6.6	x: 0 m η = 0.1	x: 0 m η = 0.4	N.P.(1)	x: 0 m η = 23.5	x: 0 m η = 23.7	CUMPLE η = 23.7
N158/N188	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.968 m η = 15.1	N.P.(2)	η = 0.3	x: 0 m η = 2.1	x: 0.968 m η = 4.5	η = 0.3	x: 0 m η = 0.2	x: 0 m η = 1.4	x: 0.968 m η = 4.6	x: 0 m η < 0.1	x: 0.968 m η = 0.2	N.P.(1)	N.P.(3)	x: 0 m η = 17.7	CUMPLE η = 17.7
N157/N188	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 25.6	x: 0.941 m η = 1.2	x: 0.941 m η = 1.9	x: 0.941 m η = 0.8	η < 0.1	x: 0.941 m η = 0.2	x: 0.941 m η = 1.4	x: 0.941 m η = 1.3	x: 0.941 m η < 0.1	x: 0.941 m η < 0.1	N.P.(1)	x: 0.941 m η = 27.7	x: 0.941 m η = 28.0	CUMPLE η = 28.0
N157/N189	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.971 m η = 17.8	N.P.(2)	x: 0 m η = 0.4	x: 0 m η = 2.4	x: 0 m η = 2.4	x: 0 m η = 0.1	x: 0 m η = 0.3	x: 0 m η = 1.5	x: 0 m η = 2.6	x: 0 m η = 0.1	x: 0 m η = 0.1	N.P.(1)	N.P.(3)	x: 0 m η = 20.8	CUMPLE η = 20.8
N156/N189	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 29.3	η = 0.1	x: 0 m η = 5.4	x: 0.947 m η = 1.7	x: 0.237 m η = 0.2	x: 0.947 m η = 0.6	x: 0.947 m η = 2.6	x: 0.947 m η = 1.8	x: 0 m η = 0.3	x: 0.947 m η < 0.1	N.P.(1)	x: 0 m η = 35.4	x: 0 m η = 36.0	CUMPLE η = 36.0
N156/N190	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.981 m η = 16.2	N.P.(2)	η = 0.1	x: 0 m η = 4.0	x: 0 m η = 1.5	η < 0.1	x: 0 m η = 0.2	x: 0 m η = 1.9	x: 0 m η = 1.5	x: 0 m η = 0.2	x: 0 m η < 0.1	N.P.(3)	N.P.(3)	x: 0 m η = 21.2	CUMPLE η = 21.2
N144/N190	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 29.4	x: 0.402 m η = 2.2	x: 0 m η = 3.9	x: 0 m η = 14.7	η = 1.4	x: 0.804 m η = 0.5	x: 0 m η = 3.9	x: 0 m η = 15.6	x: 0 m η = 0.2	x: 0 m η = 2.5	N.P.(1)	x: 0.804 m η = 32.8	x: 0.804 m η = 33.2	CUMPLE η = 33.2
N126/N191	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.026 m η = 5.7	x: 0 m η = 5.6	η = 0.5	x: 0 m η = 0.7	x: 0 m η = 4.0	x: 0.513 m η = 0.4	x: 1.026 m η = 0.1	x: 0 m η = 0.7	x: 0 m η = 4.3	x: 0 m η < 0.1	x: 0 m η = 0.2	N.P.(1)	x: 0 m η = 7.7	x: 0 m η = 7.5	CUMPLE η = 7.7
N125/N191	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.336 m η = 3.6	x: 0.336 m η = 7.4	η = 0.2	x: 0 m η = 1.4	x: 0 m η = 4.6	η = 0.4	x: 1.007 m η = 0.1	x: 0 m η = 1.1	x: 0 m η = 4.7	x: 0 m η < 0.1	x: 0 m η = 0.2	N.P.(1)	x: 0 m η = 9.6	x: 0 m η = 9.9	CUMPLE η = 9.9
N125/N192	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.034 m η = 5.6	x: 0 m η = 3.4	x: 0.862 m η = 0.5	x: 0 m η = 0.6	x: 1.034 m η = 1.3	x: 0.172 m η = 0.1	x: 0 m η = 0.1	x: 0 m η = 0.7	x: 1.034 m η = 1.3	x: 0 m η < 0.1	x: 1.034 m η < 0.1	N.P.(1)	x: 1.034 m η = 5.1	x: 1.034 m η = 7.1	CUMPLE η = 7.1
N182/N191	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 31.8	x: 0.187 m η = 0.5	x: 0.373 m η = 1.8	x: 1.12 m η = 6.3	x: 0.933 m η = 0.9	x: 1.12 m η = 0.1	x: 0.373 m η = 1.2	x: 1.12 m η = 6.4	x: 0.373 m η < 0.1	x: 1.12 m η = 0.4	N.P.(1)	x: 0.187 m η = 34.0	x: 0.373 m η = 34.1	CUMPLE η = 34.1
N192/N191	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 29.4	η = 1.0	x: 1.122 m η = 2.1	x: 1.122 m η = 7.9	η = 1.2	x: 0 m η = 0.2	x: 1.122 m η = 2.1	x: 1.122 m η = 8.4	x: 1.122 m η < 0.1	x: 1.122 m η = 0.7	N.P.(1)	x: 1.122 m η = 31.8	x: 1.122 m η = 32.1	CUMPLE η = 32.1
N124/N192	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.341 m η = 3.1	x: 0.341 m η = 8.0	x: 1.024 m η = 0.5	x: 0 m η = 1.6	x: 1.024 m η = 2.0	x: 1.024 m η = 0.1	x: 1.024 m η = 0.1	x: 0 m η = 1.1	x: 1.024 m η = 2.3	x: 0 m η < 0.1	x: 1.024 m η = 0.1	N.P.(1)	x: 0 m η = 9.1	x: 0 m η = 9.2	CUMPLE η = 9.2
N193/N192	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 26.4	x: 0.566 m η = 1.3	x: 1.131 m η = 1.7	x: 0 m η = 3.7	η = 0.3	x: 0 m η = 0.1	x: 1.131 m η = 1.7	x: 0 m η = 4.2	x: 1.131 m η < 0.1	x: 0 m η = 0.2	N.P.(1)	x: 1.131 m η = 28.2	x: 1.131 m η = 28.5	CUMPLE η = 28.5
N124/N193	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.013 m η = 6.7	x: 0 m η = 2.3	x: 0.169 m η = 0.2	x: 0 m η = 0.7	x: 0 m η = 1.9	x: 0.169 m η = 0.2	x: 0 m η = 0.1	x: 0 m η = 0.8	x: 0 m η = 2.0	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 3.2	x: 1.013 m η = 7.7	CUMPLE η = 7.7
N123/N193	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.167 m η = 1.4	x: 0 m η = 12.5	x: 1.003 m η = 0.5	x: 0 m η = 1.9	x: 1.003 m η = 3.3	x: 1.003 m η = 0.3	x: 1.003 m η = 0.2	x: 0 m η = 1.1	x: 1.003 m η = 3.5	x: 0 m η < 0.1	x: 1.003 m η = 0.1	N.P.(1)	x: 0 m η = 14.6	x: 0 m η = 14.9	CUMPLE η = 14.9
N123/N194	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.011 m η = 10.6	N.P.(2)	x: 0.169 m η = 1.1	x: 1.011 m η = 1.1	x: 1.011 m η = 1.3	η = 0.1	x: 0 m η = 0.1	x: 0 m η = 1.1	x: 1.011 m η = 1.7	x: 1.011 m η < 0.1	x: 1.011 m η < 0.1	N.P.(1)	N.P.(3)	x: 1.011 m η = 12.1	CUMPLE η = 12.1

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_z	M_y	V_x	V_y	M_zTr	M_yTr	M_zV_y	M_yV_x	MT	MP	TPTrMV	
N194/N193	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.128 m η = 0.8	x: 0 m η = 21.5	η = 1.9	x: 1.128 m η = 2.3	x: 1.128 m η = 2.9	η = 0.1	x: 0 m η = 0.2	x: 1.128 m η = 2.3	x: 1.128 m η = 3.7	x: 1.128 m η = 0.1	x: 1.128 m η = 0.1	N.P.[1]	x: 1.128 m η = 24.1	x: 1.128 m η = 24.3	CUMPLE η = 24.3
N122/N194	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.169 m η = 0.5	x: 0 m η = 16.6	η = 0.1	x: 0 m η = 2.2	x: 1.012 m η = 2.7	η = 0.2	x: 1.012 m η = 0.2	x: 1.012 m η = 1.1	x: 1.012 m η = 2.8	x: 0 m η < 0.1	x: 1.012 m η = 0.1	N.P.[1]	x: 0 m η = 19.2	x: 0 m η = 19.4	CUMPLE η = 19.4
N195/N194	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.138 m η = 3.9	x: 0 m η = 14.6	η = 1.3	x: 1.138 m η = 1.7	x: 0 m η = 12.5	x: 0.569 m η = 1.9	x: 0 m η = 0.3	x: 1.138 m η = 1.7	x: 0 m η = 13.1	x: 1.138 m η < 0.1	x: 0 m η = 1.8	x: 0 m η = 7.2	x: 0 m η = 20.4	x: 0 m η = 22.0	CUMPLE η = 22.0
N122/N195	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.999 m η = 12.6	N.P.[2]	η = 0.3	x: 0 m η = 1.3	x: 0.999 m η = 7.5	x: 0.25 m η = 0.7	x: 0 m η = 0.2	x: 0 m η = 1.2	x: 0.999 m η = 7.6	x: 0 m η < 0.1	x: 0.999 m η = 0.6	x: 0.999 m η = 16.9	N.P.[3]	x: 0.999 m η = 15.6	CUMPLE η = 16.9
N121/N195	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.993 m η = 0.1	x: 0 m η = 21.0	x: 0.745 m η = 0.3	x: 0 m η = 2.3	x: 0 m η = 6.9	x: 0.745 m η = 0.7	x: 0.993 m η = 0.2	x: 0.993 m η = 1.2	x: 0 m η = 7.0	x: 0 m η = 0.1	x: 0 m η = 0.5	N.P.[1]	x: 0 m η = 23.6	x: 0 m η = 23.9	CUMPLE η = 23.9
N121/N196	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.968 m η = 15.1	x: 0.242 m η = 0.2	x: 0.242 m η = 1.0	x: 0 m η = 2.0	x: 0 m η = 1.4	η = 0.1	x: 0 m η = 0.2	x: 0 m η = 1.6	x: 0 m η = 1.8	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 2.5	x: 0 m η = 17.7	CUMPLE η = 17.7
N196/N195	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.957 m η = 7.8	x: 0 m η = 12.4	x: 0.766 m η = 0.9	x: 0 m η = 1.8	x: 1.148 m η = 10.0	η = 1.4	x: 0 m η = 0.4	x: 0 m η = 1.9	x: 1.148 m η = 10.4	x: 0 m η < 0.1	x: 1.148 m η = 1.1	x: 0 m η = 11.7	x: 1.148 m η = 15.6	x: 1.148 m η = 15.4	CUMPLE η = 15.6
N120/N196	$w/t \leq (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m η = 25.8	x: 0.706 m η = 0.4	x: 0.941 m η = 2.0	x: 0.941 m η = 5.1	x: 0.706 m η = 0.3	x: 0.941 m η = 0.2	x: 0.941 m η = 1.3	x: 0.941 m η = 5.3	x: 0.941 m η < 0.1	x: 0.941 m η = 0.3	N.P.[1]	x: 0.941 m η = 28.2	x: 0.941 m η = 28.2	CUMPLE η = 28.2
N197/N196	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.129 m η = 11.9	x: 0 m η = 10.5	x: 0 m η = 1.4	x: 0 m η = 1.4	x: 0 m η = 2.4	x: 0 m η = 0.1	x: 0 m η = 0.3	x: 0 m η = 1.5	x: 0 m η = 3.0	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 9.4	x: 0.941 m η = 11.9	x: 0 m η = 13.5	CUMPLE η = 13.5
N120/N197	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.971 m η = 17.9	N.P.[2]	x: 0.728 m η = 0.4	x: 0 m η = 2.4	x: 0.971 m η = 4.1	x: 0.243 m η = 0.4	x: 0 m η = 0.3	x: 0 m η = 1.6	x: 0.971 m η = 4.2	x: 0 m η = 0.1	x: 0.971 m η = 0.2	N.P.[1]	N.P.[3]	x: 0 m η = 20.8	CUMPLE η = 20.8
N119/N197	$w/t \leq (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m η = 29.3	η = 0.8	x: 0 m η = 5.4	x: 0.947 m η = 6.0	x: 0.71 m η = 0.5	x: 0.947 m η = 0.6	x: 0 m η = 2.7	x: 0.947 m η = 6.3	x: 0 m η = 0.3	x: 0.947 m η = 0.4	N.P.[1]	x: 0 m η = 35.5	x: 0 m η = 36.1	CUMPLE η = 36.1
N198/N197	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.12 m η = 16.1	x: 0 m η = 7.9	η = 0.1	x: 0 m η = 9.3	x: 1.12 m η = 4.7	x: 0.187 m η = 0.6	x: 0 m η = 1.1	x: 0 m η = 9.3	x: 1.12 m η = 4.7	x: 0 m η = 0.9	x: 1.12 m η = 0.2	x: 0 m η = 28.4	x: 0.56 m η = 9.3	x: 0 m η = 27.5	CUMPLE η = 28.4
N119/N198	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.981 m η = 16.2	N.P.[2]	η = 0.4	x: 0 m η = 4.0	x: 0.981 m η = 2.6	η = 0.1	x: 0 m η = 0.2	x: 0 m η = 2.1	x: 0.981 m η = 2.7	x: 0 m η = 0.2	x: 0.981 m η = 0.1	N.P.[1]	N.P.[3]	x: 0 m η = 21.1	CUMPLE η = 21.1
N106/N198	$w/t \leq (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m η = 29.2	η = 2.2	x: 0 m η = 4.0	x: 0 m η = 13.8	η = 1.2	x: 0.804 m η = 0.5	x: 0 m η = 4.2	x: 0 m η = 14.7	x: 0 m η = 0.2	x: 0 m η = 2.2	N.P.[1]	x: 0 m η = 33.2	x: 0.804 m η = 33.0	CUMPLE η = 33.2
N105/N198	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.902 m η = 21.1	x: 0 m η = 6.1	x: 0.677 m η = 5.3	x: 0.902 m η = 8.4	x: 0 m η = 15.6	x: 0.902 m η = 2.3	x: 0.902 m η = 1.7	x: 0.902 m η = 8.5	x: 0 m η = 18.0	x: 0.902 m η = 0.7	x: 0 m η = 3.3	x: 0 m η = 44.0	x: 0 m η = 20.6	x: 0 m η = 33.5	CUMPLE η = 44.0
N183/N191	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.15 m η = 1.8	x: 0.15 m η = 2.4	η = 0.3	x: 0.3 m η = 7.7	x: 0 m η = 16.0	x: 0 m η = 5.4	x: 0.3 m η = 2.3	x: 0.3 m η = 7.8	x: 0 m η = 16.0	x: 0.3 m η = 0.7	x: 0 m η = 2.8	x: 0.3 m η = 22.6	x: 0.3 m η = 18.3	x: 0.3 m η = 21.2	CUMPLE η = 22.6
N184/N192	$w/t \leq (w/t)_{Max}$ Cumple	x: 0 m η = 1.3	x: 0 m η = 1.5	x: 0 m η = 0.4	x: 0.3 m η = 3.1	x: 0 m η = 20.3	x: 0.3 m η = 6.7	x: 0.3 m η = 0.3	x: 0.3 m η = 3.3	x: 0 m η = 20.5	x: 0.3 m η = 0.1	x: 0 m η = 4.6	x: 0.3 m η = 29.9	x: 0 m η = 24.7	x: 0 m η = 27.0	CUMPLE η = 29.9
N185/N193	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.15 m η = 0.7	x: 0.15 m η = 0.7	η = 0.3	x: 0 m η = 4.7	x: 0.3 m η = 3.3	x: 0 m η = 1.1	x: 0.3 m η = 1.4	x: 0 m η = 4.9	x: 0.3 m η = 3.3	x: 0 m η = 0.3	x: 0.3 m η = 0.1	N.P.[1]	x: 0 m η = 8.4	x: 0 m η = 7.5	CUMPLE η = 8.4
N186/N194	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.15 m η = 2.9	x: 0.15 m η = 3.3	η = 0.2	x: 0.3 m η = 14.7	x: 0 m η = 25.1	x: 0.3 m η = 8.1	x: 0.3 m η = 3.4	x: 0.3 m η = 14.8	x: 0 m η = 25.2	x: 0.3 m η = 2.3	x: 0 m η = 7.0	x: 0.3 m η = 50.5	x: 0.3 m η = 41.0	x: 0.3 m η = 37.2	CUMPLE η = 50.5
N187/N195	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.15 m η = 1.6	x: 0.15 m η = 2.1	η = 0.3	x: 0 m η = 4.7	x: 0 m η = 12.4	x: 0.3 m η = 4.1	x: 0.3 m η = 1.4	x: 0 m η = 4.9	x: 0 m η = 12.5	x: 0 m η = 0.3	x: 0 m η = 1.7	x: 0 m η = 23.3	x: 0 m η = 18.6	x: 0 m η = 18.1	CUMPLE η = 23.3
N188/N196	$w/t \leq (w/t)_{Max}$ Cumple	η = 2.2	η = 2.3	η = 0.6	x: 0.3 m η = 6.1	x: 0 m η = 14.3	η = 4.3	x: 0.3 m η = 0.7	x: 0.3 m η = 6.3	x: 0 m η = 14.6	x: 0.3 m η = 0.4	x: 0 m η = 2.3	x: 0.3 m η = 24.6	x: 0.3 m η = 20.1	x: 0 m η = 20.4	CUMPLE η = 24.6
N189/N197	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.3 m η = 1.7	x: 0.3 m η = 2.0	η = 0.7	x: 0 m η = 9.9	x: 0.3 m η = 8.8	x: 0 m η = 2.4	x: 0.3 m η = 2.0	x: 0 m η = 10.2	x: 0.3 m η = 9.1	x: 0 m η = 1.1	x: 0.3 m η = 0.9	x: 0 m η = 21.0	x: 0 m η = 18.1	x: 0 m η = 16.2	CUMPLE η = 21.0
N190/N198	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.15 m η = 0.7	x: 0.15 m η = 0.7	x: 0 m η = 0.2	x: 0.3 m η = 8.2	x: 0.3 m η = 30.4	x: 0.15 m η = 9.9	x: 0 m η = 2.1	x: 0.3 m η = 8.3	x: 0.3 m η = 30.5	x: 0.3 m η = 0.7	x: 0.3 m η = 10.3	x: 0.3 m η = 48.2	x: 0.3 m η = 38.9	x: 0.3 m η = 39.8	CUMPLE η = 48.2
N113/N207	$w/t \leq (w/t)_{Max}$ Cumple	η = 11.2	η = 12.4	x: 0.315 m η = 1.1	x: 0 m η = 7.2	x: 0 m η = 2.2	x: 0.315 m η = 0.2	x: 0 m η = 0.8	x: 0 m η = 7.7	x: 0 m η = 2.7	x: 0 m η = 0.6	x: 0 m η = 0.1	x: 0 m η = 24.2	x: 0 m η = 20.5	x: 0 m η = 20.6	CUMPLE η = 24.2
N207/N208	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.315 m η = 7.0	x: 0.315 m η = 8.1	η = 0.2	x: 0 m η = 1.3	x: 0 m η = 1.4	η = 0.1	x: 0 m η = 0.2	x: 0 m η = 1.4	x: 0 m η = 1.4	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 10.5	x: 0 m η = 10.1	CUMPLE η = 10.5
N208/N209	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.315 m η = 3.2	x: 0.315 m η = 4.0	η = 0.4	x: 0 m η = 1.1	x: 0.63 m η = 1.3	η < 0.1	x: 0 m η = 0.2	x: 0 m η = 1.2	x: 0.63 m η = 1.5	x: 0 m η < 0.1	x: 0.63 m η < 0.1	N.P.[1]	x: 0 m η = 5.8	x: 0 m η = 5.3	CUMPLE η = 5.8
N209/N210	$w/t \leq (w/t)_{Max}$ Cumple	η = 0.2	η = 0.8	x: 0.63 m η = 0.4	x: 0.63 m η = 1.2	x: 0.63 m η = 1.0	η < 0.1	x: 0 m η = 0.2	x: 0.63 m η = 1.4	x: 0.63 m η = 1.2	x: 0.63 m η < 0.1	x: 0.63 m η < 0.1	N.P.[1]	x: 0.63 m η = 3.3	x: 0.63 m η = 2.7	CUMPLE η = 3.3
N210/N211	$w/t \leq (w/t)_{Max}$ Cumple	x: 0 m η = 3.8	x: 0 m η = 5.2	η = 0.5	x: 0.63 m η = 1.2	x: 0.63 m η = 1.1	η < 0.1	x: 0.63 m η = 0.2	x: 0.63 m η = 1.4	x: 0.63 m η = 1.3	x: 0.63 m η < 0.1	x: 0.63 m η < 0.1	N.P.[1]	x: 0.63 m η = 7.3	x: 0.63 m η = 6.8	CUMPLE η = 7.3
N211/N212	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.315 m η = 7.5	x: 0.315 m η = 9.5	η = 0.5	x: 0.63 m η = 1.2	x: 0 m η = 1.4	η < 0.1	x: 0.63 m η = 0.2	x: 0.63 m η = 1.4	x: 0 m η = 1.6	x: 0.63 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0.63 m η = 11.6	x: 0.63 m η = 11.1	CUMPLE η = 11.6
N212/N213	$w/t \leq (w/t)_{Max}$ Cumple	η = 11.2	η = 13.8	η = 0.5	x: 0.63 m η = 2.3	x: 0 m η = 1.5	η = 0.1	x: 0.63 m η = 0.3	x: 0.63 m η = 2.5	x: 0 m η = 1.8	x: 0.63 m η = 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0.63 m η = 17.8	x: 0.63 m η = 16.9	CUMPLE η = 17.8
N213/N214	$w/t \leq (w/t)_{Max}$ Cumple	η = 15.1	η = 18.2	x: 0 m η = 0.3	x: 0.63 m η = 0.9	x: 0.63 m η = 1.7	x: 0 m η = 0.1	x: 0 m η = 0.1	x: 0.63 m η = 1.0	x: 0.63 m η = 1.8	x: 0.63 m η < 0.1	x: 0.63 m η < 0.1	N.P.[1]	x: 0.63 m η = 21.0	x: 0.63 m η = 20.5	CUMPLE η = 21.0
N214/N53	$w/t \leq (w/t)_{Max}$ Cumple	x: 0 m η = 17.9	x: 0 m η = 20.2	x: 0 m η = 1.3	x: 0.49 m η = 7.1	x: 0.49 m η = 4.0	x: 0 m η = 0.4	x: 0.49 m η = 0.7	x: 0.49 m η = 7.7	x: 0.49 m η = 4.5	x: 0.49 m η = 0.6	x: 0.49 m η = 0.2	x: 0.49 m η = 33.1	x: 0.49 m η = 28.5	x: 0.49 m η = 28.0	CUMPLE η = 33.1
N112/N206	$w/t \leq (w/t)_{Max}$ Cumple	η = 10.5	η = 12.5	η = 2.3	x: 0 m η = 39.2	x: 0 m η = 14.9	η = 1.4	x: 0.49 m η = 5.5	x: 0 m η = 39.7	x: 0 m η = 15.5	x: 0 m η = 16.1	x: 0 m η = 2.4	x: 0 m η = 79.4	x: 0 m η = 64.5	x: 0 m η = 62.8	CUMPLE η = 79.4
N206/N205	$w/t \leq (w/t)_{Max}$ Cumple	η = 8.0	η = 9.4	η = 0.1	x: 0 m η = 5.2	x: 0 m η = 3.1	η = 0.2	x: 0 m η = 0.6	x: 0 m η = 5.2	x: 0 m η = 3.1	x: 0 m η = 0.3	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 15.1	x: 0 m η = 15.6	CUMPLE η = 15.6
N205/N204	$w/t \leq (w/t)_{Max}$ Cumple	η = 4.5	η = 4.7	η = 0.4	x: 0 m η = 1.9	x: 0 m η = 1.9	η = 0.2	x: 0 m η = 0.3	x: 0 m η = 2.1	x: 0 m η = 2.1	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 8.7	x: 0 m η = 8.0	CUMPLE η = 8.7
N204/N203	$w/t \leq (w/t)_{Max}$ Cumple	η = 1.2	η = 0.2	η = 0.4	x: 0.63 m η = 1.0	x: 0 m η = 1.6	η = 0.1	x: 0 m η = 0.2	x: 0.63 m η = 1.2	x: 0 m η = 1.8	x: 0.63 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 2.9	x: 0.63 m η = 2.8	CUMPLE η = 2.9
N203/N202	$w/t \leq (w/t)_{Max}$ Cumple	η = 3.8	η = 3.1	η = 0.5	x: 0.63 m η = 1.2	x: 0.63 m η = 1.6	η = 0.1	x: 0 m η = 0.2	x: 0.63 m η = 1.4	x: 0.63 m η = 1.8	x: 0.63 m η < 0.1	x: 0.63 m η < 0.1	N.P.[1]	x: 0.63 m η = 5.9	x: 0 m η = 5.8	CUMPLE η = 5.9
N202/N201	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.315 m η = 7.5	x: 0.315 m η = 7.4	x: 0 m η = 0.5	x: 0.63 m η = 1.1	x: 0.63 m η = 1.8	η = 0.1	x: 0.63 m η = 0.2	x: 0.63 m η = 1.3	x: 0.63 m η = 2.0	x: 0.63 m η < 0.1	x: 0.63 m η < 0.1	N.P.[1]	x: 0.63 m η = 10.6	x: 0.63 m η = 9.9	CUMPLE η = 10.6

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N201/N200	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.315 m η = 11.2	x: 0.315 m η = 11.8	η = 0.5	x: 0.63 m η = 1.6	x: 0.63 m η = 1.9	η = 0.2	x: 0.63 m η = 0.2	x: 0.63 m η = 1.9	x: 0.63 m η = 2.1	x: 0.63 m η < 0.1	x: 0.63 m η < 0.1	N.P.[1]	x: 0.63 m η = 15.7	x: 0.63 m η = 14.9	CUMPLE η = 15.7
N200/N199	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.158 m η = 14.7	x: 0.158 m η = 16.1	η = 0.4	x: 0.63 m η = 2.4	x: 0.63 m η = 2.6	η = 0.1	x: 0.63 m η = 0.3	x: 0.63 m η = 2.5	x: 0.63 m η = 2.7	x: 0.63 m η = 0.1	x: 0.63 m η = 0.1	N.P.[1]	x: 0.63 m η = 20.3	x: 0.63 m η = 19.4	CUMPLE η = 20.3
N199/N52	$w/t \leq (w/t)_{Max}$ Cumple	η = 18.4	η = 20.8	η = 0.8	x: 0.63 m η = 28.1	x: 0.63 m η = 10.9	η = 0.7	x: 0.63 m η = 3.1	x: 0.63 m η = 28.5	x: 0.63 m η = 11.2	x: 0.63 m η = 8.2	x: 0.63 m η = 1.3	x: 0.63 m η = 66.9	x: 0.63 m η = 59.1	x: 0.63 m η = 57.1	CUMPLE η = 66.9
N52/N214	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 3.8	x: 0 m η = 5.8	x: 0.697 m η = 1.7	x: 0 m η = 17.2	x: 0 m η = 9.2	η = 0.6	x: 0.929 m η = 1.3	x: 0 m η = 17.6	x: 0 m η = 9.9	x: 0 m η = 3.1	x: 0 m η = 1.0	x: 0 m η = 38.2	x: 0 m η = 32.2	x: 0 m η = 29.7	CUMPLE η = 38.2
N199/N214	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 4.1	x: 0 m η = 4.7	η = 0.5	x: 0 m η = 3.9	x: 0 m η = 4.2	x: 0.602 m η = 0.5	x: 0 m η = 0.5	x: 0 m η = 3.9	x: 0 m η = 4.3	x: 0 m η = 0.2	x: 0 m η = 0.2	N.P.[1]	x: 0 m η = 12.7	x: 0 m η = 11.5	CUMPLE η = 12.7
N199/N213	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 5.4	x: 0 m η = 7.8	x: 0.465 m η = 0.5	x: 0 m η = 2.9	x: 0 m η = 0.2	η < 0.1	x: 0.929 m η = 0.3	x: 0 m η = 3.1	x: 0.929 m η = 0.4	x: 0 m η = 0.1	x: 0.929 m η < 0.1	N.P.[1]	x: 0 m η = 11.0	x: 0 m η = 11.2	CUMPLE η = 11.2
N200/N213	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 4.8	x: 0 m η = 5.8	x: 0.802 m η = 0.6	x: 0.802 m η = 0.4	x: 0 m η = 0.8	η < 0.1	x: 0.802 m η < 0.1	x: 0.802 m η = 0.7	x: 0 m η = 1.1	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 7.2	x: 0 m η = 6.7	CUMPLE η = 7.2
N200/N212	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.697 m η = 5.2	x: 0 m η = 7.3	η = 0.3	x: 0.929 m η = 0.9	x: 0 m η = 0.1	η < 0.1	x: 0.929 m η = 0.1	x: 0.929 m η = 1.1	x: 0 m η = 0.3	x: 0.929 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0.929 m η = 8.5	x: 0.929 m η = 8.4	CUMPLE η = 8.5
N201/N212	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 4.6	x: 0 m η = 5.8	x: 0.401 m η = 0.7	x: 0.802 m η = 1.2	x: 0 m η = 1.2	η = 0.1	x: 0.802 m η = 0.1	x: 0.802 m η = 1.5	x: 0 m η = 1.4	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 8.1	x: 0 m η = 7.4	CUMPLE η = 8.1
N201/N211	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 5.4	x: 0 m η = 7.2	η = 0.2	x: 0.929 m η = 0.9	x: 0 m η = 0.5	η < 0.1	x: 0 m η = 0.1	x: 0.929 m η = 1.0	x: 0 m η = 0.6	x: 0.929 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0.929 m η = 8.4	x: 0.929 m η = 8.3	CUMPLE η = 8.4
N202/N211	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 4.6	x: 0 m η = 5.9	η = 0.6	x: 0.802 m η = 1.1	x: 0 m η = 1.0	η = 0.1	x: 0.802 m η = 0.1	x: 0.802 m η = 1.3	x: 0 m η = 1.2	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 7.9	x: 0 m η = 7.4	CUMPLE η = 7.9
N202/N210	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 5.4	x: 0 m η = 7.1	x: 0.929 m η = 0.4	x: 0.929 m η = 0.9	x: 0 m η = 0.6	η < 0.1	x: 0 m η = 0.1	x: 0.929 m η = 1.0	x: 0 m η = 0.8	x: 0.929 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 8.0	x: 0.929 m η = 8.1	CUMPLE η = 8.1
N203/N210	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 4.5	x: 0 m η = 6.0	η = 0.5	x: 0.802 m η = 1.1	x: 0 m η = 0.9	η = 0.1	x: 0.802 m η = 0.1	x: 0.802 m η = 1.3	x: 0 m η = 1.1	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 7.8	x: 0.802 m η = 7.5	CUMPLE η = 7.8
N203/N209	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 5.5	x: 0 m η = 7.0	η = 0.5	x: 0.929 m η = 0.8	x: 0 m η = 0.7	η < 0.1	x: 0 m η = 0.1	x: 0.929 m η = 1.0	x: 0 m η = 0.9	x: 0.929 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 8.1	x: 0.929 m η = 7.9	CUMPLE η = 8.1
N204/N209	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 4.4	x: 0 m η = 6.1	η = 0.3	x: 0.802 m η = 1.1	x: 0 m η = 0.9	η = 0.1	x: 0.802 m η = 0.1	x: 0.802 m η = 1.3	x: 0 m η = 1.1	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 8.0	x: 0.802 m η = 7.7	CUMPLE η = 8.0
N204/N208	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 5.6	x: 0 m η = 6.8	x: 0.465 m η = 0.5	x: 0 m η = 0.8	x: 0 m η = 0.8	η < 0.1	x: 0 m η = 0.1	x: 0 m η = 1.1	x: 0 m η = 1.1	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 8.5	x: 0 m η = 8.1	CUMPLE η = 8.5
N205/N208	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 4.3	x: 0 m η = 6.2	x: 0 m η = 0.1	x: 0.802 m η = 1.0	x: 0 m η = 0.4	η = 0.1	x: 0.802 m η = 0.1	x: 0.802 m η = 1.0	x: 0 m η = 0.5	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0.802 m η = 7.6	x: 0.802 m η = 7.5	CUMPLE η = 7.6
N205/N207	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 5.9	x: 0 m η = 7.1	x: 0.697 m η = 0.7	x: 0 m η = 0.3	x: 0 m η = 0.8	η = 0.1	x: 0 m η = 0.1	x: 0.929 m η = 0.5	x: 0 m η = 1.1	x: 0.929 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 8.5	x: 0 m η = 8.1	CUMPLE η = 8.5
N206/N207	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 4.3	x: 0 m η = 6.4	η = 0.6	x: 0 m η = 5.0	x: 0 m η = 3.3	x: 0.401 m η = 0.3	x: 0 m η = 0.5	x: 0 m η = 5.3	x: 0 m η = 3.6	x: 0 m η = 0.3	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 14.4	x: 0 m η = 13.5	CUMPLE η = 14.4
N206/N113	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 4.0	x: 0 m η = 4.0	η = 0.5	x: 0 m η = 3.1	x: 0.929 m η = 3.6	η = 0.3	x: 0.929 m η = 0.1	x: 0 m η = 3.2	x: 0.929 m η = 3.8	x: 0 m η = 0.1	x: 0.929 m η = 0.1	N.P.[1]	x: 0 m η = 9.1	x: 0.929 m η = 9.5	CUMPLE η = 9.5
N105/N215	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.315 m η = 10.8	x: 0.315 m η = 11.8	x: 0.473 m η = 1.3	x: 0 m η = 8.1	x: 0 m η = 17.6	x: 0.315 m η = 0.9	x: 0 m η = 0.9	x: 0 m η = 8.6	x: 0 m η = 17.8	x: 0 m η = 0.8	x: 0 m η = 3.2	x: 0 m η = 29.1	x: 0 m η = 21.2	x: 0 m η = 24.1	CUMPLE η = 29.1
N215/N216	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.63 m η = 6.6	x: 0.63 m η = 7.5	x: 0.63 m η = 0.5	x: 0 m η = 1.3	x: 0 m η = 7.6	η = 0.9	x: 0 m η = 0.2	x: 0 m η = 1.4	x: 0 m η = 7.8	x: 0 m η < 0.1	x: 0 m η = 0.6	x: 0 m η = 11.9	x: 0.63 m η = 9.8	x: 0 m η = 10.1	CUMPLE η = 11.9
N216/N217	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.473 m η = 2.7	x: 0.473 m η = 3.4	x: 0.158 m η = 0.5	x: 0 m η = 1.1	x: 0.63 m η = 6.9	η = 0.4	x: 0 m η = 0.2	x: 0 m η = 1.3	x: 0.63 m η = 7.0	x: 0 m η < 0.1	x: 0.63 m η = 0.5	x: 0.63 m η = 10.3	x: 0.63 m η = 7.6	x: 0.63 m η = 8.8	CUMPLE η = 10.3
N217/N218	$w/t \leq (w/t)_{Max}$ Cumple	η = 0.7	η = 1.4	x: 0.158 m η = 0.5	x: 0.63 m η = 1.5	x: 0.63 m η = 10.1	η = 0.4	x: 0 m η = 0.2	x: 0.63 m η = 1.6	x: 0.63 m η = 10.3	x: 0.63 m η < 0.1	x: 0.63 m η = 1.1	N.P.[1]	x: 0.63 m η = 12.2	x: 0.63 m η = 13.0	CUMPLE η = 13.0
N218/N219	$w/t \leq (w/t)_{Max}$ Cumple	η = 4.3	η = 5.9	η = 0.8	x: 0.63 m η = 1.3	x: 0 m η = 8.9	η < 0.1	x: 0.63 m η = 0.2	x: 0.158 m η = 1.6	x: 0 m η = 9.2	x: 0.158 m η < 0.1	x: 0 m η = 0.9	N.P.[1]	x: 0 m η = 11.1	x: 0 m η = 11.5	CUMPLE η = 11.5
N219/N220	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.473 m η = 8.0	x: 0.473 m η = 10.3	x: 0 m η = 0.6	x: 0.63 m η = 1.3	x: 0 m η = 7.7	η = 0.1	x: 0.63 m η = 0.2	x: 0.63 m η = 1.5	x: 0 m η = 7.9	x: 0.63 m η < 0.1	x: 0 m η = 0.6	x: 0 m η = 11.7	x: 0.63 m η = 12.7	x: 0.63 m η = 12.0	CUMPLE η = 12.7
N220/N221	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.63 m η = 11.7	x: 0.63 m η = 14.6	x: 0.315 m η = 0.6	x: 0.63 m η = 2.3	x: 0 m η = 7.0	η = 0.7	x: 0.63 m η = 0.3	x: 0.63 m η = 2.6	x: 0 m η = 7.2	x: 0.63 m η = 0.1	x: 0 m η = 0.5	x: 0 m η = 11.6	x: 0.63 m η = 18.7	x: 0.63 m η = 17.8	CUMPLE η = 18.7
N221/N222	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.158 m η = 15.7	x: 0.158 m η = 19.1	η = 0.4	x: 0.63 m η = 0.9	x: 0.63 m η = 10.8	x: 0 m η = 0.8	x: 0 m η = 0.1	x: 0.63 m η = 1.1	x: 0.63 m η = 11.0	x: 0.63 m η < 0.1	x: 0.63 m η = 1.2	x: 0.63 m η = 13.6	x: 0.63 m η = 22.3	x: 0.63 m η = 21.8	CUMPLE η = 22.3
N222/N45	$w/t \leq (w/t)_{Max}$ Cumple	x: 0 m η = 18.4	x: 0 m η = 21.0	η = 1.3	x: 0.49 m η = 6.7	x: 0.49 m η = 15.5	x: 0.245 m η = 0.8	x: 0.49 m η = 0.6	x: 0.49 m η = 7.2	x: 0.49 m η = 15.7	x: 0.49 m η = 0.5	x: 0.49 m η = 2.5	x: 0.49 m η = 35.1	x: 0.49 m η = 31.2	x: 0.49 m η = 29.2	CUMPLE η = 35.1
N104/N230	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.245 m η = 9.9	x: 0.245 m η = 12.0	η = 2.3	x: 0 m η = 40.1	x: 0 m η = 16.1	x: 0.245 m η = 1.5	x: 0.49 m η = 5.7	x: 0 m η = 40.7	x: 0 m η = 16.6	x: 0 m η = 16.9	x: 0 m η = 2.8	x: 0 m η = 81.3	x: 0 m η = 66.2	x: 0 m η = 63.7	CUMPLE η = 81.3
N230/N229	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.315 m η = 7.4	x: 0.315 m η = 8.9	η = 0.6	x: 0 m η = 5.4	x: 0 m η = 10.3	x: 0.158 m η = 0.8	x: 0 m η = 0.6	x: 0 m η = 5.4	x: 0 m η = 10.5	x: 0 m η = 0.3	x: 0 m η = 1.1	x: 0 m η = 18.4	x: 0 m η = 14.9	x: 0 m η = 15.3	CUMPLE η = 18.4
N229/N228	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.315 m η = 3.9	x: 0.315 m η = 4.1	x: 0.315 m η = 0.5	x: 0 m η = 2.0	x: 0.63 m η = 6.4	x: 0 m η = 0.7	x: 0 m η = 0.3	x: 0 m η = 2.2	x: 0.63 m η = 6.5	x: 0 m η < 0.1	x: 0.63 m η = 0.4	x: 0.63 m η = 10.0	x: 0 m η = 8.3	x: 0.63 m η = 8.7	CUMPLE η = 10.0
N228/N227	$w/t \leq (w/t)_{Max}$ Cumple	η = 1.1	η < 0.1	x: 0.158 m η = 0.5	x: 0.63 m η = 1.1	x: 0.63 m η = 7.5	x: 0.158 m η = 0.1	x: 0 m η = 0.2	x: 0.63 m η = 1.3	x: 0.63 m η = 7.7	x: 0.63 m η < 0.1	x: 0.63 m η = 0.6	x: 0.63 m η = 12.0	x: 0.63 m η = 7.2	x: 0.63 m η = 10.3	CUMPLE η = 12.0
N227/N226	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.473 m η = 4.4	x: 0.473 m η = 3.9	η = 0.7	x: 0.473 m η = 1.3	x: 0.63 m η = 8.8	x: 0.158 m η = 0.1	x: 0 m η = 0.2	x: 0.473 m η = 1.6	x: 0.63 m η = 9.1	x: 0.473 m η < 0.1	x: 0.63 m η = 0.8	x: 0.63 m η = 14.4	x: 0.63 m η = 9.1	x: 0.63 m η = 12.1	CUMPLE η = 14.4
N226/N225	$w/t \leq (w/t)_{Max}$ Cumple	η = 8.1	η = 8.2	x: 0 m η = 0.6	x: 0 m η = 1.4	x: 0 m η = 9.9	x: 0.63 m η = 0.3	x: 0 m η = 0.2	x: 0 m η = 1.6	x: 0 m η = 10.2	x: 0 m η < 0.1	x: 0 m η = 1.0	x: 0 m η = 15.8	x: 0.63 m η = 11.7	x: 0 m η = 13.7	CUMPLE η = 15.8
N225/N224	$w/t \leq (w/t)_{Max}$ Cumple	η = 11.9	η = 12.5	x: 0.473 m η = 0.6	x: 0.63 m η = 1.7	x: 0 m η = 6.9	x: 0.473 m η = 0.4	x: 0.63 m η = 0.2	x: 0.63 m η = 1.9	x: 0 m η = 7.1	x: 0.63 m η < 0.1	x: 0 m η = 0.5	x: 0 m η = 11.5	x: 0.63 m η = 16.7	x: 0.63 m η = 15.8	CUMPLE η = 16.7
N224/N223	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.473 m η = 15.5	x: 0.473 m η = 16.9	x: 0.473 m η = 0.4	x: 0.63 m η = 2.4	x: 0.63 m η = 7.6	x: 0.473 m η = 0.9	x: 0.63 m η = 0.3	x: 0.63 m η = 2.6	x: 0.63 m η = 7.8	x: 0.63 m η = 0.1	x: 0.63 m η = 0.6	x: 0.63 m η = 14.1	x: 0.63 m η = 21.3	x: 0.63 m η = 20.3	CUMPLE η = 21.3
N223/N44	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.158 m η = 19.2	x: 0.158 m η = 21.6	η = 0.8	x: 0.63 m η = 28.5	x: 0.63 m η = 18.2	η = 0.9	x: 0.63 m η = 3.1	x: 0.63 m η = 28.9	x: 0.63 m η = 18.4	x: 0.63 m η = 8.4	x: 0.63 m η = 3.4	x: 0.63 m η = 69.2	x: 0.63 m η = 61.4	x: 0.63 m η = 58.6	CUMPLE η = 69.2

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N230/N105	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 4.0	x: 0 m η = 3.9	η = 4.5	x: 0.929 m η = 3.3	x: 0.929 m η = 5.3	x: 0.697 m η = 0.3	x: 0.929 m η = 0.2	x: 0.929 m η = 4.4	x: 0.929 m η = 7.2	x: 0.929 m η = 0.2	x: 0.929 m η = 0.5	x: 0.929 m η = 15.4	x: 0.929 m η = 9.5	x: 0.929 m η = 10.7	CUMPLE η = 15.4
N230/N215	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 4.3	x: 0 m η = 6.4	x: 0.401 m η = 2.3	x: 0 m η = 5.2	x: 0 m η = 3.5	x: 0.401 m η = 0.3	x: 0 m η = 0.6	x: 0 m η = 5.5	x: 0 m η = 3.7	x: 0 m η = 0.3	x: 0 m η = 0.1	N.P.(1)	x: 0 m η = 14.8	x: 0 m η = 13.8	CUMPLE η = 14.8
N229/N215	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 6.0	x: 0 m η = 7.1	x: 0.232 m η = 1.2	x: 0 m η = 0.3	x: 0 m η = 0.9	x: 0.929 m η = 0.1	x: 0 m η = 0.1	x: 0 m η = 0.8	x: 0.929 m η = 1.2	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 8.7	x: 0 m η = 8.2	CUMPLE η = 8.7
N229/N216	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 4.4	x: 0 m η = 6.3	x: 0.602 m η = 0.1	x: 0.802 m η = 1.0	x: 0 m η = 0.9	x: 0.401 m η = 0.1	x: 0.802 m η = 0.1	x: 0.802 m η = 1.1	x: 0 m η = 0.9	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0.802 m η = 7.7	x: 0.802 m η = 7.6	CUMPLE η = 7.7
N228/N216	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 5.7	x: 0 m η = 6.9	x: 0 m η = 1.3	x: 0.929 m η = 0.9	x: 0 m η = 0.9	η < 0.1	x: 0 m η = 0.1	x: 0.929 m η = 1.1	x: 0 m η = 1.2	x: 0.929 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 8.7	x: 0 m η = 8.1	CUMPLE η = 8.7
N228/N217	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 4.4	x: 0 m η = 6.2	x: 0.401 m η = 1.5	x: 0.802 m η = 1.1	x: 0 m η = 1.0	x: 0.602 m η = 0.1	x: 0.802 m η = 0.1	x: 0.802 m η = 1.3	x: 0 m η = 1.2	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 8.1	x: 0.802 m η = 7.8	CUMPLE η = 8.1
N227/N217	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 5.6	x: 0 m η = 7.0	x: 0.697 m η = 2.5	x: 0.929 m η = 0.8	x: 0 m η = 1.4	x: 0.465 m η < 0.1	x: 0 m η = 0.1	x: 0.697 m η = 1.5	x: 0 m η = 2.5	x: 0.697 m η < 0.1	x: 0 m η = 0.1	N.P.(1)	x: 0 m η = 8.4	x: 0.929 m η = 8.0	CUMPLE η = 8.4
N227/N218	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 4.5	x: 0 m η = 6.1	x: 0.802 m η = 2.0	x: 0.802 m η = 1.1	x: 0 m η = 1.0	x: 0.802 m η = 0.1	x: 0.802 m η = 0.1	x: 0.802 m η = 1.4	x: 0.802 m η = 1.4	x: 0.802 m η < 0.1	x: 0.802 m η < 0.1	N.P.(1)	x: 0 m η = 8.0	x: 0 m η = 7.6	CUMPLE η = 8.0
N226/N218	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 5.5	x: 0 m η = 7.1	x: 0 m η = 3.0	x: 0.929 m η = 0.9	x: 0.929 m η = 1.5	x: 0.232 m η < 0.1	x: 0 m η = 0.1	x: 0.697 m η = 1.8	x: 0.929 m η = 2.8	x: 0.697 m η < 0.1	x: 0.929 m η = 0.1	N.P.(1)	x: 0 m η = 8.3	x: 0.929 m η = 8.2	CUMPLE η = 8.3
N226/N219	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 4.6	x: 0 m η = 6.0	x: 0 m η = 2.1	x: 0.802 m η = 1.1	x: 0 m η = 1.0	x: 0.401 m η = 0.1	x: 0.802 m η = 0.1	x: 0.802 m η = 1.4	x: 0 m η = 1.5	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 8.0	x: 0 m η = 7.5	CUMPLE η = 8.0
N225/N219	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 5.4	x: 0 m η = 7.2	η = 2.5	x: 0.929 m η = 1.0	x: 0.929 m η = 1.4	x: 0.232 m η < 0.1	x: 0 m η = 0.1	x: 0.929 m η = 1.5	x: 0.929 m η = 2.5	x: 0.929 m η < 0.1	x: 0.929 m η = 0.1	N.P.(1)	x: 0.929 m η = 8.4	x: 0.929 m η = 8.4	CUMPLE η = 8.4
N225/N220	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 4.6	x: 0 m η = 5.8	x: 0.201 m η = 1.6	x: 0.802 m η = 1.2	x: 0 m η = 1.2	η = 0.1	x: 0.802 m η = 0.1	x: 0.802 m η = 1.6	x: 0 m η = 1.6	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 8.3	x: 0 m η = 7.5	CUMPLE η = 8.3
N224/N220	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 5.3	x: 0 m η = 7.3	η = 1.3	x: 0.929 m η = 1.0	x: 0.929 m η = 0.5	η < 0.1	x: 0.929 m η = 0.1	x: 0.929 m η = 1.1	x: 0.929 m η = 1.0	x: 0.929 m η < 0.1	x: 0.929 m η < 0.1	N.P.(1)	x: 0.929 m η = 8.4	x: 0.929 m η = 8.5	CUMPLE η = 8.5
N224/N221	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 4.8	x: 0 m η = 5.9	η = 0.7	x: 0 m η = 0.6	x: 0 m η = 0.9	η = 0.1	x: 0.802 m η = 0.1	x: 0 m η = 0.7	x: 0 m η = 1.2	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 7.3	x: 0 m η = 6.8	CUMPLE η = 7.3
N223/N221	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 5.5	x: 0 m η = 7.8	x: 0.465 m η = 1.3	x: 0 m η = 2.9	x: 0 m η = 0.7	η < 0.1	x: 0.929 m η = 0.3	x: 0 m η = 3.2	x: 0 m η = 1.3	x: 0 m η = 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 11.1	x: 0 m η = 11.3	CUMPLE η = 11.3
N223/N222	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 4.1	x: 0 m η = 4.7	x: 0.401 m η = 2.1	x: 0 m η = 3.9	x: 0 m η = 4.2	x: 0.401 m η = 0.5	x: 0 m η = 0.5	x: 0 m η = 3.9	x: 0 m η = 4.3	x: 0 m η = 0.2	x: 0 m η = 0.2	N.P.(1)	x: 0 m η = 12.8	x: 0 m η = 11.6	CUMPLE η = 12.8
N44/N222	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 3.9	x: 0 m η = 5.8	x: 0 m η = 4.9	x: 0 m η = 17.5	x: 0 m η = 9.7	η = 0.6	x: 0.929 m η = 1.3	x: 0 m η = 18.0	x: 0 m η = 10.6	x: 0 m η = 3.3	x: 0 m η = 1.1	x: 0 m η = 39.6	x: 0 m η = 33.5	x: 0 m η = 30.3	CUMPLE η = 39.6
N231/N232	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.41 m η = 25.4	x: 1.41 m η = 39.7	η = 1.8	x: 0 m η = 1.9	x: 1.41 m η = 18.7	x: 0.705 m η = 1.7	x: 0 m η = 0.2	x: 0 m η = 2.7	x: 1.41 m η = 19.5	x: 0 m η = 0.1	x: 1.41 m η = 3.8	x: 1.41 m η = 51.9	x: 1.41 m η = 62.5	x: 1.41 m η = 63.1	CUMPLE η = 63.1
N232/N233	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.233 m η = 13.7	x: 0.233 m η = 13.5	η = 0.6	x: 1.167 m η = 1.5	x: 0 m η = 37.6	x: 1.167 m η = 4.7	x: 0 m η = 0.1	x: 0 m η = 1.2	x: 0 m η = 37.9	x: 1.167 m η < 0.1	x: 0 m η = 14.6	x: 0 m η = 62.1	x: 0 m η = 51.6	x: 0 m η = 60.6	CUMPLE η = 62.1
N233/N234	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.35 m η = 13.5	x: 0 m η = 4.1	η = 1.2	x: 1.35 m η = 4.3	x: 1.35 m η = 53.4	x: 0.225 m η = 6.2	x: 0 m η = 0.3	x: 1.35 m η = 4.3	x: 1.35 m η = 53.9	x: 1.35 m η = 0.2	x: 1.35 m η = 29.4	x: 1.35 m η = 79.6	x: 1.35 m η = 55.3	x: 1.35 m η = 75.0	CUMPLE η = 79.6
N234/N235	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.79 m η = 16.6	x: 0 m η = 6.4	η = 6.9	x: 0 m η = 10.7	x: 0 m η = 50.7	η = 10.1	x: 0.79 m η = 2.2	x: 0 m η = 10.7	x: 0 m η = 53.7	x: 0 m η = 1.2	x: 0 m η = 29.8	x: 0 m η = 87.5	x: 0 m η = 60.3	x: 0 m η = 74.0	CUMPLE η = 87.5
N234/N236	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.536 m η = 2.5	x: 0.536 m η = 4.6	x: 0.536 m η = 2.1	x: 1.073 m η = 9.7	x: 1.073 m η = 14.8	x: 0.179 m η = 2.0	x: 1.073 m η = 1.4	x: 1.073 m η = 9.7	x: 1.073 m η = 15.7	x: 1.073 m η = 1.0	x: 1.073 m η = 2.5	x: 1.073 m η = 26.1	x: 1.073 m η = 24.9	x: 1.073 m η = 23.5	CUMPLE η = 26.1
N231/N239	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.755 m η = 23.9	x: 0 m η = 56.3	x: 0.566 m η = 5.1	x: 0.755 m η = 11.0	x: 0 m η = 20.2	x: 0.566 m η = 1.8	x: 0.755 m η = 1.2	x: 0.755 m η = 13.2	x: 0 m η = 22.4	x: 0.755 m η = 1.8	x: 0 m η = 5.0	x: 0 m η = 13.9	x: 0.755 m η = 63.7	x: 0.755 m η = 62.5	CUMPLE η = 63.7
N239/N232	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.847 m η = 28.5	x: 0 m η = 20.0	η = 0.7	x: 0 m η = 10.5	x: 0 m η = 57.0	x: 0.635 m η = 6.6	x: 0 m η = 0.9	x: 0 m η = 10.5	x: 0 m η = 57.4	x: 0 m η = 1.1	x: 0 m η = 33.3	x: 0 m η = 82.9	x: 0 m η = 28.3	x: 0 m η = 78.9	CUMPLE η = 82.9
N232/N238	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.217 m η = 10.3	x: 0.217 m η = 24.7	x: 0.652 m η = 1.6	x: 0.869 m η = 4.0	x: 0 m η = 7.8	η = 0.6	x: 0 m η = 0.5	x: 0 m η = 4.1	x: 0 m η = 8.4	x: 0 m η = 0.2	x: 0 m η = 0.7	x: 0 m η = 13.4	x: 0.869 m η = 29.2	x: 0.869 m η = 29.6	CUMPLE η = 29.6
N238/N233	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.983 m η = 15.6	x: 0 m η = 11.8	η = 0.4	x: 0 m η = 2.9	x: 0 m η = 28.7	η = 2.9	x: 0.983 m η = 0.3	x: 0 m η = 2.9	x: 0 m η = 28.9	x: 0 m η = 0.1	x: 0 m η = 8.4	x: 0 m η = 46.0	x: 0 m η = 33.2	x: 0 m η = 45.1	CUMPLE η = 46.0
N233/N237	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.685 m η = 6.7	x: 0.685 m η = 17.0	x: 0 m η = 0.8	x: 0 m η = 3.1	x: 0 m η = 1.4	η < 0.1	x: 0 m η = 0.3	x: 0 m η = 2.7	x: 0 m η = 1.7	x: 0 m η = 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 19.9	x: 0 m η = 20.1	CUMPLE η = 20.1
N237/N234	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 9.5	x: 0 m η = 8.4	x: 0.557 m η = 4.9	x: 0.928 m η = 1.5	x: 1.114 m η = 28.7	x: 0.557 m η = 2.2	x: 0 m η = 0.1	x: 0 m η = 3.0	x: 1.114 m η = 30.8	x: 0 m η = 0.1	x: 1.114 m η = 9.6	x: 1.114 m η = 49.7	x: 1.114 m η = 40.1	x: 1.114 m η = 44.3	CUMPLE η = 49.7
N236/N235	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.096 m η = 12.4	x: 0 m η = 57.6	η = 4.0	x: 0 m η = 3.9	x: 0 m η = 9.4	η = 0.5	x: 0 m η = 0.4	x: 0 m η = 3.4	x: 0 m η = 11.1	x: 0 m η = 0.2	x: 0 m η = 1.2	N.P.(1)	x: 0 m η = 63.1	x: 0 m η = 62.4	CUMPLE η = 63.1
N244/N240	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.41 m η = 25.3	x: 1.41 m η = 39.3	η = 1.8	x: 0 m η = 1.9	x: 1.41 m η = 17.6	x: 0.529 m η = 1.6	x: 0 m η = 0.2	x: 0 m η = 2.7	x: 1.41 m η = 18.4	x: 0 m η = 0.1	x: 1.41 m η = 3.4	x: 1.41 m η = 50.3	x: 1.41 m η = 60.7	x: 1.41 m η = 61.3	CUMPLE η = 61.3
N240/N241	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.233 m η = 13.3	x: 0.233 m η = 12.8	x: 1.167 m η = 0.6	x: 0.933 m η = 1.5	x: 0 m η = 37.0	x: 0.233 m η = 4.6	x: 0 m η = 0.1	x: 0 m η = 1.2	x: 0 m η = 37.2	x: 0.7 m η < 0.1	x: 0 m η = 14.1	x: 0 m η = 60.8	x: 0 m η = 50.3	x: 0 m η = 59.4	CUMPLE η = 60.8
N241/N242	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.35 m η = 13.7	x: 0 m η = 4.8	x: 0.225 m η = 1.1	x: 1.35 m η = 4.4	x: 1.35 m η = 52.1	x: 0.45 m η = 6.0	x: 0 m η = 0.3	x: 1.35 m η = 4.4	x: 1.35 m η = 52.6	x: 1.35 m η = 0.2	x: 1.35 m η = 28.0	x: 1.35 m η = 78.4	x: 1.35 m η = 54.3	x: 1.35 m η = 73.8	CUMPLE η = 78.4
N242/N243	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.79 m η = 16.8	x: 0 m η = 6.6	x: 0.592 m η = 6.5	x: 0 m η = 10.3	x: 0 m η = 49.6	η = 9.7	x: 0.79 m η = 1.9	x: 0 m η = 10.3	x: 0 m η = 52.4	x: 0 m η = 1.1	x: 0 m η = 28.4	x: 0 m η = 86.1	x: 0 m η = 58.9	x: 0 m η = 73.2	CUMPLE η = 86.1
N244/N248	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.755 m η = 25.2	x: 0 m η = 57.7	x: 0.189 m η = 4.8	x: 0.755 m η = 10.5	x: 0 m η = 19.3	x: 0.566 m η = 1.8	x: 0.755 m η = 1.1	x: 0.755 m η = 12.6	x: 0 m η = 21.4	x: 0.755 m η = 1.6	x: 0 m η = 4.6	x: 0 m η = 14.2	x: 0.755 m η = 64.8	x: 0.755 m η = 63.8	CUMPLE η = 64.8
N248/N240	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.847 m η = 29.2	x: 0 m η = 21.0	η = 0.8	x: 0 m η = 10.7	x: 0 m η = 54.4	x: 0.635 m η = 6.3	x: 0 m η = 0.9	x: 0 m η = 10.7	x: 0 m η = 54.8	x: 0 m η = 1.2	x: 0 m η = 30.4	x: 0 m η = 81.1	x: 0 m η = 29.8	x: 0 m η = 76.4	CUMPLE η = 81.1
N240/N247	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.217 m η = 10.8	x: 0.217 m η = 25.4	x: 0.652 m η = 1.6	x: 0.869 m η = 4.1	x: 0 m η = 8.0	η = 0.6	x: 0 m η = 0.5	x: 0 m η = 4.2	x: 0 m η = 8.7	x: 0 m η = 0.2	x: 0 m η = 0.8	x: 0 m η = 14.2	x: 0.869 m η = 30.0	x: 0.869 m η = 30.4	CUMPLE η = 30.4
N247/N241	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.983 m η = 15.9	x: 0 m η = 12.4	x: 0.246 m η = 0.4	x: 0 m η = 3.0	x: 0 m η = 27.9	x: 0.246 m η = 2.8	x: 0.983 m η = 0.3	x: 0 m η = 3.0	x: 0 m η = 28.1	x: 0 m η = 0.1	x: 0 m η = 8.0	x: 0 m η = 45.0	x: 0 m η = 32.6	x: 0 m η = 44.3	CUMPLE η = 45.0
N241/N246	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.685 m η = 6.9	x: 0.685 m η = 17.2	x: 1.028 m η = 0.7	x: 0 m η = 3.0	x: 0 m η = 1.3	η < 0.1	x: 0 m η = 0.3	x: 0 m η = 2.7	x: 0 m η = 1.6	x: 0 m η = 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 20.2	x: 0 m η = 20.3	CUMPLE η = 20.3

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N246/N242	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 9.4	x: 0 m η = 8.2	x: 0.557 m η = 4.8	x: 1.114 m η = 1.6	x: 1.114 m η = 28.0	η = 2.1	x: 0 m η = 0.1	x: 0.371 m η = 2.9	x: 1.114 m η = 30.1	x: 0.371 m η = 0.1	x: 1.114 m η = 9.1	x: 1.114 m η = 48.9	x: 1.114 m η = 39.2	x: 1.114 m η = 43.5	CUMPLE η = 48.9
N242/N245	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.358 m η = 2.5	x: 0.358 m η = 4.6	x: 0.358 m η = 2.2	x: 1.073 m η = 8.5	x: 1.073 m η = 14.2	x: 0.358 m η = 1.9	x: 1.073 m η = 1.2	x: 1.073 m η = 8.5	x: 1.073 m η = 15.2	x: 1.073 m η = 0.7	x: 1.073 m η = 2.3	x: 1.073 m η = 25.1	x: 1.073 m η = 24.0	x: 1.073 m η = 22.6	CUMPLE η = 25.1
N245/N243	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.096 m η = 13.5	x: 0 m η = 61.6	x: 0.914 m η = 4.2	x: 0 m η = 3.6	x: 0 m η = 9.9	x: 0.914 m η = 0.6	x: 0 m η = 0.4	x: 0 m η = 3.3	x: 0 m η = 11.7	x: 0 m η = 0.1	x: 0 m η = 1.4	N.P.[1]	x: 0 m η = 66.8	x: 0 m η = 66.0	CUMPLE η = 66.8
N236/N249	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.617 m η = 7.0	x: 0 m η = 26.3	x: 0.617 m η = 4.8	x: 0 m η = 17.4	x: 0 m η = 6.9	η = 1.0	x: 0 m η = 3.3	x: 0 m η = 17.5	x: 0 m η = 9.0	x: 0 m η = 3.2	x: 0 m η = 0.8	x: 0 m η = 10.3	x: 0 m η = 44.3	x: 0 m η = 48.1	CUMPLE η = 48.1
N249/N250	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.081 m η = 9.0	x: 0 m η = 20.5	x: 0.18 m η = 2.1	x: 1.081 m η = 1.8	x: 0 m η = 4.4	η = 0.7	x: 1.081 m η = 0.3	x: 1.081 m η = 1.9	x: 0 m η = 5.4	x: 1.081 m η < 0.1	x: 0 m η = 0.3	x: 1.081 m η = 10.7	x: 1.081 m η = 22.8	x: 1.081 m η = 22.9	CUMPLE η = 22.9
N250/N251	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.088 m η = 10.3	x: 0 m η = 16.2	x: 0.544 m η = 1.9	x: 0 m η = 2.2	x: 1.088 m η = 1.8	x: 0.363 m η = 0.3	x: 0 m η = 0.3	x: 0 m η = 2.2	x: 1.088 m η = 2.6	x: 0 m η < 0.1	x: 1.088 m η = 0.1	x: 0.544 m η = 11.7	x: 0 m η = 18.7	x: 0 m η = 19.0	CUMPLE η = 19.0
N251/N252	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.08 m η = 10.6	x: 0 m η = 11.6	x: 0.9 m η = 0.8	x: 0 m η = 1.1	x: 0 m η = 3.0	η = 0.4	x: 0 m η = 0.2	x: 0 m η = 1.1	x: 0 m η = 3.3	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 5.9	x: 0 m η = 13.0	x: 0 m η = 13.0	CUMPLE η = 13.0
N252/N253	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.085 m η = 11.0	x: 1.085 m η = 8.3	η = 0.2	x: 1.085 m η = 1.7	x: 1.085 m η = 4.2	η = 0.6	x: 0 m η = 0.2	x: 1.085 m η = 1.7	x: 1.085 m η = 4.2	x: 1.085 m η < 0.1	x: 1.085 m η = 0.2	x: 0.723 m η = 12.4	x: 0 m η = 9.5	x: 0.723 m η = 12.3	CUMPLE η = 12.4
N253/N254	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.082 m η = 11.1	x: 1.082 m η = 5.2	η = 0.4	x: 1.082 m η = 1.7	x: 0 m η = 1.6	η = 0.1	x: 0 m η = 0.1	x: 1.082 m η = 1.7	x: 0 m η = 1.8	x: 1.082 m η < 0.1	x: 0 m η < 0.1	x: 1.082 m η = 13.4	x: 0 m η = 6.4	x: 1.082 m η = 13.2	CUMPLE η = 13.4
N254/N255	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.085 m η = 13.6	x: 0 m η = 2.4	x: 0.542 m η = 0.9	x: 0.904 m η = 1.8	x: 0 m η = 0.9	x: 0 m η = 0.1	x: 0 m η = 0.1	x: 0.904 m η = 1.8	x: 0 m η = 1.3	x: 0.904 m η < 0.1	x: 0 m η < 0.1	x: 1.085 m η = 16.0	x: 0 m η = 3.6	x: 0.904 m η = 15.8	CUMPLE η = 16.0
N255/N256	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.081 m η = 15.4	N.P.[2]	η = 0.5	x: 0.901 m η = 2.0	x: 0 m η = 1.2	x: 0.54 m η = 0.2	x: 0 m η = 0.1	x: 0.36 m η = 1.1	x: 0 m η = 1.3	x: 0.901 m η < 0.1	x: 0 m η < 0.1	x: 1.081 m η = 18.2	N.P.[3]	x: 0.901 m η = 18.0	CUMPLE η = 18.2
N257/N256	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.08 m η = 16.0	N.P.[2]	η = 0.7	x: 0.72 m η = 2.0	x: 0 m η = 1.9	x: 0.36 m η = 0.3	x: 0 m η = 0.1	x: 0.54 m η = 1.2	x: 0 m η = 2.0	x: 0.54 m η < 0.1	x: 0 m η < 0.1	x: 0.72 m η = 18.7	N.P.[3]	x: 0.72 m η = 18.6	CUMPLE η = 18.7
N258/N257	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.084 m η = 15.0	N.P.[2]	x: 1.084 m η = 0.9	x: 0.722 m η = 2.0	x: 0 m η = 1.8	η = 0.2	x: 0 m η = 0.1	x: 0.722 m η = 2.0	x: 0 m η = 1.9	x: 0.722 m η < 0.1	x: 0 m η < 0.1	x: 0.903 m η = 17.6	N.P.[3]	x: 0.903 m η = 17.5	CUMPLE η = 17.6
N259/N258	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.08 m η = 12.7	x: 0.54 m η = 2.6	η = 0.3	x: 1.08 m η = 1.9	x: 1.08 m η = 1.9	x: 1.08 m η = 0.2	x: 0 m η = 0.1	x: 1.08 m η = 1.9	x: 1.08 m η = 2.0	x: 1.08 m η < 0.1	x: 1.08 m η < 0.1	x: 1.08 m η = 15.2	x: 0 m η = 4.6	x: 1.08 m η = 15.0	CUMPLE η = 15.2
N260/N259	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.722 m η = 10.3	x: 0.722 m η = 6.2	η = 0.5	x: 1.083 m η = 1.9	x: 0 m η = 1.9	η = 0.3	x: 0 m η = 0.2	x: 1.083 m η = 1.9	x: 0 m η = 2.0	x: 1.083 m η < 0.1	x: 0 m η < 0.1	x: 0.18 m η = 12.7	x: 0 m η = 7.9	x: 0.722 m η = 11.9	CUMPLE η = 12.7
N261/N260	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.087 m η = 9.8	x: 0.362 m η = 9.5	x: 0.724 m η = 0.7	x: 1.087 m η = 1.3	x: 0 m η = 0.4	x: 1.087 m η = 0.1	x: 0 m η = 0.2	x: 0.724 m η = 1.4	x: 0 m η = 0.7	x: 0.724 m η < 0.1	x: 0 m η < 0.1	x: 0.543 m η = 11.9	x: 0 m η = 11.2	x: 0.724 m η = 11.2	CUMPLE η = 11.9
N262/N261	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.085 m η = 9.3	x: 0 m η = 13.6	η = 1.9	x: 0 m η = 1.9	x: 1.085 m η = 4.4	x: 0.542 m η = 0.6	x: 0 m η = 0.3	x: 0 m η = 2.0	x: 1.085 m η = 5.2	x: 0 m η < 0.1	x: 1.085 m η = 0.3	x: 1.085 m η = 12.2	x: 0 m η = 16.5	x: 0 m η = 16.2	CUMPLE η = 16.5
N263/N262	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.077 m η = 8.5	x: 0 m η = 18.3	x: 0 m η = 2.2	x: 1.077 m η = 1.5	x: 0 m η = 4.6	x: 0.718 m η = 0.7	x: 1.077 m η = 0.2	x: 1.077 m η = 1.6	x: 0 m η = 5.6	x: 1.077 m η < 0.1	x: 0 m η = 0.3	x: 0 m η = 4.6	x: 1.077 m η = 20.8	x: 1.077 m η = 20.5	CUMPLE η = 20.8
N245/N263	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.801 m η = 7.3	x: 0 m η = 24.1	η = 4.3	x: 0 m η = 14.9	x: 0 m η = 7.1	η = 0.9	x: 0 m η = 2.1	x: 0 m η = 15.0	x: 0 m η = 9.0	x: 0 m η = 2.3	x: 0 m η = 0.8	x: 0 m η = 15.5	x: 0 m η = 39.6	x: 0 m η = 42.7	CUMPLE η = 42.7
N265/N264	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.94 m η = 5.9	x: 0 m η = 16.6	η = 0.7	x: 1.128 m η = 2.3	x: 0 m η = 9.4	η = 1.4	x: 0 m η = 0.3	x: 1.128 m η = 2.3	x: 0 m η = 9.4	x: 1.128 m η = 0.1	x: 0 m η = 0.9	x: 0 m η = 11.8	x: 1.128 m η = 21.3	x: 1.128 m η = 20.4	CUMPLE η = 21.3
N266/N265	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.126 m η = 9.0	x: 0 m η = 14.7	x: 0.375 m η = 0.9	x: 1.126 m η = 1.8	x: 1.126 m η = 7.0	x: 0.375 m η = 1.0	x: 0 m η = 0.3	x: 1.126 m η = 1.9	x: 1.126 m η = 7.4	x: 1.126 m η < 0.1	x: 1.126 m η = 0.6	x: 0 m η = 12.8	x: 1.126 m η = 17.6	x: 1.126 m η = 17.0	CUMPLE η = 17.6
N267/N266	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.126 m η = 12.6	x: 1.126 m η = 12.7	η = 1.5	x: 0 m η = 1.2	x: 0 m η = 2.5	x: 0.188 m η = 0.2	x: 0 m η = 0.3	x: 1.126 m η = 1.3	x: 0 m η = 3.2	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 15.6	x: 1.126 m η = 14.9	x: 1.126 m η = 14.8	CUMPLE η = 15.6
N268/N267	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.12 m η = 17.0	x: 0 m η = 10.5	x: 0.373 m η = 0.6	x: 0 m η = 8.2	x: 1.12 m η = 3.5	x: 0 m η = 0.4	x: 0 m η = 1.0	x: 0 m η = 8.3	x: 1.12 m η = 3.8	x: 0 m η = 0.7	x: 1.12 m η = 0.1	x: 0 m η = 25.4	x: 1.12 m η = 12.7	x: 0 m η = 24.3	CUMPLE η = 25.4
N243/N268	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.187 m η = 22.4	x: 0.594 m η = 8.7	x: 0.396 m η = 3.5	x: 1.187 m η = 7.1	x: 0 m η = 13.0	x: 0.594 m η = 1.6	x: 1.187 m η = 1.0	x: 1.187 m η = 7.2	x: 0 m η = 14.6	x: 1.187 m η = 0.5	x: 0 m η = 2.1	x: 1.187 m η = 31.8	x: 0 m η = 13.4	x: 1.187 m η = 31.3	CUMPLE η = 31.8
N259/N264	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.934 m η = 9.5	x: 0.701 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 1.3	x: 0.934 m η = 3.4	x: 0.701 m η = 0.2	x: 0 m η = 0.2	x: 0 m η = 1.3	x: 0.934 m η = 3.5	x: 0 m η < 0.1	x: 0.934 m η = 0.1	N.P.[1]	x: 0 m η = 4.4	x: 0.934 m η = 10.9	CUMPLE η = 10.9
N260/N264	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.006 m η = 1.1	x: 0 m η = 17.3	x: 0.671 m η = 0.9	x: 0 m η = 1.9	x: 1.006 m η = 1.0	x: 0.671 m η = 0.1	x: 1.006 m η = 0.2	x: 0 m η = 1.2	x: 1.006 m η = 1.2	x: 0 m η < 0.1	x: 1.006 m η < 0.1	N.P.[1]	x: 0 m η = 19.4	x: 0 m η = 19.7	CUMPLE η = 19.7
N260/N265	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.94 m η = 12.5	N.P.[2]	η = 0.4	x: 0.94 m η = 1.6	x: 0 m η = 7.2	η = 0.7	x: 0 m η = 0.2	x: 0 m η = 1.4	x: 0 m η = 7.4	x: 0.94 m η < 0.1	x: 0 m η = 0.5	x: 0 m η = 16.7	N.P.[3]	x: 0 m η = 15.1	CUMPLE η = 16.7
N261/N265	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 21.9	η = 0.4	x: 0 m η = 2.2	x: 0 m η = 7.1	η = 0.6	x: 1.014 m η = 0.2	x: 1.014 m η = 1.1	x: 0 m η = 7.3	x: 0 m η < 0.1	x: 0 m η = 0.5	N.P.[1]	x: 0 m η = 24.5	x: 0 m η = 24.6	CUMPLE η = 24.6
N261/N266	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.935 m η = 14.2	N.P.[2]	x: 0.234 m η = 1.1	x: 0 m η = 2.3	x: 0.935 m η = 2.0	η = 0.2	x: 0 m η = 0.3	x: 0 m η = 1.7	x: 0.935 m η = 2.4	x: 0 m η = 0.1	x: 0.935 m η = 0.1	N.P.[1]	N.P.[3]	x: 0 m η = 17.1	CUMPLE η = 17.1
N262/N266	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 26.9	x: 0.846 m η = 0.2	x: 1.015 m η = 1.5	x: 1.015 m η = 4.1	η = 0.2	x: 1.015 m η = 0.2	x: 1.015 m η = 0.9	x: 1.015 m η = 4.2	x: 1.015 m η < 0.1	x: 1.015 m η = 0.2	N.P.[1]	x: 1.015 m η = 28.9	x: 1.015 m η = 28.8	CUMPLE η = 28.9
N262/N267	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.932 m η = 16.3	N.P.[2]	x: 0 m η = 0.9	x: 0 m η = 2.9	x: 0.932 m η = 4.6	x: 0.466 m η = 0.5	x: 0 m η = 0.3	x: 0 m η = 1.8	x: 0.932 m η = 5.0	x: 0 m η = 0.1	x: 0.932 m η = 0.3	N.P.[1]	N.P.[3]	x: 0 m η = 20.0	CUMPLE η = 20.0
N263/N267	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 31.3	x: 0.508 m η = 0.8	x: 0 m η = 4.1	x: 1.017 m η = 6.7	x: 0.847 m η = 0.5	x: 1.017 m η = 0.4	x: 1.017 m η = 2.4	x: 1.017 m η = 7.0	x: 0 m η = 0.2	x: 1.017 m η = 0.5	N.P.[1]	x: 0 m η = 36.1	x: 0 m η = 36.5	CUMPLE η = 36.5
N263/N268	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.932 m η = 16.4	N.P.[2]	x: 0 m η = 0.5	x: 0 m η = 4.1	x: 0.932 m η = 4.7	η = 0.3	x: 0 m η = 0.2	x: 0 m η = 2.2	x: 0.932 m η = 4.9	x: 0 m η = 0.2	x: 0.932 m η = 0.2	N.P.[1]	N.P.[3]	x: 0 m η = 21.5	CUMPLE η = 21.5
N245/N268	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 32.0	η = 3.0	x: 0 m η = 5.4	x: 0 m η = 8.8	x: 0.871 m η = 0.6	x: 0.871 m η = 0.5	x: 0 m η = 5.4	x: 0 m η = 10.1	x: 0 m η = 0.3	x: 0 m η = 1.0	N.P.[1]	x: 0 m η = 38.0	x: 0 m η = 38.5	CUMPLE η = 38.5
N273/N269	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.41 m η = 22.5	x: 1.41 m η = 36.1	η = 1.8	x: 0 m η = 1.9	x: 1.41 m η = 18.8	η = 1.7	x: 0 m η = 0.1	x: 0 m η = 2.7	x: 1.41 m η = 19.6	x: 0 m η = 0.1	x: 1.41 m η = 3.9	x: 1.41 m η = 49.3	x: 1.41 m η = 58.9	x: 1.41 m η = 59.5	CUMPLE η = 59.5
N269/N270	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 14.3	x: 0 m η = 14.2	x: 0 m η = 0.6	x: 0.933 m η = 1.5	x: 0 m η = 37.6	x: 0.7 m η = 4.7	x: 0 m η = 0.1	x: 0 m η = 1.3	x: 0 m η = 37.9	x: 1.167 m η < 0.1	x: 0 m η = 14.5	x: 0 m η = 63.1	x: 0 m η = 52.5	x: 0 m η = 61.2	CUMPLE η = 63.1
N270/N271	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.35 m η = 13.5	x: 0 m η = 4.1	η = 1.2	x: 1.35 m η = 4.5	x: 1.35 m η = 54.4	η = 6.3	x: 0 m η = 0.3	x: 1.35 m η = 4.5	x: 1.35 m η = 54.9	x: 1.35 m η = 0.2	x: 1.35 m η = 30.6	x: 1.35 m η = 76.8	x: 1.35 m η = 12.7	x: 1.35 m η = 73.5	CUMPLE η = 76.8
N271/N272	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.79 m η = 16.8	x: 0 m η = 6.1	x: 0.592 m η = 6.6	x: 0 m η = 10.6	x: 0 m η = 49.3	x: 0.592 m η = 10.0	x: 0.79 m η = 2.2	x: 0 m η = 10.6	x: 0 m η = 52.2	x: 0 m η = 1.2	x: 0 m η = 28.3	x: 0 m η = 79.0	x: 0 m η = 10.9	x: 0 m η = 68.7	CUMPLE η = 79.0



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2018))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N271/N274	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0 m η = 1.9	x: 0 m η = 4.0	η = 2.3	x: 1.073 m η = 9.8	x: 1.073 m η = 14.8	η = 2.0	x: 1.073 m η = 1.4	x: 1.073 m η = 9.8	x: 1.073 m η = 15.8	x: 1.073 m η = 1.0	x: 1.073 m η = 2.5	x: 1.073 m η = 28.4	x: 1.073 m η = 22.6	x: 1.073 m η = 22.6	CUMPLE η = 28.4
N269/N275	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.869 m η = 10.2	x: 0 m η = 24.6	x: 0.217 m η = 1.6	x: 0.869 m η = 4.0	x: 0 m η = 7.8	η = 0.6	x: 0 m η = 0.4	x: 0.869 m η = 4.0	x: 0 m η = 8.5	x: 0.869 m η = 0.2	x: 0 m η = 0.7	N.P.(1)	x: 0.869 m η = 29.0	x: 0.869 m η = 29.5	CUMPLE η = 29.5
N275/N270	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.983 m η = 15.6	x: 0 m η = 11.9	η = 0.4	x: 0 m η = 2.9	x: 0 m η = 28.7	η = 2.9	x: 0.983 m η = 0.3	x: 0 m η = 2.9	x: 0 m η = 28.8	x: 0 m η = 0.1	x: 0 m η = 8.4	x: 0 m η = 43.2	x: 0 m η = 14.9	x: 0 m η = 41.6	CUMPLE η = 43.2
N270/N276	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.028 m η = 6.4	x: 0 m η = 16.6	η = 0.8	x: 0 m η = 3.1	x: 1.028 m η = 1.3	η < 0.1	x: 0 m η = 0.3	x: 0 m η = 2.7	x: 1.028 m η = 1.7	x: 0 m η = 0.1	x: 1.028 m η < 0.1	N.P.(1)	x: 0 m η = 19.6	x: 0 m η = 19.9	CUMPLE η = 19.9
N276/N271	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0 m η = 9.3	x: 0 m η = 8.1	x: 0.743 m η = 5.0	x: 0.928 m η = 1.6	x: 1.114 m η = 29.4	x: 0.186 m η = 2.2	x: 0 m η = 0.1	x: 1.114 m η = 3.3	x: 1.114 m η = 31.5	x: 1.114 m η = 0.1	x: 1.114 m η = 10.0	x: 1.114 m η = 49.7	x: 1.114 m η = 39.4	x: 1.114 m η = 44.0	CUMPLE η = 49.7
N274/N272	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.365 m η = 12.7	x: 0 m η = 57.7	x: 0.731 m η = 3.8	x: 0 m η = 3.8	x: 0 m η = 9.2	x: 0.731 m η = 0.5	x: 0 m η = 0.3	x: 0 m η = 3.9	x: 0 m η = 10.8	x: 0 m η = 0.2	x: 0 m η = 1.2	N.P.(1)	x: 0 m η = 63.1	x: 0 m η = 62.5	CUMPLE η = 63.1
N281/N277	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.41 m η = 21.7	x: 1.41 m η = 34.9	x: 1.41 m η = 1.8	x: 0 m η = 1.8	x: 1.41 m η = 17.6	η = 1.6	x: 0 m η = 0.1	x: 0 m η = 2.6	x: 1.41 m η = 18.4	x: 0 m η = 0.1	x: 1.41 m η = 3.4	x: 1.41 m η = 47.0	x: 1.41 m η = 56.3	x: 1.41 m η = 56.9	CUMPLE η = 56.9
N277/N278	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.4 m η = 14.3	x: 0 m η = 14.1	x: 0 m η = 0.6	x: 0.7 m η = 1.5	x: 0 m η = 36.9	x: 0.467 m η = 4.6	x: 0 m η = 0.1	x: 0 m η = 1.2	x: 0 m η = 37.1	x: 0.7 m η < 0.1	x: 0 m η = 14.0	x: 0 m η = 62.2	x: 0 m η = 51.6	x: 0 m η = 60.4	CUMPLE η = 62.2
N278/N279	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.35 m η = 13.7	x: 0 m η = 5.1	x: 0.45 m η = 1.1	x: 1.35 m η = 4.7	x: 1.35 m η = 53.1	η = 6.1	x: 0 m η = 0.4	x: 1.35 m η = 4.7	x: 1.35 m η = 53.6	x: 1.35 m η = 0.2	x: 1.35 m η = 29.1	x: 1.35 m η = 74.3	x: 0 m η = 8.1	x: 1.35 m η = 71.3	CUMPLE η = 74.3
N279/N280	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.79 m η = 17.0	x: 0 m η = 6.3	x: 0.592 m η = 6.1	x: 0 m η = 10.1	x: 0 m η = 48.3	x: 0.592 m η = 9.7	x: 0.79 m η = 1.9	x: 0 m η = 10.2	x: 0 m η = 51.0	x: 0 m η = 1.1	x: 0 m η = 27.0	x: 0 m η = 76.7	x: 0 m η = 11.2	x: 0 m η = 67.2	CUMPLE η = 76.7
N285/N277	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.424 m η = 29.7	x: 0.424 m η = 21.7	x: 0.847 m η = 0.8	x: 0 m η = 10.8	x: 0 m η = 54.5	x: 0.635 m η = 6.3	x: 0 m η = 1.0	x: 0 m η = 10.9	x: 0 m η = 54.8	x: 0 m η = 1.2	x: 0 m η = 30.4	x: 0 m η = 84.3	x: 0 m η = 30.5	x: 0 m η = 80.2	CUMPLE η = 84.3
N277/N284	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.869 m η = 10.8	x: 0 m η = 25.4	η = 1.6	x: 0.869 m η = 4.1	x: 0 m η = 8.0	η = 0.6	x: 0 m η = 0.5	x: 0.869 m η = 4.1	x: 0 m η = 8.7	x: 0.869 m η = 0.2	x: 0 m η = 0.8	N.P.(1)	x: 0.869 m η = 29.9	x: 0.869 m η = 30.4	CUMPLE η = 30.4
N284/N278	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.983 m η = 16.1	x: 0 m η = 12.7	η = 0.4	x: 0 m η = 3.1	x: 0 m η = 27.9	η = 2.8	x: 0.983 m η = 0.3	x: 0 m η = 3.1	x: 0 m η = 28.0	x: 0 m η = 0.1	x: 0 m η = 7.9	x: 0 m η = 41.8	x: 0 m η = 15.7	x: 0 m η = 40.1	CUMPLE η = 41.8
N278/N283	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.685 m η = 7.1	x: 0.685 m η = 17.4	x: 0.856 m η = 0.7	x: 0 m η = 3.1	x: 1.028 m η = 1.3	η < 0.1	x: 0 m η = 0.3	x: 0 m η = 2.7	x: 1.028 m η = 1.7	x: 0 m η = 0.1	x: 1.028 m η < 0.1	N.P.(1)	x: 0 m η = 20.7	x: 0 m η = 20.8	CUMPLE η = 20.8
N283/N279	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0 m η = 10.0	x: 0 m η = 9.2	x: 0 m η = 4.9	x: 1.114 m η = 1.7	x: 1.114 m η = 28.7	η = 2.2	x: 0 m η = 0.1	x: 1.114 m η = 3.4	x: 1.114 m η = 30.8	x: 1.114 m η = 0.1	x: 1.114 m η = 9.5	x: 1.114 m η = 48.4	x: 1.114 m η = 38.3	x: 1.114 m η = 42.9	CUMPLE η = 48.4
N279/N282	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.073 m η = 2.0	x: 0 m η = 4.0	x: 0.358 m η = 2.3	x: 1.073 m η = 8.6	x: 1.073 m η = 14.2	η = 1.9	x: 1.073 m η = 1.2	x: 1.073 m η = 8.7	x: 1.073 m η = 15.3	x: 1.073 m η = 0.8	x: 1.073 m η = 2.4	x: 1.073 m η = 27.7	x: 1.073 m η = 21.7	x: 1.073 m η = 21.8	CUMPLE η = 27.7
N282/N280	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.365 m η = 14.3	x: 0 m η = 61.8	x: 0.731 m η = 4.0	x: 0 m η = 3.5	x: 0 m η = 9.7	x: 0.731 m η = 0.6	x: 0 m η = 0.4	x: 0 m η = 3.9	x: 0 m η = 11.4	x: 0 m η = 0.2	x: 0 m η = 1.3	N.P.(1)	x: 0 m η = 66.9	x: 0 m η = 66.2	CUMPLE η = 66.9
N274/N286	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.617 m η = 6.6	x: 0 m η = 26.6	η = 4.8	x: 0 m η = 17.6	x: 0 m η = 6.6	η = 1.0	x: 0 m η = 3.3	x: 0 m η = 17.7	x: 0 m η = 8.7	x: 0 m η = 3.2	x: 0 m η = 0.8	x: 0 m η = 8.9	x: 0 m η = 44.7	x: 0 m η = 48.6	CUMPLE η = 48.6
N286/N287	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0 m η = 8.8	x: 0 m η = 20.5	η = 2.0	x: 1.081 m η = 1.8	x: 0 m η = 4.4	x: 0.721 m η = 0.7	x: 1.081 m η = 0.3	x: 1.081 m η = 1.8	x: 0 m η = 5.3	x: 1.081 m η < 0.1	x: 0 m η = 0.3	x: 1.081 m η = 10.5	x: 1.081 m η = 22.7	x: 1.081 m η = 22.8	CUMPLE η = 22.8
N287/N288	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.088 m η = 10.4	x: 1.088 m η = 16.4	x: 0.544 m η = 1.9	x: 0 m η = 2.2	x: 1.088 m η = 1.8	η = 0.3	x: 0 m η = 0.3	x: 0 m η = 2.3	x: 1.088 m η = 2.6	x: 0 m η = 0.1	x: 1.088 m η = 0.1	x: 0.544 m η = 11.8	x: 0 m η = 18.9	x: 0 m η = 19.2	CUMPLE η = 19.2
N288/N289	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.08 m η = 10.8	x: 0 m η = 12.0	x: 0.9 m η = 0.8	x: 0 m η = 1.1	x: 0 m η = 2.9	x: 0.54 m η = 0.4	x: 0 m η = 0.2	x: 0 m η = 1.1	x: 0 m η = 3.3	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 7.0	x: 0 m η = 13.4	x: 0 m η = 13.4	CUMPLE η = 13.4
N289/N290	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.904 m η = 11.4	x: 0 m η = 8.9	η = 0.2	x: 1.085 m η = 1.7	x: 1.085 m η = 4.3	x: 0.362 m η = 0.6	x: 0 m η = 0.2	x: 1.085 m η = 1.7	x: 1.085 m η = 4.4	x: 1.085 m η < 0.1	x: 1.085 m η = 0.2	x: 0.904 m η = 12.9	x: 0 m η = 10.1	x: 0.723 m η = 12.8	CUMPLE η = 12.9
N290/N291	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.082 m η = 11.5	x: 1.082 m η = 6.1	η = 0.6	x: 1.082 m η = 1.7	x: 0 m η = 1.4	η = 0.1	x: 0 m η = 0.1	x: 1.082 m η = 1.8	x: 0 m η = 1.7	x: 1.082 m η < 0.1	x: 0 m η < 0.1	x: 1.082 m η = 13.3	x: 0 m η = 7.1	x: 1.082 m η = 13.0	CUMPLE η = 13.3
N291/N292	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.085 m η = 13.4	x: 1.085 m η = 3.7	x: 0.542 m η = 0.8	x: 0.904 m η = 1.8	x: 0 m η = 0.9	x: 0.362 m η = 0.1	x: 0 m η = 0.1	x: 0.904 m η = 1.8	x: 0 m η = 1.3	x: 0.904 m η < 0.1	x: 0 m η < 0.1	x: 1.085 m η = 15.9	x: 1.085 m η = 4.5	x: 0.904 m η = 15.6	CUMPLE η = 15.9
N292/N293	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.081 m η = 15.2	x: 0.72 m η = 1.0	η = 0.5	x: 1.081 m η = 2.1	x: 0 m η = 1.2	η = 0.1	x: 0 m η = 0.1	x: 1.081 m η = 2.1	x: 0 m η = 1.2	x: 1.081 m η < 0.1	x: 0 m η < 0.1	x: 1.081 m η = 18.1	x: 1.081 m η = 1.7	x: 1.081 m η = 17.8	CUMPLE η = 18.1
N294/N293	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.08 m η = 15.8	N.P.(2)	x: 0.54 m η = 0.7	x: 0.72 m η = 2.1	x: 0 m η = 1.9	x: 0.36 m η = 0.3	x: 0 m η = 0.1	x: 0.72 m η = 1.3	x: 0 m η = 2.0	x: 0.72 m η < 0.1	x: 0 m η < 0.1	x: 0.72 m η = 18.5	N.P.(3)	x: 0.72 m η = 18.4	CUMPLE η = 18.5
N295/N294	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.084 m η = 14.8	N.P.(2)	x: 0.903 m η = 0.7	x: 0.903 m η = 2.0	x: 0 m η = 1.8	x: 0.542 m η = 0.2	x: 0 m η = 0.1	x: 0.903 m η = 2.0	x: 0 m η = 2.0	x: 0.903 m η < 0.1	x: 0 m η < 0.1	x: 1.084 m η = 17.5	N.P.(3)	x: 0.903 m η = 17.3	CUMPLE η = 17.5
N296/N295	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.08 m η = 12.5	x: 0 m η = 0.8	x: 1.08 m η = 0.3	x: 0 m η = 2.0	x: 1.08 m η = 1.9	x: 1.08 m η = 0.2	x: 0 m η = 0.2	x: 0 m η = 2.1	x: 1.08 m η = 1.9	x: 0 m η < 0.1	x: 1.08 m η < 0.1	x: 1.08 m η = 15.1	x: 0 m η = 3.6	x: 1.08 m η = 14.9	CUMPLE η = 15.1
N297/N296	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.083 m η = 10.4	x: 0 m η = 6.5	η = 0.5	x: 1.083 m η = 1.9	x: 0 m η = 2.0	η = 0.3	x: 0 m η = 0.2	x: 1.083 m η = 2.0	x: 0 m η = 2.1	x: 1.083 m η < 0.1	x: 0 m η < 0.1	x: 0.902 m η = 13.3	x: 0 m η = 8.2	x: 1.083 m η = 12.7	CUMPLE η = 13.3
N298/N297	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.087 m η = 10.1	x: 1.087 m η = 9.9	x: 0.906 m η = 0.7	x: 1.087 m η = 1.3	x: 0 m η = 0.5	x: 1.087 m η = 0.1	x: 0 m η = 0.2	x: 1.087 m η = 1.4	x: 0 m η = 0.7	x: 1.087 m η < 0.1	x: 0 m η < 0.1	x: 1.087 m η = 4.7	x: 0 m η = 11.5	x: 0.724 m η = 11.3	CUMPLE η = 11.5
N299/N298	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.904 m η = 9.4	x: 0.904 m η = 13.8	x: 1.085 m η = 1.9	x: 0 m η = 1.9	x: 1.085 m η = 4.4	η = 0.6	x: 0 m η = 0.3	x: 0 m η = 2.0	x: 1.085 m η = 5.2	x: 0 m η < 0.1	x: 1.085 m η = 0.3	x: 1.085 m η = 12.2	x: 0 m η = 16.6	x: 0 m η = 16.4	CUMPLE η = 16.6
N300/N299	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.077 m η = 8.2	x: 0 m η = 18.0	η = 2.2	x: 1.077 m η = 1.5	x: 0 m η = 4.7	x: 0 m η = 0.7	x: 1.077 m η = 0.2	x: 1.077 m η = 1.5	x: 0 m η = 5.7	x: 1.077 m η < 0.1	x: 0 m η = 0.3	x: 1.077 m η = 2.6	x: 1.077 m η = 20.4	x: 1.077 m η = 20.1	CUMPLE η = 20.4
N282/N300	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.801 m η = 6.5	x: 0 m η = 24.3	x: 0.801 m η = 4.5	x: 0 m η = 15.0	x: 0 m η = 7.1	x: 0.2 m η = 0.9	x: 0 m η = 2.2	x: 0 m η = 15.1	x: 0 m η = 9.1	x: 0 m η = 2.3	x: 0 m η = 0.8	x: 0 m η = 11.0	x: 0 m η = 40.0	x: 0 m η = 43.1	CUMPLE η = 43.1
N302/N301	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.128 m η = 1.7	x: 0 m η = 16.5	η = 1.0	x: 1.128 m η = 2.3	x: 0 m η = 9.7	η = 1.4	x: 0 m η = 0.3	x: 1.128 m η = 2.1	x: 0 m η = 10.2	x: 1.128 m η = 0.1	x: 0 m η = 1.1	x: 0 m η = 7.7	x: 1.128 m η = 18.9	x: 0 m η = 20.2	CUMPLE η = 20.2
N303/N302	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.375 m η = 6.2	x: 0.375 m η = 11.8	x: 0.751 m η = 2.2	x: 1.126 m η = 1.8	x: 1.126 m η = 7.3	x: 0.751 m η = 1.0	x: 0 m η = 0.3	x: 1.126 m η = 1.9	x: 1.126 m η = 8.1	x: 1.126 m η < 0.1	x: 1.126 m η = 0.7	x: 0 m η = 10.0	x: 1.126 m η = 15.5	x: 1.126 m η = 14.6	CUMPLE η = 15.5
N304/N303	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.126 m η = 10.9	x: 0 m η = 10.8	η = 1.8	x: 0 m η = 1.2	x: 0 m η = 2.4	x: 0.188 m η = 0.2	x: 0 m η = 0.3	x: 0 m η = 1.5	x: 0 m η = 3.1	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 14.1	x: 1.126 m η = 13.1	x: 0 m η = 12.8	CUMPLE η = 14.1
N305/N304	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.12 m η = 16.1	x: 0 m η = 9.6	x: 0.187 m η = 0.2	x: 0 m η = 8.2	x: 1.12 m η = 3.3	x: 0.373 m η = 0.4	x: 0 m η = 1.0	x: 0 m η = 8.2	x: 1.12 m η = 3.4	x: 0 m η = 0.7	x: 1.12 m η = 0.1	x: 0 m η = 24.7	x: 0 m η = 11.9	x: 0 m η = 23.9	CUMPLE η = 24.7
N280/N305	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.187 m η = 22.4	x: 0 m η = 8.6	x: 0.594 m η = 5.0	x: 1.187 m η = 7.1	x: 0 m η = 12.7	x: 0.594 m η = 1.5	x: 1.187 m η = 1.0	x: 1.187 m η = 7.2	x: 0 m η = 15.0	x: 1.187 m η = 0.5	x: 0 m η = 2.3	x: 0 m η = 39.0	x: 0 m η = 18.3	x: 1.187 m η = 31.3	CUMPLE η = 39.0

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))														Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N296/N301	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.934 m η = 12.2	x: 0 m η = 8.9	x: 0 m η = 1.1	x: 0 m η = 2.1	x: 0.934 m η = 2.7	x: 0.701 m η = 0.3	x: 0 m η = 0.2	x: 0 m η = 2.1	x: 0.934 m η = 2.7	x: 0 m η < 0.1	x: 0.934 m η = 0.1	N.P.(1)	x: 0 m η = 12.7	x: 0 m η = 15.9	CUMPLE η = 15.9
N297/N301	$w / t \leq (w / t)_{Max.}$ Cumple	x: 1.006 m η = 1.3	x: 0 m η = 17.6	η = 0.2	x: 0 m η = 1.9	x: 1.006 m η = 3.6	x: 0.168 m η = 0.2	x: 1.006 m η = 0.2	x: 1.006 m η = 1.8	x: 1.006 m η = 3.6	x: 0 m η < 0.1	x: 1.006 m η = 0.1	N.P.(1)	x: 0 m η = 19.7	x: 0 m η = 20.0	CUMPLE η = 20.0
N297/N302	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.94 m η = 12.6	N.P.(2)	η = 0.1	x: 0.94 m η = 1.6	x: 0.94 m η = 8.8	x: 0.235 m η = 0.9	x: 0 m η = 0.2	x: 0 m η = 1.3	x: 0.94 m η = 8.8	x: 0.94 m η < 0.1	x: 0.94 m η = 0.8	x: 0.94 m η = 18.4	N.P.(3)	x: 0.94 m η = 17.1	CUMPLE η = 18.4
N298/N302	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.676 m η = 0.5	x: 0 m η = 22.5	η = 0.2	x: 0 m η = 2.2	x: 0.845 m η = 0.8	x: 0.845 m η = 0.8	x: 1.014 m η = 0.2	x: 1.014 m η = 1.3	x: 0 m η = 7.8	x: 0 m η < 0.1	x: 0 m η = 0.6	N.P.(1)	x: 0 m η = 24.9	x: 0 m η = 25.3	CUMPLE η = 25.3
N298/N303	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.935 m η = 14.5	x: 0.234 m η = 0.2	η = 0.2	x: 0 m η = 2.3	x: 0.935 m η = 7.6	x: 0.234 m η = 0.6	x: 0 m η = 0.3	x: 0 m η = 1.6	x: 0.935 m η = 7.7	x: 0 m η = 0.1	x: 0.935 m η = 0.6	x: 0.935 m η = 19.6	x: 0.935 m η = 8.0	x: 0.935 m η = 18.1	CUMPLE η = 19.6
N299/N303	$w / t \leq (w / t)_{Max.}$ Cumple	N.P.(4)	x: 0 m η = 27.4	x: 0.846 m η = 1.2	x: 1.015 m η = 1.6	x: 0 m η = 2.2	x: 0.846 m η = 0.1	x: 1.015 m η = 0.2	x: 1.015 m η = 1.4	x: 0 m η = 2.7	x: 1.015 m η < 0.1	x: 0 m η = 0.1	N.P.(1)	x: 1.015 m η = 29.2	x: 1.015 m η = 29.3	CUMPLE η = 29.3
N299/N304	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.932 m η = 16.6	N.P.(2)	η = 0.1	x: 0 m η = 3.0	x: 0 m η = 1.9	η = 0.1	x: 0 m η = 0.3	x: 0 m η = 1.8	x: 0 m η = 1.9	x: 0 m η = 0.1	x: 0 m η < 0.1	N.P.(1)	N.P.(3)	x: 0 m η = 20.3	CUMPLE η = 20.3
N300/N304	$w / t \leq (w / t)_{Max.}$ Cumple	N.P.(4)	x: 0 m η = 31.7	x: 0.339 m η = 0.3	x: 0 m η = 4.1	x: 1.017 m η = 1.1	x: 0.339 m η = 0.1	x: 1.017 m η = 0.4	x: 1.017 m η = 2.5	x: 1.017 m η = 1.2	x: 0 m η = 0.2	x: 1.017 m η < 0.1	N.P.(1)	x: 0 m η = 36.7	x: 0 m η = 36.9	CUMPLE η = 36.9
N300/N305	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.932 m η = 16.6	N.P.(2)	η = 0.2	x: 0 m η = 4.1	x: 0 m η = 0.6	x: 0.466 m η < 0.1	x: 0 m η = 0.3	x: 0 m η = 2.3	x: 0 m η = 0.6	x: 0 m η = 0.2	x: 0 m η < 0.1	N.P.(1)	N.P.(3)	x: 0 m η = 21.8	CUMPLE η = 21.8
N282/N305	$w / t \leq (w / t)_{Max.}$ Cumple	N.P.(4)	x: 0 m η = 32.3	η = 2.4	x: 0 m η = 5.5	x: 0 m η = 11.1	x: 0.653 m η = 1.1	x: 0.871 m η = 0.5	x: 0 m η = 5.6	x: 0 m η = 12.1	x: 0 m η = 0.3	x: 0 m η = 1.5	N.P.(1)	x: 0 m η = 38.2	x: 0 m η = 38.8	CUMPLE η = 38.8
N281/N285	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.566 m η = 26.0	x: 0.566 m η = 58.7	x: 0.378 m η = 4.8	x: 0.755 m η = 11.2	x: 0 m η = 19.3	x: 0.189 m η = 1.8	x: 0.755 m η = 1.1	x: 0.755 m η = 13.3	x: 0 m η = 21.4	x: 0.755 m η = 1.8	x: 0 m η = 4.6	x: 0 m η = 16.8	x: 0.755 m η = 66.5	x: 0.755 m η = 65.6	CUMPLE η = 66.5
N306/N269	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.424 m η = 28.7	x: 0.424 m η = 20.3	x: 0.847 m η = 0.7	x: 0 m η = 10.5	x: 0 m η = 57.1	x: 0.635 m η = 6.6	x: 0 m η = 0.9	x: 0 m η = 10.5	x: 0 m η = 57.4	x: 0 m η = 1.1	x: 0 m η = 33.4	x: 0 m η = 86.4	x: 0 m η = 28.5	x: 0 m η = 82.7	CUMPLE η = 86.4
N273/N306	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.566 m η = 24.3	x: 0.566 m η = 56.7	x: 0.189 m η = 5.1	x: 0.755 m η = 11.3	x: 0 m η = 20.2	x: 0.189 m η = 1.8	x: 0.755 m η = 1.2	x: 0.755 m η = 13.5	x: 0 m η = 22.4	x: 0.755 m η = 1.8	x: 0 m η = 5.1	x: 0 m η = 15.7	x: 0.755 m η = 64.6	x: 0.755 m η = 63.5	CUMPLE η = 64.6
N306/N239	$w / t \leq (w / t)_{Max.}$ Cumple	η < 0.1	η < 0.1	η = 3.5	x: 0.3 m η = 25.2	x: 0.3 m η = 2.5	η = 1.0	x: 0.3 m η = 51.5	x: 0.3 m η = 26.7	x: 0.3 m η = 4.0	x: 0.3 m η = 87.0	x: 0.3 m η = 0.2	x: 0.3 m η = 63.4	x: 0.3 m η = 30.7	x: 0.3 m η = 44.9	CUMPLE η = 44.9
N269/N232	$w / t \leq (w / t)_{Max.}$ Cumple	η = 0.1	η = 0.1	η = 0.5	x: 0.3 m η = 27.1	x: 0.3 m η = 30.4	η = 12.5	x: 0.3 m η = 52.3	x: 0.3 m η = 27.3	x: 0.3 m η = 30.6	x: 0.3 m η = 89.3	x: 0.3 m η = 10.9	x: 0.3 m η = 97.4	x: 0.3 m η = 58.0	x: 0.3 m η = 66.5	CUMPLE η = 66.5
N275/N238	$w / t \leq (w / t)_{Max.}$ Cumple	η < 0.1	η < 0.1	η < 0.1	x: 0.3 m η = 60.6	x: 0.3 m η = 3.8	x: 0.15 m η = 1.6	x: 0.15 m η = 68.4	x: 0.3 m η = 60.6	x: 0.3 m η = 3.9	x: 0.3 m η = 34.5	x: 0.3 m η = 0.2	x: 0.3 m η = 25.5	x: 0.3 m η = 64.2	x: 0.3 m η = 42.7	CUMPLE η = 42.7
N270/N233	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.15 m η < 0.1	x: 0.15 m η < 0.1	x: 0.15 m η = 1.1	x: 0 m η = 51.5	x: 0.3 m η = 30.8	x: 0.15 m η = 13.1	x: 0.15 m η = 64.5	x: 0 m η = 52.0	x: 0.3 m η = 31.3	x: 0 m η = 72.6	x: 0.3 m η = 11.5	x: 0 m η = 29.0	x: 0 m η = 83.3	x: 0 m η = 73.6	CUMPLE η = 73.6
N276/N237	$w / t \leq (w / t)_{Max.}$ Cumple	η < 0.1	η < 0.1	η = 1.5	x: 0 m η = 40.2	x: 0 m η = 15.5	η = 5.2	x: 0.3 m η = 47.0	x: 0 m η = 40.9	x: 0 m η = 16.2	x: 0 m η = 20.4	x: 0 m η = 2.9	x: 0 m η = 96.1	x: 0 m η = 56.9	x: 0 m η = 39.1	CUMPLE η = 39.1
N271/N234	$w / t \leq (w / t)_{Max.}$ Cumple	η = 0.6	η = 0.8	η = 1.0	x: 0 m η = 15.4	x: 0.3 m η = 25.6	x: 0 m η = 8.4	x: 0.3 m η = 5.0	x: 0 m η = 15.9	x: 0.3 m η = 26.0	x: 0 m η = 2.8	x: 0.3 m η = 7.5	x: 0 m η = 51.9	x: 0 m η = 41.7	x: 0 m η = 37.1	CUMPLE η = 51.9
N274/N236	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.15 m η = 0.3	x: 0.15 m η = 0.3	η = 0.7	x: 0.3 m η = 35.0	x: 0.3 m η = 13.4	η = 4.4	x: 0.15 m η = 11.7	x: 0.3 m η = 35.3	x: 0.3 m η = 13.7	x: 0.3 m η = 13.8	x: 0.3 m η = 2.1	x: 0.3 m η = 80.5	x: 0.3 m η = 48.7	x: 0.3 m η = 46.6	CUMPLE η = 80.5
N272/N235	$w / t \leq (w / t)_{Max.}$ Cumple	η = 2.6	η = 1.6	x: 0.15 m η = 0.8	x: 0.3 m η = 77.6	x: 0.3 m η = 30.1	x: 0.15 m η = 9.8	x: 0 m η = 25.8	x: 0.3 m η = 77.9	x: 0.3 m η = 30.5	x: 0.3 m η = 67.4	x: 0.3 m η = 10.2	x: 0.3 m η = 36.9	x: 0.3 m η = 19.7	x: 0.3 m η = 12.6	CUMPLE η = 36.9
N286/N249	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.15 m η = 0.1	x: 0.15 m η = 0.1	η = 0.8	x: 0.3 m η = 21.7	x: 0 m η = 14.7	η = 4.9	x: 0.3 m η = 7.2	x: 0.3 m η = 22.1	x: 0 m η = 15.1	x: 0.3 m η = 5.4	x: 0 m η = 2.5	x: 0.3 m η = 46.1	x: 0.3 m η = 36.0	x: 0.3 m η = 32.6	CUMPLE η = 46.1
N287/N250	$w / t \leq (w / t)_{Max.}$ Cumple	η < 0.1	η < 0.1	η = 0.7	x: 0.3 m η = 15.6	x: 0 m η = 17.4	x: 0.15 m η = 5.8	x: 0.3 m η = 5.2	x: 0.3 m η = 15.9	x: 0 m η = 17.7	x: 0.3 m η = 2.8	x: 0 m η = 3.5	x: 0.3 m η = 41.8	x: 0.3 m η = 32.2	x: 0.3 m η = 29.0	CUMPLE η = 41.8
N288/N251	$w / t \leq (w / t)_{Max.}$ Cumple	η < 0.1	η < 0.1	x: 0.15 m η = 0.4	x: 0 m η = 6.1	x: 0.3 m η = 15.0	η = 5.0	x: 0.3 m η = 2.1	x: 0 m η = 6.3	x: 0.3 m η = 15.2	x: 0.3 m η = 0.4	x: 0.3 m η = 2.5	x: 0 m η = 25.2	x: 0.3 m η = 21.5	x: 0.3 m η = 20.2	CUMPLE η = 25.2
N289/N252	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.15 m η < 0.1	x: 0.15 m η < 0.1	x: 0.15 m η = 0.1	x: 0.3 m η = 3.4	x: 0 m η = 22.4	x: 0.15 m η = 7.5	x: 0.3 m η = 1.1	x: 0.3 m η = 3.4	x: 0 m η = 22.5	x: 0.3 m η = 0.1	x: 0 m η = 5.6	x: 0 m η = 31.3	x: 0 m η = 25.9	x: 0 m η = 28.3	CUMPLE η = 31.3
N290/N253	$w / t \leq (w / t)_{Max.}$ Cumple	η = 0.4	η = 0.4	η = 0.2	x: 0.3 m η = 3.8	x: 0.3 m η = 14.1	η = 4.7	x: 0.3 m η = 1.2	x: 0.3 m η = 3.9	x: 0.3 m η = 14.2	x: 0.3 m η = 0.2	x: 0.3 m η = 2.2	x: 0.3 m η = 22.1	x: 0.3 m η = 18.5	x: 0.3 m η = 18.7	CUMPLE η = 22.1
N291/N254	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0 m η = 0.1	x: 0 m η = 0.1	x: 0 m η = 0.3	x: 0.3 m η = 1.4	x: 0 m η = 4.4	η = 1.5	x: 0.3 m η = 0.3	x: 0.3 m η = 1.5	x: 0 m η = 4.4	x: 0.3 m η < 0.1	x: 0 m η = 0.2	N.P.(1)	x: 0 m η = 4.4	x: 0 m η = 5.4	CUMPLE η = 5.4
N292/N255	$w / t \leq (w / t)_{Max.}$ Cumple	η = 0.1	η = 0.1	x: 0.3 m η = 0.2	x: 0 m η = 3.4	x: 0.3 m η = 7.2	η = 2.4	x: 0.3 m η = 1.1	x: 0 m η = 3.5	x: 0.3 m η = 7.2	x: 0 m η = 0.1	x: 0.3 m η = 0.6	x: 0 m η = 9.1	x: 0.3 m η = 7.0	x: 0.3 m η = 9.0	CUMPLE η = 9.1
N293/N256	$w / t \leq (w / t)_{Max.}$ Cumple	η = 0.6	η = 0.7	η = 0.3	x: 0.3 m η = 6.1	x: 0 m η = 11.4	x: 0.3 m η = 3.8	x: 0.3 m η = 2.0	x: 0.3 m η = 6.1	x: 0 m η = 11.4	x: 0.3 m η = 0.4	x: 0 m η = 1.5	x: 0 m η = 15.2	x: 0 m η = 12.0	x: 0 m η = 14.5	CUMPLE η = 15.2
N294/N257	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.15 m η = 0.1	x: 0.15 m η = 0.1	η = 0.3	x: 0.3 m η = 1.7	x: 0.3 m η = 12.9	x: 0 m η = 4.3	x: 0.3 m η = 0.6	x: 0.3 m η = 1.8	x: 0.3 m η = 12.9	x: 0.3 m η < 0.1	x: 0.3 m η = 1.9	x: 0 m η = 17.0	x: 0.3 m η = 13.1	x: 0.3 m η = 16.1	CUMPLE η = 17.0
N295/N258	$w / t \leq (w / t)_{Max.}$ Cumple	η = 0.1	η = 0.1	η = 0.3	x: 0.3 m η = 3.1	x: 0 m η = 11.1	η = 3.7	x: 0.3 m η = 0.9	x: 0.3 m η = 3.1	x: 0 m η = 11.2	x: 0.3 m η = 0.1	x: 0 m η = 1.4	x: 0 m η = 15.3	x: 0 m η = 11.6	x: 0 m η = 13.9	CUMPLE η = 15.3
N296/N259	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.3 m η = 0.1	x: 0.3 m η = 0.1	η = 0.1	x: 0.3 m η = 4.4	x: 0 m η = 12.7	x: 0.3 m η = 4.2	x: 0.3 m η = 1.4	x: 0.3 m η = 4.4	x: 0 m η = 12.8	x: 0.3 m η = 0.2	x: 0 m η = 1.8	x: 0.3 m η = 20.8	x: 0.3 m η = 16.1	x: 0.3 m η = 16.4	CUMPLE η = 20.8
N301/N264	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0 m η = 2.0	x: 0 m η = 2.3	η = 0.3	x: 0 m η = 11.6	x: 0.3 m η = 25.6	x: 0 m η = 8.2	x: 0 m η = 2.3	x: 0 m η = 11.5	x: 0.3 m η = 25.6	x: 0 m η = 1.4	x: 0.3 m η = 7.3	x: 0 m η = 45.8	x: 0 m η = 37.2	x: 0 m η = 34.9	CUMPLE η = 45.8
N297/N260	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0 m η = 0.1	x: 0 m η = 0.1	x: 0.3 m η = 0.5	x: 0 m η = 2.0	x: 0 m η = 14.0	x: 0 m η = 4.7	x: 0.3 m η = 0.6	x: 0 m η = 2.2	x: 0 m η = 14.0	x: 0 m η = 0.1	x: 0 m η = 2.2	x: 0 m η = 19.0	x: 0 m η = 14.7	x: 0 m η = 17.6	CUMPLE η = 19.0
N302/N265	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0 m η = 1.3	x: 0 m η = 1.8	η = 0.4	x: 0.3 m η = 7.4	x: 0.3 m η = 13.1	x: 0.3 m η = 4.2	x: 0 m η = 1.5	x: 0.3 m η = 7.5	x: 0.3 m η = 13.2	x: 0.3 m η = 0.6	x: 0.3 m η = 1.9	x: 0.3 m η = 25.0	x: 0.3 m η = 19.3	x: 0.3 m η = 18.3	CUMPLE η = 25.0
N298/N261	$w / t \leq (w / t)_{Max.}$ Cumple	η = 0.7	η = 0.7	η = 0.5	x: 0.3 m η = 3.1	x: 0 m η = 16.5	η = 5.4	x: 0.3 m η = 0.8	x: 0.3 m η = 3.3	x: 0 m η = 16.7	x: 0.3 m η = 0.1	x: 0 m η = 3.1	x: 0.3 m η = 23.2	x: 0.3 m η = 20.1	x: 0 m η = 21.4	CUMPLE η = 23.2
N303/N266	$w / t \leq (w / t)_{Max.}$ Cumple	x: 0.3 m η = 2.2	x: 0.3 m η = 2.4	x: 0.3 m η = 0.6	x: 0.3 m η = 8.5	x: 0 m η = 11.4	η = 3.3	x: 0 m η = 1.0	x: 0.3 m η = 8.8	x: 0 m η = 11.7	x: 0.3 m η = 0.8	x: 0 m η = 1.5	x: 0.3 m η = 23.2	x: 0.3 m η = 19.1	x: 0 m η = 16.9	CUMPLE η = 23.2
N299/N262	$w / t \leq (w / t)_{Max.}$ Cumple	η = 0.1	η = 0.1	η = 0.7	x: 0.3 m η = 13.2	x: 0 m η = 24.5	x: 0.3 m η = 8.1	x: 0.3 m η = 4.2	x: 0.3 m η = 13.5	x: 0 m η = 24.8	x: 0.3 m η = 2.0	x: 0 m η = 6.8	x: 0.3 m η = 47.3	x: 0.3 m η = 36.5	x: 0.3 m η = 34.1	CUMPLE η = 47.3

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N304/N267	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.3 m η = 2.5	x: 0.3 m η = 2.8	x: 0.3 m η = 0.7	x: 0 m η = 11.1	x: 0.3 m η = 7.2	η = 2.3	x: 0 m η = 1.7	x: 0 m η = 11.4	x: 0.3 m η = 7.2	x: 0 m η = 1.3	x: 0.3 m η = 0.6	x: 0 m η = 19.7	x: 0 m η = 16.6	x: 0 m η = 16.9	CUMPLE η = 19.7
N300/N263	$w/t \leq (w/t)_{Máx}$ Cumple	η = 0.1	η = 0.1	η = 0.8	x: 0.3 m η = 20.2	x: 0 m η = 19.2	x: 0.3 m η = 6.4	x: 0.3 m η = 6.5	x: 0.3 m η = 20.6	x: 0 m η = 19.6	x: 0.3 m η = 4.7	x: 0 m η = 4.2	x: 0.3 m η = 49.6	x: 0.3 m η = 38.6	x: 0.3 m η = 34.5	CUMPLE η = 49.6
N305/N268	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0 m η = 2.2	x: 0 m η = 2.2	η = 0.4	x: 0.3 m η = 7.1	x: 0.3 m η = 25.8	x: 0 m η = 8.1	x: 0 m η = 1.4	x: 0.3 m η = 7.2	x: 0.3 m η = 26.0	x: 0.3 m η = 0.5	x: 0.3 m η = 7.4	x: 0.3 m η = 43.0	x: 0.3 m η = 35.0	x: 0.3 m η = 35.3	CUMPLE η = 43.0
N282/N245	$w/t \leq (w/t)_{Máx}$ Cumple	η = 0.1	η = 0.1	η = 0.6	x: 0.3 m η = 35.5	x: 0.3 m η = 13.1	η = 4.4	x: 0.3 m η = 11.8	x: 0.3 m η = 35.7	x: 0.3 m η = 13.4	x: 0.3 m η = 14.1	x: 0.3 m η = 2.0	x: 0.3 m η = 60.8	x: 0.3 m η = 48.9	x: 0.3 m η = 47.0	CUMPLE η = 60.8
N280/N243	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.15 m η = 6.0	x: 0.15 m η = 5.2	η = 0.8	x: 0.3 m η = 78.8	x: 0.3 m η = 27.9	x: 0 m η = 9.0	x: 0 m η = 26.2	x: 0.3 m η = 79.2	x: 0.3 m η = 28.2	x: 0.3 m η = 69.5	x: 0.3 m η = 8.8	x: 0.3 m η = 39.2	x: 0.3 m η = 12.3	x: 0.3 m η = 20.9	CUMPLE η = 39.2
N279/N242	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.15 m η = 2.3	x: 0.15 m η = 2.7	x: 0.15 m η = 1.0	x: 0 m η = 14.6	x: 0.3 m η = 24.9	η = 8.2	x: 0.15 m η = 4.7	x: 0 m η = 15.0	x: 0.3 m η = 25.3	x: 0 m η = 2.5	x: 0.3 m η = 7.1	x: 0 m η = 51.4	x: 0 m η = 42.2	x: 0 m η = 37.9	CUMPLE η = 51.4
N283/N246	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.15 m η < 0.1	x: 0.15 m η < 0.1	η = 1.4	x: 0 m η = 36.0	x: 0 m η = 15.2	η = 5.1	x: 0.3 m η = 45.5	x: 0 m η = 36.7	x: 0 m η = 15.8	x: 0 m η = 27.5	x: 0 m η = 2.8	x: 0 m η = 90.2	x: 0 m η = 52.3	x: 0 m η = 91.0	CUMPLE η = 91.0
N278/N241	$w/t \leq (w/t)_{Máx}$ Cumple	η < 0.1	η < 0.1	η = 1.0	x: 0 m η = 48.1	x: 0.3 m η = 30.1	η = 12.8	x: 0.3 m η = 63.0	x: 0 m η = 48.6	x: 0.3 m η = 30.6	x: 0 m η = 60.5	x: 0.3 m η = 11.0	x: 0 m η = 23.8	x: 0 m η = 79.2	x: 0 m η = 57.0	CUMPLE η = 57.0
N284/N247	$w/t \leq (w/t)_{Máx}$ Cumple	η < 0.1	η < 0.1	η = 0.1	x: 0.3 m η = 55.5	x: 0.3 m η = 3.7	x: 0.15 m η = 1.6	x: 0.15 m η = 66.2	x: 0.3 m η = 55.5	x: 0.3 m η = 3.7	x: 0.3 m η = 85.7	x: 0.3 m η = 0.2	x: 0.3 m η = 99.0	x: 0.3 m η = 59.0	x: 0.3 m η = 77.8	CUMPLE η = 77.8
N277/N240	$w/t \leq (w/t)_{Máx}$ Cumple	η < 0.1	η < 0.1	x: 0.15 m η = 0.5	x: 0.3 m η = 22.9	x: 0.3 m η = 29.2	x: 0.15 m η = 12.0	x: 0.15 m η = 50.6	x: 0.3 m η = 23.1	x: 0.3 m η = 29.4	x: 0.3 m η = 77.1	x: 0.3 m η = 10.1	x: 0.3 m η = 90.6	x: 0.3 m η = 52.3	x: 0.3 m η = 49.1	CUMPLE η = 49.1
N285/N248	$w/t \leq (w/t)_{Máx}$ Cumple	η < 0.1	η < 0.1	η = 3.4	x: 0.3 m η = 20.4	x: 0.3 m η = 2.6	η = 1.1	x: 0.3 m η = 49.5	x: 0.3 m η = 21.8	x: 0.3 m η = 4.1	x: 0.3 m η = 72.9	x: 0.3 m η = 0.2	x: 0.3 m η = 57.4	x: 0.3 m η = 25.9	x: 0.3 m η = 26.5	CUMPLE η = 26.5
N301/N307	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.373 m η = 10.4	x: 0.373 m η = 25.8	η = 0.3	x: 1.118 m η = 2.3	x: 1.118 m η = 4.5	x: 0 m η = 0.5	x: 0 m η = 0.3	x: 0 m η = 2.1	x: 1.118 m η = 4.6	x: 1.118 m η = 0.1	x: 1.118 m η = 0.2	x: 0 m η = 15.5	x: 0 m η = 30.2	x: 0 m η = 29.3	CUMPLE η = 30.2
N264/N308	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.559 m η = 3.0	x: 0 m η = 23.7	η = 0.2	x: 1.118 m η = 2.3	x: 1.118 m η = 4.7	η = 0.5	x: 0 m η = 0.2	x: 0.559 m η = 1.3	x: 1.118 m η = 4.8	x: 1.118 m η = 0.1	x: 1.118 m η = 0.2	x: 0 m η = 6.8	x: 1.118 m η = 26.1	x: 1.118 m η = 26.6	CUMPLE η = 26.6
N296/N307	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.006 m η = 8.0	x: 0 m η = 17.5	x: 0 m η = 0.7	x: 0 m η = 1.8	x: 0 m η = 2.2	x: 0.335 m η = 0.2	x: 1.006 m η = 0.2	x: 1.006 m η = 1.2	x: 0 m η = 2.5	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 1.006 m η = 19.4	x: 1.006 m η = 19.1	CUMPLE η = 19.4
N295/N307	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.715 m η = 9.7	x: 0.715 m η = 8.1	η = 0.7	x: 0 m η = 2.0	x: 0 m η = 2.2	x: 0 m η = 0.1	x: 0 m η = 0.2	x: 0 m η = 2.1	x: 0 m η = 2.4	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0.953 m η = 11.2	x: 0.953 m η = 12.5	CUMPLE η = 12.5
N259/N308	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.006 m η = 3.7	x: 0 m η = 11.4	x: 0 m η = 0.2	x: 0 m η = 1.8	x: 1.006 m η = 5.2	x: 0.503 m η = 0.5	x: 1.006 m η = 0.2	x: 1.006 m η = 1.0	x: 1.006 m η = 5.3	x: 0 m η < 0.1	x: 1.006 m η = 0.3	N.P.[1]	x: 1.006 m η = 12.9	x: 0 m η = 13.2	CUMPLE η = 13.2
N258/N308	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.953 m η = 6.7	x: 0 m η = 4.1	η = 0.1	x: 0 m η = 1.2	x: 0.953 m η = 5.4	x: 0.476 m η = 0.5	x: 0 m η = 0.1	x: 0 m η = 1.2	x: 0.953 m η = 5.4	x: 0 m η < 0.1	x: 0.953 m η = 0.3	x: 0.953 m η = 10.7	x: 0.953 m η = 6.5	x: 0.953 m η = 10.0	CUMPLE η = 10.7
N307/N309	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0 m η = 3.9	x: 0 m η = 28.4	x: 1.119 m η = 1.2	x: 1.119 m η = 2.0	x: 0 m η = 2.7	x: 0.932 m η = 0.2	x: 0 m η = 0.2	x: 0.932 m η = 1.4	x: 0 m η = 3.3	x: 1.119 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 6.9	x: 1.119 m η = 30.5	x: 1.119 m η = 30.9	CUMPLE η = 30.9
N309/N310	$w/t \leq (w/t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 30.9	η = 2.5	x: 1.122 m η = 2.2	x: 0 m η = 5.2	x: 0.561 m η = 0.9	x: 0 m η = 0.2	x: 1.122 m η = 2.2	x: 0 m η = 6.3	x: 1.122 m η < 0.1	x: 0 m η = 0.4	N.P.[1]	x: 1.122 m η = 33.2	x: 1.122 m η = 33.6	CUMPLE η = 33.6
N308/N311	$w/t \leq (w/t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 28.2	x: 1.119 m η = 0.6	x: 1.119 m η = 2.0	x: 0 m η = 3.1	η = 0.2	x: 0 m η = 0.1	x: 1.119 m η = 2.1	x: 0 m η = 3.2	x: 1.119 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 1.119 m η = 30.5	x: 1.119 m η = 30.7	CUMPLE η = 30.7
N311/N312	$w/t \leq (w/t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 30.6	x: 0.561 m η = 1.1	x: 1.122 m η = 2.1	x: 0 m η = 5.0	x: 0.561 m η = 0.8	x: 0 m η = 0.1	x: 1.122 m η = 2.3	x: 0 m η = 5.5	x: 1.122 m η = 0.1	x: 0 m η = 0.3	N.P.[1]	x: 1.122 m η = 33.0	x: 1.122 m η = 33.2	CUMPLE η = 33.2
N307/N308	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0 m η = 2.2	x: 0 m η = 2.5	η = 0.3	x: 0 m η = 12.0	x: 0.3 m η = 12.1	x: 0.3 m η = 4.0	x: 0 m η = 2.3	x: 0 m η = 12.0	x: 0.3 m η = 12.2	x: 0 m η = 1.5	x: 0.3 m η = 1.7	x: 0 m η = 24.5	x: 0 m η = 20.5	x: 0 m η = 19.1	CUMPLE η = 24.5
N309/N311	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.3 m η = 1.1	x: 0.3 m η = 1.3	η = 0.2	x: 0 m η = 4.4	x: 0 m η = 13.6	x: 0.3 m η = 4.6	x: 0 m η = 0.9	x: 0 m η = 4.5	x: 0 m η = 13.7	x: 0 m η = 0.2	x: 0 m η = 2.1	x: 0 m η = 23.5	x: 0 m η = 19.4	x: 0 m η = 19.1	CUMPLE η = 23.5
N310/N312	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0 m η = 5.7	x: 0 m η = 6.8	η = 0.3	x: 0 m η = 8.1	x: 0.3 m η = 15.0	x: 0 m η = 4.9	x: 0 m η = 0.8	x: 0 m η = 8.2	x: 0.3 m η = 15.1	x: 0 m η = 0.7	x: 0.3 m η = 2.5	x: 0 m η = 33.7	x: 0 m η = 28.6	x: 0.3 m η = 27.1	CUMPLE η = 33.7
N295/N309	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.339 m η = 7.1	x: 0.339 m η = 13.3	x: 0.339 m η = 0.8	x: 0 m η = 1.5	x: 1.017 m η = 1.8	x: 0.339 m η = 0.2	x: 1.017 m η = 0.1	x: 0 m η = 1.1	x: 1.017 m η = 2.1	x: 0 m η < 0.1	x: 1.017 m η < 0.1	N.P.[1]	x: 0 m η = 14.6	x: 0 m η = 14.7	CUMPLE η = 14.7
N294/N309	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.974 m η = 7.8	x: 0 m η = 7.7	η = 0.3	x: 0 m η = 1.5	x: 0.974 m η = 1.8	x: 0 m η = 0.2	x: 0.974 m η = 0.2	x: 0 m η = 1.5	x: 0.974 m η = 1.9	x: 0 m η < 0.1	x: 0.974 m η < 0.1	N.P.[1]	x: 0.974 m η = 10.4	x: 0.974 m η = 10.3	CUMPLE η = 10.4
N294/N310	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.021 m η = 6.3	x: 0.34 m η = 9.7	η = 0.3	x: 0 m η = 1.1	x: 0 m η = 3.0	x: 1.021 m η = 0.2	x: 1.021 m η = 0.1	x: 0 m η = 1.0	x: 0 m η = 3.0	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 11.1	x: 0 m η = 10.9	CUMPLE η = 11.1
N293/N310	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.492 m η = 6.1	x: 0.492 m η = 8.1	x: 0.739 m η = 0.9	x: 0 m η = 1.4	x: 0 m η = 3.9	x: 0.985 m η = 0.4	x: 0.985 m η = 0.2	x: 0 m η = 1.4	x: 0 m η = 4.3	x: 0 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 0 m η = 11.1	x: 0.985 m η = 10.8	CUMPLE η = 11.1
N258/N311	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.017 m η = 4.7	x: 0 m η = 9.8	x: 0.678 m η = 0.5	x: 0 m η = 1.5	x: 1.017 m η = 3.1	x: 0.678 m η = 0.2	x: 1.017 m η = 0.1	x: 0 m η = 0.9	x: 1.017 m η = 3.3	x: 0 m η < 0.1	x: 1.017 m η = 0.1	N.P.[1]	x: 0 m η = 11.2	x: 0 m η = 11.0	CUMPLE η = 11.2
N257/N311	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.974 m η = 6.1	x: 0.974 m η = 5.4	η = 0.4	x: 0 m η = 1.1	x: 0.974 m η = 2.0	η = 0.2	x: 0.974 m η = 0.1	x: 0 m η = 1.2	x: 0.974 m η = 2.1	x: 0 m η < 0.1	x: 0.974 m η < 0.1	N.P.[1]	x: 0.974 m η = 8.4	x: 0.974 m η = 8.6	CUMPLE η = 8.6
N257/N312	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.021 m η = 5.1	x: 0 m η = 7.9	x: 0.851 m η = 1.0	x: 0 m η = 1.1	x: 1.021 m η = 6.3	x: 0.51 m η = 0.6	x: 1.021 m η = 0.1	x: 0 m η = 1.1	x: 1.021 m η = 6.7	x: 0 m η < 0.1	x: 1.021 m η = 0.5	x: 1.021 m η = 9.0	x: 0 m η = 9.6	x: 1.021 m η = 9.3	CUMPLE η = 9.6
N256/N312	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.985 m η = 5.3	x: 0 m η = 6.8	η = 0.2	x: 0 m η = 1.1	x: 0.985 m η = 10.2	x: 0.246 m η = 0.9	x: 0.985 m η = 0.1	x: 0 m η = 1.2	x: 0.985 m η = 10.2	x: 0 m η < 0.1	x: 0.985 m η = 1.0	x: 0.985 m η = 13.5	x: 0.985 m η = 10.0	x: 0.985 m η = 13.2	CUMPLE η = 13.5
N293/N313	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.026 m η = 6.3	x: 0 m η = 6.6	x: 1.026 m η = 0.3	x: 0 m η = 0.8	x: 1.026 m η = 7.8	x: 0.513 m η = 0.7	x: 1.026 m η = 0.1	x: 0 m η = 0.8	x: 1.026 m η = 7.9	x: 0 m η < 0.1	x: 1.026 m η = 0.6	x: 1.026 m η = 12.1	x: 0 m η = 8.8	x: 0 m η = 11.4	CUMPLE η = 12.1
N292/N313	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.007 m η = 4.3	x: 0.336 m η = 8.4	x: 0.168 m η = 0.4	x: 0 m η = 1.4	x: 0 m η = 6.2	x: 0.504 m η = 0.6	x: 1.007 m η = 0.1	x: 0 m η = 1.3	x: 0 m η = 6.3	x: 0 m η < 0.1	x: 0 m η = 0.4	x: 0 m η = 8.7	x: 1.007 m η = 10.6	x: 0 m η = 10.8	CUMPLE η = 10.8
N310/N313	$w/t \leq (w/t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 31.9	x: 0 m η = 1.2	x: 0.373 m η = 1.9	x: 1.12 m η = 4.7	x: 0.933 m η = 0.7	x: 1.12 m η = 0.1	x: 0.56 m η = 1.5	x: 1.12 m η = 5.2	x: 0.373 m η < 0.1	x: 1.12 m η = 0.3	N.P.[1]	x: 0.373 m η = 33.9	x: 0.373 m η = 34.2	CUMPLE η = 34.2
N314/N313	$w/t \leq (w/t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 29.5	η = 1.7	x: 1.122 m η = 2.1	x: 1.122 m η = 7.2	x: 0.374 m η = 1.1	x: 0 m η = 0.2	x: 1.122 m η = 2.2	x: 1.122 m η = 7.9	x: 1.122 m η < 0.1	x: 1.122 m η = 0.6	N.P.[1]	x: 1.122 m η = 31.8	x: 1.122 m η = 32.2	CUMPLE η = 32.2
N315/N314	$w/t \leq (w/t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 26.4	η = 0.3	x: 1.131 m η = 1.7	x: 0 m η = 3.7	x: 0.566 m η = 0.3	x: 0 m η = 0.1	x: 1.131 m η = 1.7	x: 0 m η = 3.9	x: 1.131 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 1.131 m η = 28.2	x: 1.131 m η = 28.6	CUMPLE η = 28.6
N316/N315	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.94 m η = 1.9	x: 0 m η = 21.4	x: 0.94 m η = 0.6	x: 1.128 m η = 2.3	x: 1.128 m η = 3.8	η = 0.2	x: 0 m η = 0.2	x: 1.128 m η = 2.3	x: 1.128 m η = 4.0	x: 1.128 m η = 0.1	x: 1.128 m η = 0.2	N.P.[1]	x: 1.128 m η = 23.9	x: 1.128 m η = 24.3	CUMPLE η = 24.3

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N317/N316	$w/t \leq (w/t)_{max}$ Cumple	x: 1.138 m η = 5.3	x: 0 m η = 14.4	η = 0.4	x: 1.138 m η = 1.7	x: 0 m η = 12.6	η = 1.9	x: 0 m η = 0.3	x: 0 m η = 1.2	x: 0 m η = 12.7	x: 1.138 m η < 0.1	x: 0 m η = 1.7	x: 0 m η = 9.2	x: 0 m η = 19.7	x: 0 m η = 22.1	CUMPLE η = 22.1
N318/N317	$w/t \leq (w/t)_{max}$ Cumple	x: 0.957 m η = 8.9	x: 0.957 m η = 13.9	x: 0.957 m η = 1.1	x: 0 m η = 2.0	x: 1.148 m η = 10.6	x: 1.148 m η = 1.5	x: 0 m η = 0.4	x: 0 m η = 2.1	x: 1.148 m η = 11.1	x: 0 m η < 0.1	x: 1.148 m η = 1.2	x: 1.148 m η = 14.8	x: 1.148 m η = 16.2	x: 1.148 m η = 17.0	CUMPLE η = 17.0
N319/N318	$w/t \leq (w/t)_{max}$ Cumple	x: 1.129 m η = 13.3	x: 0 m η = 12.3	η = 2.1	x: 0 m η = 1.5	x: 0 m η = 2.3	η = 0.1	x: 0 m η = 0.3	x: 0 m η = 1.7	x: 0 m η = 3.3	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 9.6	x: 1.129 m η = 14.0	x: 0 m η = 14.7	CUMPLE η = 14.7
N320/N319	$w/t \leq (w/t)_{max}$ Cumple	x: 1.12 m η = 17.7	x: 0 m η = 9.8	x: 0.187 m η = 0.6	x: 0 m η = 9.3	x: 1.12 m η = 4.7	x: 0.187 m η = 0.6	x: 0 m η = 1.1	x: 0 m η = 9.3	x: 1.12 m η = 5.0	x: 0 m η = 0.9	x: 1.12 m η = 0.2	x: 0 m η = 27.9	x: 0.187 m η = 11.2	x: 0 m η = 27.7	CUMPLE η = 27.9
N272/N320	$w/t \leq (w/t)_{max}$ Cumple	x: 0.902 m η = 21.4	x: 0 m η = 8.0	x: 0.677 m η = 5.9	x: 0.902 m η = 8.3	x: 0 m η = 15.2	η = 2.2	x: 0.902 m η = 1.6	x: 0.902 m η = 8.4	x: 0 m η = 17.8	x: 0.902 m η = 0.7	x: 0 m η = 3.2	x: 0 m η = 43.3	x: 0 m η = 21.0	x: 0 m η = 32.9	CUMPLE η = 43.3
N292/N314	$w/t \leq (w/t)_{max}$ Cumple	x: 1.034 m η = 6.1	x: 0 m η = 4.1	η = 0.2	x: 0 m η = 0.7	x: 1.034 m η = 3.8	η = 0.2	x: 0 m η = 0.1	x: 0 m η = 0.7	x: 1.034 m η = 3.8	x: 0 m η < 0.1	x: 1.034 m η = 0.1	N.P.[1]	x: 1.034 m η = 5.4	x: 1.034 m η = 8.9	CUMPLE η = 8.9
N291/N314	$w/t \leq (w/t)_{max}$ Cumple	x: 0.341 m η = 3.7	x: 0.341 m η = 8.9	x: 0.512 m η = 1.0	x: 0 m η = 1.6	x: 1.024 m η = 1.2	x: 0.512 m η = 0.1	x: 1.024 m η = 0.1	x: 0 m η = 1.3	x: 1.024 m η = 1.7	x: 0 m η < 0.1	x: 1.024 m η < 0.1	N.P.[1]	x: 1.024 m η = 10.1	x: 1.024 m η = 10.2	CUMPLE η = 10.2
N291/N315	$w/t \leq (w/t)_{max}$ Cumple	x: 1.013 m η = 6.9	x: 0.675 m η = 3.0	x: 1.013 m η = 0.6	x: 0 m η = 0.8	x: 0 m η = 1.7	x: 1.013 m η = 0.1	x: 0 m η = 0.1	x: 0 m η = 0.8	x: 0 m η = 1.9	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 3.7	x: 1.013 m η = 7.8	CUMPLE η = 7.8
N290/N315	$w/t \leq (w/t)_{max}$ Cumple	x: 0.167 m η = 2.0	x: 0 m η = 12.7	η = 0.7	x: 0 m η = 1.9	x: 0 m η = 0.9	x: 0.502 m η = 0.1	x: 1.003 m η = 0.2	x: 0 m η = 1.2	x: 0 m η = 1.3	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 14.6	x: 0 m η = 15.1	CUMPLE η = 15.1
N290/N316	$w/t \leq (w/t)_{max}$ Cumple	x: 1.011 m η = 10.9	x: 0.843 m η = 0.1	x: 0.337 m η = 0.7	x: 1.011 m η = 1.2	x: 1.011 m η = 1.0	x: 0 m η = 0.1	x: 0 m η = 0.1	x: 0 m η = 1.1	x: 1.011 m η = 1.3	x: 1.011 m η < 0.1	x: 1.011 m η < 0.1	N.P.[1]	x: 0 m η = 0.5	x: 1.011 m η = 12.4	CUMPLE η = 12.4
N289/N316	$w/t \leq (w/t)_{max}$ Cumple	x: 0.169 m η = 1.1	x: 0 m η = 17.0	x: 0.675 m η = 0.3	x: 0 m η = 2.2	x: 0 m η = 0.7	x: 1.012 m η < 0.1	x: 1.012 m η = 0.2	x: 1.012 m η = 1.2	x: 0 m η = 0.8	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 19.5	x: 0 m η = 19.7	CUMPLE η = 19.7
N289/N317	$w/t \leq (w/t)_{max}$ Cumple	x: 0.999 m η = 12.9	N.P.[2]	η = 0.6	x: 0 m η = 1.4	x: 0.999 m η = 6.3	x: 0.25 m η = 0.6	x: 0 m η = 0.2	x: 0 m η = 1.3	x: 0.999 m η = 6.6	x: 0 m η < 0.1	x: 0.999 m η = 0.4	x: 0 m η = 15.7	N.P.[3]	x: 0 m η = 14.6	CUMPLE η = 15.7
N288/N317	$w/t \leq (w/t)_{max}$ Cumple	x: 0 m η = 0.6	x: 0 m η = 21.4	η = 0.3	x: 0 m η = 2.4	x: 0 m η = 5.8	x: 0.993 m η = 0.5	x: 0.993 m η = 0.2	x: 0.993 m η = 1.4	x: 0 m η = 5.9	x: 0 m η = 0.1	x: 0 m η = 0.3	N.P.[1]	x: 0 m η = 24.0	x: 0 m η = 24.4	CUMPLE η = 24.4
N288/N318	$w/t \leq (w/t)_{max}$ Cumple	x: 0.968 m η = 15.5	N.P.[2]	x: 0.726 m η = 1.0	x: 0 m η = 2.1	x: 0 m η = 3.3	x: 0.726 m η = 0.3	x: 0 m η = 0.2	x: 0 m η = 1.7	x: 0 m η = 3.8	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	N.P.[3]	x: 0 m η = 18.1	CUMPLE η = 18.1
N287/N318	$w/t \leq (w/t)_{max}$ Cumple	N.P.[4]	x: 0 m η = 26.3	x: 0.706 m η = 0.4	x: 0.941 m η = 2.0	x: 0.941 m η = 7.8	x: 0 m η = 0.6	x: 0.941 m η = 0.2	x: 0.941 m η = 1.3	x: 0.941 m η = 8.0	x: 0.941 m η < 0.1	x: 0.941 m η = 0.6	N.P.[1]	x: 0.941 m η = 28.5	x: 0.941 m η = 28.7	CUMPLE η = 28.7
N287/N319	$w/t \leq (w/t)_{max}$ Cumple	x: 0.971 m η = 18.3	N.P.[2]	η = 0.1	x: 0 m η = 2.4	x: 0 m η = 5.2	η = 0.5	x: 0 m η = 0.3	x: 0 m η = 1.5	x: 0 m η = 5.2	x: 0 m η = 0.1	x: 0 m η = 0.3	N.P.[1]	N.P.[3]	x: 0 m η = 21.3	CUMPLE η = 21.3
N286/N319	$w/t \leq (w/t)_{max}$ Cumple	N.P.[4]	x: 0 m η = 29.9	η = 0.6	x: 0 m η = 5.5	x: 0.947 m η = 6.0	x: 0.71 m η = 0.5	x: 0.947 m η = 0.6	x: 0.947 m η = 2.7	x: 0.947 m η = 6.2	x: 0 m η = 0.3	x: 0.947 m η = 0.4	N.P.[1]	x: 0 m η = 36.2	x: 0 m η = 36.7	CUMPLE η = 36.7
N286/N320	$w/t \leq (w/t)_{max}$ Cumple	x: 0.981 m η = 16.6	N.P.[2]	η = 0.2	x: 0 m η = 4.1	x: 0.981 m η = 1.1	η < 0.1	x: 0 m η = 0.2	x: 0 m η = 2.2	x: 0.981 m η = 1.2	x: 0 m η = 0.2	x: 0.981 m η < 0.1	N.P.[1]	N.P.[3]	x: 0 m η = 21.7	CUMPLE η = 21.7
N274/N320	$w/t \leq (w/t)_{max}$ Cumple	N.P.[4]	x: 0 m η = 29.8	x: 0.603 m η = 2.1	x: 0 m η = 4.4	x: 0 m η = 14.1	x: 0.603 m η = 1.4	x: 0.804 m η = 0.6	x: 0 m η = 4.4	x: 0 m η = 15.0	x: 0 m η = 0.2	x: 0 m η = 2.3	N.P.[1]	x: 0 m η = 33.8	x: 0.804 m η = 33.5	CUMPLE η = 33.8
N256/N321	$w/t \leq (w/t)_{max}$ Cumple	x: 1.026 m η = 5.9	x: 0 m η = 6.0	x: 0.513 m η = 0.5	x: 0 m η = 0.8	x: 1.026 m η = 6.5	x: 0.684 m η = 0.6	x: 1.026 m η = 0.1	x: 0 m η = 0.8	x: 1.026 m η = 6.6	x: 0 m η < 0.1	x: 1.026 m η = 0.4	x: 1.026 m η = 9.5	x: 0 m η = 6.9	x: 1.026 m η = 8.9	CUMPLE η = 9.5
N255/N321	$w/t \leq (w/t)_{max}$ Cumple	x: 0.504 m η = 4.2	x: 0 m η = 7.9	η = 0.2	x: 0 m η = 1.3	x: 0 m η = 5.8	x: 0.671 m η = 0.5	x: 1.007 m η = 0.1	x: 0 m η = 1.4	x: 0 m η = 5.9	x: 0 m η < 0.1	x: 0 m η = 0.3	x: 0 m η = 7.8	x: 0 m η = 9.3	x: 0 m η = 9.8	CUMPLE η = 9.8
N255/N322	$w/t \leq (w/t)_{max}$ Cumple	x: 1.034 m η = 5.9	x: 0 m η = 4.0	η = 0.7	x: 0 m η = 0.7	x: 0 m η = 1.3	x: 0.172 m η = 0.1	x: 0 m η = 0.1	x: 0 m η = 0.7	x: 0 m η = 1.6	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 5.3	x: 0 m η = 7.0	CUMPLE η = 7.0
N312/N321	$w/t \leq (w/t)_{max}$ Cumple	N.P.[4]	x: 0 m η = 30.9	η = 2.1	x: 0.373 m η = 1.8	x: 1.12 m η = 4.5	x: 0.933 m η = 0.7	x: 1.12 m η = 0.1	x: 0.373 m η = 1.8	x: 1.12 m η = 5.5	x: 0.373 m η < 0.1	x: 1.12 m η = 0.3	N.P.[1]	x: 0.56 m η = 33.0	x: 0.373 m η = 33.2	CUMPLE η = 33.2
N322/N321	$w/t \leq (w/t)_{max}$ Cumple	N.P.[4]	x: 0 m η = 29.2	η = 0.3	x: 1.122 m η = 2.1	x: 1.122 m η = 7.4	η = 1.2	x: 0 m η = 0.2	x: 1.122 m η = 2.3	x: 1.122 m η = 7.5	x: 1.122 m η = 0.1	x: 1.122 m η = 0.6	N.P.[1]	x: 1.122 m η = 31.7	x: 1.122 m η = 31.8	CUMPLE η = 31.8
N254/N322	$w/t \leq (w/t)_{max}$ Cumple	x: 1.024 m η = 3.6	x: 0 m η = 8.7	x: 0.171 m η = 0.3	x: 0 m η = 1.6	x: 1.024 m η = 3.3	x: 0.171 m η = 0.2	x: 1.024 m η = 0.1	x: 1.024 m η = 1.1	x: 1.024 m η = 3.5	x: 0 m η < 0.1	x: 1.024 m η = 0.1	N.P.[1]	x: 0 m η = 9.9	x: 1.024 m η = 10.0	CUMPLE η = 10.0
N323/N322	$w/t \leq (w/t)_{max}$ Cumple	N.P.[4]	x: 0 m η = 26.2	x: 0.189 m η = 1.0	x: 1.131 m η = 1.7	x: 0 m η = 3.7	x: 0.189 m η = 0.3	x: 0 m η = 0.1	x: 1.131 m η = 1.8	x: 0 m η = 4.1	x: 1.131 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 1.131 m η = 28.2	x: 1.131 m η = 28.3	CUMPLE η = 28.3
N254/N323	$w/t \leq (w/t)_{max}$ Cumple	x: 1.013 m η = 6.8	x: 0 m η = 2.9	η = 0.1	x: 0 m η = 0.9	x: 1.013 m η = 3.2	η = 0.3	x: 0 m η = 0.1	x: 0 m η = 0.9	x: 1.013 m η = 3.2	x: 0 m η < 0.1	x: 1.013 m η = 0.1	N.P.[1]	x: 0 m η = 3.6	x: 1.013 m η = 7.6	CUMPLE η = 7.6
N253/N323	$w/t \leq (w/t)_{max}$ Cumple	x: 1.003 m η = 2.1	x: 0 m η = 12.5	x: 0.167 m η = 0.3	x: 0 m η = 1.9	x: 1.003 m η = 3.6	x: 0.334 m η = 0.3	x: 1.003 m η = 0.2	x: 1.003 m η = 1.1	x: 1.003 m η = 3.7	x: 0 m η < 0.1	x: 1.003 m η = 0.1	N.P.[1]	x: 0 m η = 14.4	x: 0 m η = 14.8	CUMPLE η = 14.8
N253/N324	$w/t \leq (w/t)_{max}$ Cumple	x: 1.011 m η = 10.7	x: 0 m η = 0.2	x: 0.169 m η = 0.8	x: 1.011 m η = 1.2	x: 0 m η = 0.6	x: 0.169 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 1.1	x: 0 m η = 0.9	x: 1.011 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 1.2	x: 1.011 m η = 12.2	CUMPLE η = 12.2
N324/N323	$w/t \leq (w/t)_{max}$ Cumple	x: 1.128 m η = 2.2	x: 0 m η = 21.3	x: 0.752 m η = 1.2	x: 1.128 m η = 2.3	x: 1.128 m η = 3.8	η = 0.2	x: 0 m η = 0.2	x: 1.128 m η = 1.4	x: 1.128 m η = 4.4	x: 1.128 m η = 0.1	x: 1.128 m η = 0.2	N.P.[1]	x: 1.128 m η = 23.7	x: 1.128 m η = 24.2	CUMPLE η = 24.2
N252/N324	$w/t \leq (w/t)_{max}$ Cumple	x: 0.169 m η = 1.2	x: 0 m η = 16.7	η = 0.2	x: 0 m η = 2.2	x: 1.012 m η = 1.0	η < 0.1	x: 1.012 m η = 0.2	x: 1.012 m η = 1.2	x: 1.012 m η = 1.1	x: 0 m η < 0.1	x: 1.012 m η < 0.1	N.P.[1]	x: 0 m η = 19.1	x: 0 m η = 19.5	CUMPLE η = 19.5
N325/N324	$w/t \leq (w/t)_{max}$ Cumple	x: 0.948 m η = 5.4	x: 0 m η = 14.5	x: 1.138 m η = 0.6	x: 1.138 m η = 1.7	x: 0 m η = 12.5	x: 1.138 m η = 1.8	x: 0 m η = 0.3	x: 0 m η = 1.1	x: 0 m η = 12.7	x: 1.138 m η < 0.1	x: 0 m η = 1.7	x: 0 m η = 9.4	x: 0 m η = 18.5	x: 0 m η = 20.7	CUMPLE η = 20.7
N252/N325	$w/t \leq (w/t)_{max}$ Cumple	x: 0.999 m η = 12.8	N.P.[2]	η = 0.5	x: 0 m η = 1.4	x: 0.999 m η = 7.0	η = 0.7	x: 0 m η = 0.2	x: 0 m η = 1.4	x: 0.999 m η = 7.2	x: 0 m η < 0.1	x: 0.999 m η = 0.5	x: 0.999 m η = 16.2	N.P.[3]	x: 0.999 m η = 14.9	CUMPLE η = 16.2
N251/N325	$w/t \leq (w/t)_{max}$ Cumple	x: 0 m η = 0.6	x: 0 m η = 21.0	x: 0.993 m η = 0.2	x: 0 m η = 2.3	x: 0 m η = 6.0	η = 0.6	x: 0.993 m η = 0.2	x: 0.993 m η = 1.3	x: 0 m η = 6.1	x: 0 m η = 0.1	x: 0 m η = 0.4	N.P.[1]	x: 0 m η = 23.7	x: 0 m η = 23.9	CUMPLE η = 23.9
N251/N326	$w/t \leq (w/t)_{max}$ Cumple	x: 0.968 m η = 15.3	N.P.[2]	η = 1.0	x: 0 m η = 2.1	x: 0 m η = 3.2	η = 0.2	x: 0 m η = 0.2	x: 0 m η = 1.6	x: 0 m η = 3.6	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	N.P.[3]	x: 0 m η = 17.8	CUMPLE η = 17.8
N326/N325	$w/t \leq (w/t)_{max}$ Cumple	x: 1.148 m η = 9.1	x: 0 m η = 13.8	η = 0.9	x: 0 m η = 2.0	x: 1.148 m η = 10.4	η = 1.5	x: 0 m η = 0.4	x: 0 m η = 2.0	x: 1.148 m η = 10.7	x: 0 m η < 0.1	x: 1.148 m η = 1.2	x: 0 m η = 11.5	x: 0.957 m η = 15.0	x: 0.766 m η = 15.1	CUMPLE η = 15.1
N250/N326	$w/t \leq (w/t)_{max}$ Cumple	N.P.[4]	x: 0 m η = 25.9	η = 0.4	x: 0.941 m η = 1.9	x: 0.941 m η = 7.4	x: 0.941 m η = 0.6	x: 0.941 m η = 0.2	x: 0.941 m η = 1.2	x: 0.941 m η = 7.6	x: 0.941 m η < 0.1	x: 0.941 m η = 0.6	N.P.[1]	x: 0.941 m η = 28.2	x: 0.941 m η = 28.3	CUMPLE η = 28.3
N327/N326	$w/t \leq (w/t)_{max}$ Cumple	x: 1.129 m η = 13.4	x: 0 m η = 12.2	η = 1.3	x: 1.129 m η = 1.4	x: 0 m η = 2.3	η < 0.1	x: 0 m η = 0.3	x: 0 m η = 1.5	x: 0 m η = 2.9	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 8.0	x: 1.129 m η = 13.8	x: 0 m η = 14.8	CUMPLE η = 14.8

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2018))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N250/N327	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.971 m η = 18.0	N.P.[2]	x: 0.485 m η = 0.3	x: 0 m η = 2.4	x: 0.971 m η = 6.1	x: 0.485 m η = 0.6	x: 0 m η = 0.3	x: 0 m η = 1.6	x: 0.971 m η = 6.2	x: 0 m η = 0.1	x: 0.971 m η = 0.4	x: 0 m η = 16.2	N.P.[3]	x: 0 m η = 21.0	CUMPLE η = 21.0
N249/N327	$w/t \leq (w/t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 29.5	x: 0.71 m η = 0.8	x: 0 m η = 5.4	x: 0.947 m η = 7.5	x: 0.71 m η = 0.6	x: 0.947 m η = 0.6	x: 0.947 m η = 2.7	x: 0.947 m η = 7.9	x: 0 m η = 0.3	x: 0.947 m η = 0.6	N.P.[1]	x: 0 m η = 35.7	x: 0 m η = 36.3	CUMPLE η = 36.3
N328/N327	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.12 m η = 17.7	x: 0 m η = 9.7	η = 0.2	x: 0 m η = 9.3	x: 1.12 m η = 4.7	x: 0.373 m η = 0.6	x: 0 m η = 1.1	x: 0 m η = 9.4	x: 1.12 m η = 4.8	x: 0 m η = 0.9	x: 1.12 m η = 0.2	x: 0 m η = 28.3	x: 0 m η = 11.3	x: 0 m η = 27.8	CUMPLE η = 28.3
N249/N328	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.981 m η = 16.4	N.P.[2]	x: 0.245 m η = 0.4	x: 0 m η = 4.0	x: 0.981 m η = 3.9	x: 0.245 m η = 0.2	x: 0 m η = 0.2	x: 0 m η = 2.0	x: 0.981 m η = 4.0	x: 0 m η = 0.2	x: 0.981 m η = 0.2	N.P.[1]	N.P.[3]	x: 0 m η = 21.4	CUMPLE η = 21.4
N238/N328	$w/t \leq (w/t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 29.5	x: 0.603 m η = 2.2	x: 0 m η = 4.3	x: 0 m η = 12.5	x: 0.804 m η = 1.0	x: 0.804 m η = 0.5	x: 0 m η = 4.4	x: 0 m η = 13.4	x: 0 m η = 0.2	x: 0 m η = 1.8	N.P.[1]	x: 0.804 m η = 33.0	x: 0.804 m η = 33.3	CUMPLE η = 33.3
N235/N328	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.902 m η = 21.4	x: 0.451 m η = 7.7	η = 4.7	x: 0.902 m η = 8.3	x: 0 m η = 15.2	x: 0.677 m η = 2.3	x: 0.902 m η = 1.6	x: 0.902 m η = 7.7	x: 0 m η = 17.3	x: 0.902 m η = 0.7	x: 0 m η = 3.0	x: 0 m η = 33.7	x: 0.226 m η = 11.0	x: 0.902 m η = 31.8	CUMPLE η = 33.7
N313/N321	$w/t \leq (w/t)_{Máx}$ Cumple	η = 0.7	η = 1.3	η = 0.2	x: 0.3 m η = 7.5	x: 0.3 m η = 12.4	η = 4.2	x: 0 m η = 2.0	x: 0.3 m η = 7.6	x: 0.3 m η = 12.4	x: 0.3 m η = 0.6	x: 0.3 m η = 1.7	x: 0.3 m η = 22.0	x: 0.3 m η = 16.7	x: 0.3 m η = 16.1	CUMPLE η = 22.0
N314/N322	$w/t \leq (w/t)_{Máx}$ Cumple	η = 2.2	η = 2.5	x: 0 m η = 0.3	x: 0 m η = 5.0	x: 0 m η = 19.5	x: 0.3 m η = 6.4	x: 0 m η = 0.4	x: 0 m η = 5.1	x: 0 m η = 19.6	x: 0 m η = 0.3	x: 0 m η = 4.3	x: 0 m η = 32.7	x: 0 m η = 27.2	x: 0 m η = 27.6	CUMPLE η = 32.7
N315/N323	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.3 m η = 1.4	x: 0.3 m η = 1.6	η = 0.2	x: 0 m η = 7.6	x: 0.3 m η = 3.6	η = 1.2	x: 0 m η = 1.5	x: 0 m η = 7.7	x: 0.3 m η = 3.6	x: 0 m η = 0.6	x: 0.3 m η = 0.1	x: 0 m η = 12.4	x: 0 m η = 10.4	x: 0 m η = 11.1	CUMPLE η = 12.4
N316/N324	$w/t \leq (w/t)_{Máx}$ Cumple	η = 1.0	η = 1.2	η = 0.1	x: 0.3 m η = 10.5	x: 0 m η = 26.1	x: 0.3 m η = 8.7	x: 0 m η = 3.1	x: 0.3 m η = 10.5	x: 0 m η = 26.1	x: 0.3 m η = 1.2	x: 0 m η = 7.6	x: 0.3 m η = 45.9	x: 0.3 m η = 37.2	x: 0.3 m η = 35.6	CUMPLE η = 45.9
N317/N325	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.15 m η = 2.3	x: 0.15 m η = 2.8	η = 0.2	x: 0 m η = 5.2	x: 0 m η = 10.8	x: 0.3 m η = 3.6	x: 0 m η = 1.6	x: 0 m η = 5.3	x: 0 m η = 10.9	x: 0 m η = 0.3	x: 0 m η = 1.3	x: 0 m η = 22.5	x: 0 m η = 18.1	x: 0 m η = 17.2	CUMPLE η = 22.5
N318/N326	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.3 m η = 3.8	x: 0.3 m η = 4.1	x: 0.15 m η = 0.6	x: 0 m η = 10.8	x: 0.3 m η = 10.8	x: 0.15 m η = 3.6	x: 0.3 m η = 3.6	x: 0 m η = 11.1	x: 0.3 m η = 11.0	x: 0 m η = 1.4	x: 0.3 m η = 1.3	x: 0 m η = 31.3	x: 0 m η = 25.8	x: 0 m η = 22.9	CUMPLE η = 31.3
N319/N327	$w/t \leq (w/t)_{Máx}$ Cumple	η = 2.8	η = 3.2	x: 0.3 m η = 0.8	x: 0 m η = 2.5	x: 0.3 m η = 9.7	η = 3.1	x: 0 m η = 0.4	x: 0 m η = 2.8	x: 0.3 m η = 10.0	x: 0 m η = 0.1	x: 0.3 m η = 1.1	x: 0 m η = 17.5	x: 0 m η = 14.9	x: 0.3 m η = 15.3	CUMPLE η = 17.5
N320/N328	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.15 m η = 1.8	x: 0.15 m η = 1.8	x: 0 m η = 0.3	x: 0.3 m η = 8.0	x: 0.3 m η = 31.1	x: 0.15 m η = 10.0	x: 0 m η = 1.8	x: 0.3 m η = 8.1	x: 0.3 m η = 31.2	x: 0.3 m η = 0.7	x: 0.3 m η = 10.7	x: 0.3 m η = 50.4	x: 0.3 m η = 40.8	x: 0.3 m η = 41.7	CUMPLE η = 50.4
N329/N330	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.41 m η = 22.6	x: 1.41 m η = 36.2	x: 1.41 m η = 1.8	x: 0 m η = 1.9	x: 1.41 m η = 18.8	x: 1.41 m η = 1.7	x: 0 m η = 0.1	x: 0 m η = 2.7	x: 1.41 m η = 19.6	x: 0 m η = 0.1	x: 1.41 m η = 3.9	x: 1.41 m η = 49.5	x: 1.41 m η = 59.1	x: 1.41 m η = 59.7	CUMPLE η = 59.7
N330/N331	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0 m η = 14.3	x: 0 m η = 14.2	x: 0 m η = 0.7	x: 1.167 m η = 1.5	x: 0 m η = 37.5	x: 0.467 m η = 4.7	x: 0 m η = 0.1	x: 1.4 m η = 1.3	x: 0 m η = 37.8	x: 1.167 m η < 0.1	x: 0 m η = 14.5	x: 0 m η = 63.1	x: 0 m η = 52.5	x: 0 m η = 61.1	CUMPLE η = 63.1
N331/N332	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.35 m η = 13.5	x: 0 m η = 4.1	x: 0 m η = 1.2	x: 1.35 m η = 4.3	x: 1.35 m η = 53.2	η = 6.1	x: 0 m η = 0.3	x: 1.35 m η = 4.4	x: 1.35 m η = 53.7	x: 1.35 m η = 0.2	x: 1.35 m η = 29.2	x: 1.35 m η = 75.5	x: 0 m η = 9.0	x: 1.35 m η = 72.0	CUMPLE η = 75.5
N332/N333	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.79 m η = 16.6	x: 0 m η = 6.4	η = 7.0	x: 0 m η = 10.8	x: 0 m η = 50.7	x: 0.592 m η = 10.1	x: 0.79 m η = 2.2	x: 0 m η = 10.8	x: 0 m η = 53.8	x: 0 m η = 1.2	x: 0 m η = 29.9	x: 0 m η = 81.5	x: 0 m η = 10.9	x: 0 m η = 70.7	CUMPLE η = 81.5
N332/N334	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.179 m η = 1.9	x: 0.179 m η = 4.0	η = 2.1	x: 1.073 m η = 9.7	x: 1.073 m η = 14.5	η = 1.9	x: 1.073 m η = 1.4	x: 1.073 m η = 9.8	x: 1.073 m η = 15.4	x: 1.073 m η = 1.0	x: 1.073 m η = 2.4	x: 1.073 m η = 27.6	x: 1.073 m η = 22.3	x: 1.073 m η = 22.1	CUMPLE η = 27.6
N329/N337	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.755 m η = 24.3	x: 0.566 m η = 56.8	x: 0.189 m η = 5.1	x: 0.755 m η = 11.3	x: 0 m η = 20.3	x: 0.189 m η = 1.8	x: 0.755 m η = 1.2	x: 0.755 m η = 13.5	x: 0 m η = 22.5	x: 0.755 m η = 1.8	x: 0 m η = 5.1	x: 0 m η = 15.3	x: 0.755 m η = 65.2	x: 0.755 m η = 64.3	CUMPLE η = 65.2
N337/N330	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.424 m η = 28.7	x: 0.424 m η = 20.3	x: 0.847 m η = 0.8	x: 0 m η = 10.6	x: 0 m η = 57.1	x: 0.635 m η = 6.6	x: 0 m η = 0.9	x: 0 m η = 10.6	x: 0 m η = 57.4	x: 0 m η = 1.1	x: 0 m η = 33.4	x: 0 m η = 86.8	x: 0 m η = 28.4	x: 0 m η = 82.9	CUMPLE η = 86.8
N330/N336	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.869 m η = 10.2	x: 0 m η = 24.6	x: 0.652 m η = 1.6	x: 0.869 m η = 4.0	x: 0 m η = 7.7	η = 0.6	x: 0 m η = 0.4	x: 0.869 m η = 4.0	x: 0 m η = 8.3	x: 0.869 m η = 0.2	x: 0 m η = 0.7	N.P.[1]	x: 0.869 m η = 29.0	x: 0.869 m η = 29.5	CUMPLE η = 29.5
N336/N331	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.983 m η = 15.6	x: 0 m η = 11.9	η = 0.4	x: 0 m η = 2.9	x: 0 m η = 28.7	η = 2.9	x: 0.983 m η = 0.3	x: 0 m η = 2.9	x: 0 m η = 28.9	x: 0 m η = 0.1	x: 0 m η = 8.4	x: 0 m η = 43.2	x: 0 m η = 14.8	x: 0 m η = 41.7	CUMPLE η = 43.2
N331/N335	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.685 m η = 6.5	x: 0.685 m η = 16.8	x: 0.514 m η = 0.8	x: 0 m η = 3.1	x: 0 m η = 1.4	η < 0.1	x: 0 m η = 0.3	x: 0 m η = 2.7	x: 0 m η = 1.7	x: 0 m η = 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 19.8	x: 0 m η = 20.1	CUMPLE η = 20.1
N335/N332	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0 m η = 9.4	x: 0 m η = 8.1	x: 0.928 m η = 4.9	x: 0.928 m η = 1.5	x: 1.114 m η = 28.9	x: 0.371 m η = 2.2	x: 0 m η = 0.1	x: 1.114 m η = 3.1	x: 1.114 m η = 31.0	x: 1.114 m η = 0.1	x: 1.114 m η = 9.6	x: 1.114 m η = 48.8	x: 1.114 m η = 38.7	x: 1.114 m η = 43.4	CUMPLE η = 48.8
N334/N333	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.731 m η = 12.7	x: 0 m η = 57.8	x: 1.096 m η = 3.9	x: 0 m η = 3.9	x: 0 m η = 9.4	x: 0.548 m η = 0.5	x: 0 m η = 0.4	x: 0 m η = 4.1	x: 0 m η = 11.1	x: 0 m η = 0.2	x: 0 m η = 1.2	N.P.[1]	x: 0 m η = 63.3	x: 0 m η = 62.6	CUMPLE η = 63.3
N342/N338	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.41 m η = 22.3	x: 1.41 m η = 35.7	η = 1.8	x: 0 m η = 1.9	x: 1.41 m η = 18.2	x: 1.234 m η = 1.6	x: 0 m η = 0.1	x: 0 m η = 2.6	x: 1.41 m η = 19.0	x: 0 m η = 0.1	x: 1.41 m η = 3.6	x: 1.41 m η = 48.4	x: 1.41 m η = 57.8	x: 1.41 m η = 58.4	CUMPLE η = 58.4
N338/N339	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.233 m η = 15.1	x: 0 m η = 15.1	x: 1.4 m η = 0.8	x: 0.933 m η = 1.5	x: 0 m η = 37.3	x: 0.233 m η = 4.8	x: 0 m η = 0.1	x: 1.4 m η = 1.3	x: 0 m η = 37.6	x: 0.7 m η < 0.1	x: 0 m η = 14.4	x: 0 m η = 63.8	x: 0 m η = 54.8	x: 0 m η = 61.7	CUMPLE η = 63.8
N339/N340	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.35 m η = 13.7	x: 0 m η = 4.3	η = 1.0	x: 1.35 m η = 4.4	x: 1.35 m η = 53.1	x: 0 m η = 6.3	x: 0 m η = 0.3	x: 1.35 m η = 4.5	x: 1.35 m η = 53.5	x: 1.35 m η = 0.2	x: 1.35 m η = 29.0	x: 1.35 m η = 76.1	x: 1.35 m η = 6.8	x: 1.35 m η = 72.4	CUMPLE η = 76.1
N340/N341	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.79 m η = 16.8	x: 0 m η = 6.5	η = 6.7	x: 0 m η = 10.4	x: 0 m η = 51.4	x: 0.592 m η = 10.1	x: 0.79 m η = 1.9	x: 0 m η = 10.4	x: 0 m η = 54.4	x: 0 m η = 1.1	x: 0 m η = 30.6	x: 0 m η = 81.6	x: 0 m η = 10.7	x: 0 m η = 71.3	CUMPLE η = 81.6
N342/N346	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.755 m η = 25.6	x: 0.755 m η = 58.2	x: 0.189 m η = 5.0	x: 0.755 m η = 11.5	x: 0 m η = 19.7	x: 0.378 m η = 1.8	x: 0.755 m η = 1.2	x: 0.755 m η = 13.7	x: 0 m η = 21.8	x: 0.755 m η = 1.9	x: 0 m η = 4.8	x: 0 m η = 16.2	x: 0.755 m η = 67.1	x: 0.755 m η = 66.0	CUMPLE η = 67.1
N346/N338	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.424 m η = 29.4	x: 0.424 m η = 21.2	x: 0.424 m η = 0.8	x: 0 m η = 10.7	x: 0 m η = 56.0	x: 0.635 m η = 6.5	x: 0 m η = 0.9	x: 0 m η = 10.8	x: 0 m η = 56.4	x: 0 m η = 1.2	x: 0 m η = 32.2	x: 0 m η = 87.0	x: 0 m η = 29.8	x: 0 m η = 82.7	CUMPLE η = 87.0
N338/N345	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.869 m η = 10.7	x: 0 m η = 25.2	x: 0.869 m η = 1.5	x: 0.869 m η = 4.1	x: 0 m η = 6.7	η = 0.5	x: 0 m η = 0.5	x: 0.869 m η = 4.1	x: 0 m η = 7.3	x: 0.869 m η = 0.2	x: 0 m η = 0.5	N.P.[1]	x: 0.869 m η = 29.7	x: 0.869 m η = 30.2	CUMPLE η = 30.2
N345/N339	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.983 m η = 15.9	x: 0 m η = 12.4	x: 0.492 m η = 0.1	x: 0 m η = 3.0	x: 0.983 m η = 29.7	x: 0.492 m η = 3.0	x: 0.983 m η = 0.3	x: 0 m η = 3.0	x: 0.983 m η = 29.8	x: 0 m η = 0.1	x: 0.983 m η = 9.0	x: 0.983 m η = 43.5	x: 0 m η = 15.7	x: 0.983 m η = 42.2	CUMPLE η = 43.5
N339/N344	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.685 m η = 6.7	x: 0.685 m η = 17.0	x: 0.514 m η = 0.3	x: 0 m η = 3.0	x: 0 m η = 1.6	η < 0.1	x: 0 m η = 0.3	x: 0 m η = 2.7	x: 0 m η = 1.8	x: 0 m η = 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 20.1	x: 0 m η = 20.2	CUMPLE η = 20.2
N344/N340	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0 m η = 9.4	x: 0 m η = 8.1	η = 4.7	x: 1.114 m η = 1.6	x: 1.114 m η = 28.5	x: 0.928 m η = 2.2	x: 0 m η = 0.1	x: 1.114 m η = 3.1	x: 1.114 m η = 30.5	x: 1.114 m η = 0.1	x: 1.114 m η = 9.4	x: 1.114 m η = 48.1	x: 1.114 m η = 38.1	x: 1.114 m η = 42.9	CUMPLE η = 48.1
N340/N343	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.073 m η = 2.0	x: 0 m η = 4.0	η = 2.5	x: 1.073 m η = 8.6	x: 1.073 m η = 14.8	x: 0.715 m η = 2.0	x: 1.073 m η = 1.2	x: 1.073 m η = 8.6	x: 1.073 m η = 15.8	x: 1.073 m η = 0.8	x: 1.073 m η = 2.6	x: 1.073 m η = 28.1	x: 1.073 m η = 22.6	x: 1.073 m η = 22.5	CUMPLE η = 28.1
N343/N341	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.365 m η = 13.8	x: 0 m η = 61.9	x: 1.096 m η = 4.2	x: 0 m η = 3.6	x: 0 m η = 10.3	x: 1.096 m η = 0.6	x: 0 m η = 0.4	x: 0 m η = 4.1	x: 0 m η = 12.1	x: 0 m η = 0.2	x: 0 m η = 1.5	N.P.[1]	x: 0 m η = 67.2	x: 0 m η = 66.4	CUMPLE η = 67.2



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N334/N347	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.617 m η = 6.6	x: 0 m η = 26.5	x: 0.617 m η = 4.8	x: 0 m η = 17.6	x: 0 m η = 6.2	η = 0.9	x: 0 m η = 3.3	x: 0 m η = 17.6	x: 0 m η = 8.3	x: 0 m η = 3.2	x: 0 m η = 0.7	x: 0 m η = 9.2	x: 0 m η = 44.6	x: 0 m η = 46.5	CUMPLE η = 46.5
N347/N348	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0 m η = 8.7	x: 0 m η = 20.4	x: 0.721 m η = 2.0	x: 1.081 m η = 1.8	x: 0 m η = 4.2	x: 0.721 m η = 0.7	x: 1.081 m η = 0.3	x: 1.081 m η = 1.8	x: 0 m η = 5.1	x: 1.081 m η < 0.1	x: 0 m η = 0.3	x: 1.081 m η = 10.4	x: 1.081 m η = 22.3	x: 1.081 m η = 22.6	CUMPLE η = 22.6
N348/N349	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.907 m η = 10.2	x: 0.907 m η = 16.1	x: 1.088 m η = 1.8	x: 0 m η = 2.2	x: 1.088 m η = 0.8	x: 0.363 m η = 0.1	x: 0 m η = 0.3	x: 0 m η = 2.3	x: 1.088 m η = 1.6	x: 0 m η = 0.1	x: 1.088 m η < 0.1	x: 0.725 m η = 11.6	x: 0 m η = 18.5	x: 0 m η = 18.9	CUMPLE η = 18.9
N349/N350	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.08 m η = 10.4	x: 0 m η = 11.6	x: 0.9 m η = 0.7	x: 0 m η = 1.1	x: 0 m η = 3.1	η = 0.4	x: 0 m η = 0.2	x: 0 m η = 1.2	x: 0 m η = 3.4	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 7.3	x: 0 m η = 12.9	x: 0 m η = 13.0	CUMPLE η = 13.0
N350/N351	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.085 m η = 10.8	x: 1.085 m η = 8.3	η = 0.2	x: 1.085 m η = 1.7	x: 1.085 m η = 4.5	x: 1.085 m η = 0.7	x: 0 m η = 0.2	x: 1.085 m η = 1.7	x: 1.085 m η = 4.5	x: 1.085 m η < 0.1	x: 1.085 m η = 0.2	x: 0.723 m η = 12.4	x: 0 m η = 9.3	x: 0.723 m η = 12.2	CUMPLE η = 12.4
N351/N352	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.082 m η = 10.9	x: 0.902 m η = 5.1	η = 0.4	x: 1.082 m η = 1.7	x: 0 m η = 1.7	η = 0.1	x: 0 m η = 0.1	x: 1.082 m η = 1.8	x: 0 m η = 1.9	x: 1.082 m η < 0.1	x: 0 m η < 0.1	x: 1.082 m η = 13.3	x: 0 m η = 5.8	x: 1.082 m η = 13.0	CUMPLE η = 13.3
N352/N353	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.085 m η = 13.4	x: 0.904 m η = 2.3	x: 0.542 m η = 0.8	x: 0.904 m η = 1.8	x: 0 m η = 1.0	x: 0.362 m η = 0.1	x: 0 m η = 0.1	x: 0.904 m η = 1.8	x: 0 m η = 1.3	x: 0.904 m η < 0.1	x: 0 m η < 0.1	x: 1.085 m η = 15.9	x: 0 m η = 2.9	x: 0.904 m η = 15.6	CUMPLE η = 15.9
N353/N354	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.081 m η = 15.2	x: 0 m η = 0.5	η = 0.5	x: 1.081 m η = 2.1	x: 0 m η = 1.0	x: 0.36 m η = 0.2	x: 0 m η = 0.1	x: 1.081 m η = 2.1	x: 1.081 m η = 1.1	x: 1.081 m η < 0.1	x: 1.081 m η < 0.1	x: 1.081 m η = 18.1	x: 0 m η = 1.7	x: 1.081 m η = 17.8	CUMPLE η = 18.1
N355/N354	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.08 m η = 15.8	x: 0 m η = 0.1	x: 0.72 m η = 1.1	x: 0.72 m η = 2.1	x: 1.08 m η = 1.9	x: 0.36 m η = 0.3	x: 0 m η = 0.1	x: 0.72 m η = 1.5	x: 1.08 m η = 2.3	x: 0.72 m η < 0.1	x: 1.08 m η = 0.1	x: 0.72 m η = 18.5	x: 0 m η = 2.9	x: 0.72 m η = 18.4	CUMPLE η = 18.5
N356/N355	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.084 m η = 14.8	N.P.[2]	η = 1.5	x: 0.903 m η = 2.0	x: 0 m η = 1.7	η = 0.3	x: 0 m η = 0.1	x: 0.903 m η = 2.0	x: 0 m η = 1.9	x: 0.903 m η < 0.1	x: 0 m η < 0.1	x: 1.084 m η = 17.5	N.P.[3]	x: 0.903 m η = 17.3	CUMPLE η = 17.5
N357/N356	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.08 m η = 12.5	x: 0 m η = 2.5	x: 0.72 m η = 0.8	x: 1.08 m η = 1.9	x: 1.08 m η = 2.6	x: 0.72 m η = 0.3	x: 0 m η = 0.1	x: 1.08 m η = 1.9	x: 1.08 m η = 3.0	x: 1.08 m η < 0.1	x: 1.08 m η = 0.1	x: 1.08 m η = 15.1	x: 0 m η = 5.1	x: 1.08 m η = 14.8	CUMPLE η = 15.1
N358/N357	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.18 m η = 10.3	x: 0.18 m η = 6.4	η = 0.4	x: 1.083 m η = 1.9	x: 0 m η = 2.9	x: 1.083 m η = 0.5	x: 0 m η = 0.2	x: 1.083 m η = 1.9	x: 0 m η = 3.0	x: 1.083 m η < 0.1	x: 0 m η = 0.1	x: 0.18 m η = 13.3	x: 0.18 m η = 8.3	x: 0.18 m η = 12.2	CUMPLE η = 13.3
N359/N358	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.087 m η = 9.9	x: 0 m η = 9.8	η = 0.8	x: 1.087 m η = 1.3	x: 0 m η = 2.9	η = 0.3	x: 0 m η = 0.2	x: 1.087 m η = 1.4	x: 0 m η = 3.2	x: 1.087 m η < 0.1	x: 0 m η = 0.1	x: 0.906 m η = 12.0	x: 0 m η = 11.5	x: 0.724 m η = 11.4	CUMPLE η = 12.0
N360/N359	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.904 m η = 9.4	x: 0.904 m η = 13.9	η = 1.4	x: 0 m η = 2.0	x: 0 m η = 1.4	x: 1.085 m η = 0.2	x: 0 m η = 0.3	x: 0 m η = 2.2	x: 0 m η = 2.0	x: 0 m η < 0.1	x: 0 m η < 0.1	x: 0 m η = 4.8	x: 0 m η = 16.4	x: 0 m η = 16.3	CUMPLE η = 16.4
N361/N360	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0 m η = 8.6	x: 0 m η = 18.5	η = 1.3	x: 1.077 m η = 1.5	x: 0 m η = 3.1	x: 0.539 m η = 0.5	x: 1.077 m η = 0.2	x: 1.077 m η = 1.7	x: 0 m η = 3.6	x: 1.077 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 1.077 m η = 20.6	x: 1.077 m η = 20.4	CUMPLE η = 20.6
N343/N361	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.801 m η = 7.3	x: 0 m η = 24.3	η = 3.4	x: 0 m η = 15.0	x: 0 m η = 5.8	η = 0.7	x: 0 m η = 2.2	x: 0 m η = 15.1	x: 0 m η = 7.2	x: 0 m η = 2.3	x: 0 m η = 0.5	x: 0 m η = 11.0	x: 0 m η = 40.0	x: 0 m η = 43.1	CUMPLE η = 43.1
N363/N362	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.128 m η = 5.8	x: 0 m η = 16.5	η = 0.7	x: 1.128 m η = 2.3	x: 0 m η = 10.5	x: 0.752 m η = 1.5	x: 0 m η = 0.3	x: 0.94 m η = 1.6	x: 0 m η = 10.7	x: 1.128 m η = 0.1	x: 0 m η = 1.2	x: 0 m η = 10.9	x: 1.128 m η = 20.5	x: 0 m η = 21.6	CUMPLE η = 21.6
N364/N363	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.126 m η = 8.6	x: 0 m η = 14.6	x: 0.375 m η = 0.6	x: 1.126 m η = 1.8	x: 1.126 m η = 8.1	x: 0.375 m η = 1.1	x: 0 m η = 0.3	x: 1.126 m η = 1.9	x: 1.126 m η = 8.4	x: 1.126 m η < 0.1	x: 1.126 m η = 0.7	x: 0 m η = 12.8	x: 1.126 m η = 17.7	x: 1.126 m η = 17.4	CUMPLE η = 17.7
N365/N364	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.126 m η = 12.4	x: 0 m η = 12.6	η = 0.7	x: 0 m η = 1.2	x: 0 m η = 2.3	x: 0.188 m η = 0.2	x: 0 m η = 0.3	x: 0 m η = 1.3	x: 0 m η = 2.6	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 7.6	x: 1.126 m η = 14.9	x: 1.126 m η = 14.4	CUMPLE η = 14.9
N366/N365	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.12 m η = 17.0	x: 0 m η = 10.6	η = 0.3	x: 0 m η = 8.3	x: 1.12 m η = 4.1	η = 0.5	x: 0 m η = 1.0	x: 0 m η = 8.3	x: 1.12 m η = 4.2	x: 0 m η = 0.7	x: 1.12 m η = 0.2	x: 0 m η = 25.8	x: 0 m η = 12.7	x: 0 m η = 24.5	CUMPLE η = 25.8
N341/N366	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.187 m η = 22.4	x: 0.396 m η = 9.0	x: 0.989 m η = 3.8	x: 1.187 m η = 7.2	x: 0 m η = 13.4	x: 0.989 m η = 1.6	x: 1.187 m η = 1.0	x: 1.187 m η = 7.2	x: 0 m η = 15.1	x: 1.187 m η = 0.5	x: 0 m η = 2.3	x: 0 m η = 39.1	x: 0 m η = 18.3	x: 0 m η = 31.5	CUMPLE η = 39.1
N357/N362	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.934 m η = 9.6	x: 0.701 m η = 1.6	η = 0.2	x: 0 m η = 1.3	x: 0.934 m η = 5.3	x: 0 m η = 0.4	x: 0 m η = 0.1	x: 0 m η = 1.4	x: 0.934 m η = 5.4	x: 0 m η < 0.1	x: 0.934 m η = 0.3	x: 0.934 m η = 12.9	x: 0.934 m η = 4.6	x: 0.934 m η = 12.0	CUMPLE η = 12.9
N358/N362	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0 m η = 1.1	x: 0 m η = 17.6	η = 1.0	x: 0 m η = 1.9	x: 1.006 m η = 3.7	η = 0.3	x: 1.006 m η = 0.2	x: 0 m η = 1.1	x: 1.006 m η = 4.2	x: 0 m η < 0.1	x: 1.006 m η = 0.2	N.P.[1]	x: 0 m η = 19.7	x: 0 m η = 20.0	CUMPLE η = 20.0
N358/N363	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.94 m η = 12.6	N.P.[2]	x: 0.47 m η = 0.9	x: 0.94 m η = 1.6	x: 0 m η = 4.5	x: 0.47 m η = 0.5	x: 0 m η = 0.2	x: 0 m η = 1.6	x: 0 m η = 4.9	x: 0.94 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	N.P.[3]	x: 0.94 m η = 14.6	CUMPLE η = 14.6
N359/N363	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.014 m η = 0.1	x: 0 m η = 22.5	x: 0.845 m η = 0.7	x: 0 m η = 2.2	x: 0 m η = 3.6	x: 0.845 m η = 0.3	x: 1.014 m η = 0.2	x: 0 m η = 1.3	x: 0 m η = 3.9	x: 0 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 0 m η = 24.9	x: 0 m η = 25.3	CUMPLE η = 25.3
N359/N364	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.935 m η = 14.5	x: 0.234 m η < 0.1	x: 0.468 m η = 1.3	x: 0 m η = 2.3	x: 0.935 m η = 3.5	x: 0.468 m η = 0.4	x: 0 m η = 0.3	x: 0 m η = 2.0	x: 0.935 m η = 4.1	x: 0 m η = 0.1	x: 0.935 m η = 0.2	N.P.[1]	x: 0.234 m η = 2.7	x: 0 m η = 17.3	CUMPLE η = 17.3
N360/N364	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 27.4	x: 0.338 m η = 0.2	x: 1.015 m η = 1.6	x: 1.015 m η = 6.9	x: 0.169 m η = 0.5	x: 1.015 m η = 0.2	x: 1.015 m η = 0.9	x: 1.015 m η = 7.0	x: 1.015 m η < 0.1	x: 1.015 m η = 0.5	N.P.[1]	x: 1.015 m η = 29.2	x: 1.015 m η = 29.3	CUMPLE η = 29.3
N360/N365	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.932 m η = 16.6	N.P.[2]	η = 0.8	x: 0 m η = 3.0	x: 0.932 m η = 8.3	x: 0.466 m η = 0.8	x: 0 m η = 0.3	x: 0 m η = 2.0	x: 0.932 m η = 8.6	x: 0 m η = 0.1	x: 0.932 m η = 0.7	x: 0.932 m η = 21.2	N.P.[3]	x: 0 m η = 20.3	CUMPLE η = 21.2
N361/N365	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 31.7	x: 0.339 m η = 1.1	x: 0 m η = 4.1	x: 1.017 m η = 7.8	x: 0.339 m η = 0.6	x: 1.017 m η = 0.4	x: 1.017 m η = 2.5	x: 1.017 m η = 8.3	x: 0 m η = 0.2	x: 1.017 m η = 0.7	N.P.[1]	x: 0 m η = 36.7	x: 0 m η = 36.9	CUMPLE η = 36.9
N361/N366	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.932 m η = 16.6	N.P.[2]	x: 0 m η = 0.5	x: 0 m η = 4.1	x: 0.932 m η = 6.3	x: 0 m η = 0.4	x: 0 m η = 0.3	x: 0 m η = 2.3	x: 0.932 m η = 6.5	x: 0 m η = 0.2	x: 0.932 m η = 0.4	x: 0.932 m η = 15.1	N.P.[3]	x: 0 m η = 21.7	CUMPLE η = 21.7
N343/N366	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 32.4	x: 0.653 m η = 3.3	x: 0 m η = 5.4	x: 0 m η = 7.8	η = 0.5	x: 0.871 m η = 0.5	x: 0 m η = 5.4	x: 0 m η = 9.3	x: 0 m η = 0.3	x: 0 m η = 0.9	N.P.[1]	x: 0 m η = 38.4	x: 0 m η = 38.9	CUMPLE η = 38.9
N371/N367	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.41 m η = 25.3	x: 1.41 m η = 39.6	η = 1.8	x: 0 m η = 1.9	x: 1.41 m η = 18.8	η = 1.7	x: 0 m η = 0.2	x: 0 m η = 2.7	x: 1.41 m η = 19.6	x: 0 m η = 0.1	x: 1.41 m η = 3.9	x: 1.41 m η = 51.9	x: 1.41 m η = 62.5	x: 1.41 m η = 63.0	CUMPLE η = 63.0
N367/N368	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.233 m η = 13.6	x: 0.233 m η = 13.3	η = 0.7	x: 0.933 m η = 1.5	x: 0 m η = 37.4	x: 1.167 m η = 4.7	x: 0 m η = 0.1	x: 0 m η = 1.2	x: 0 m η = 37.7	x: 1.167 m η < 0.1	x: 0 m η = 14.4	x: 0 m η = 61.8	x: 0 m η = 51.3	x: 0 m η = 60.2	CUMPLE η = 61.8
N368/N369	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.35 m η = 13.6	x: 0 m η = 4.0	η = 1.3	x: 1.35 m η = 4.5	x: 1.35 m η = 54.2	x: 0.225 m η = 6.2	x: 0 m η = 0.3	x: 1.35 m η = 4.5	x: 1.35 m η = 54.8	x: 1.35 m η = 0.2	x: 1.35 m η = 30.4	x: 1.35 m η = 80.7	x: 1.35 m η = 56.2	x: 1.35 m η = 76.2	CUMPLE η = 80.7
N369/N370	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.79 m η = 16.7	x: 0 m η = 6.1	η = 6.9	x: 0 m η = 10.5	x: 0 m η = 49.4	η = 10.0	x: 0.79 m η = 2.2	x: 0 m η = 10.5	x: 0 m η = 52.5	x: 0 m η = 1.2	x: 0 m η = 28.5	x: 0 m η = 86.5	x: 0 m η = 58.2	x: 0 m η = 72.8	CUMPLE η = 86.5
N369/N372	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.536 m η = 2.4	x: 0.536 m η = 4.5	x: 0.179 m η = 2.4	x: 1.073 m η = 9.7	x: 1.073 m η = 14.3	x: 0.179 m η = 1.9	x: 1.073 m η = 1.4	x: 1.073 m η = 9.7	x: 1.073 m η = 15.4	x: 1.073 m η = 1.0	x: 1.073 m η = 2.4	x: 1.073 m η = 25.9	x: 1.073 m η = 24.7	x: 1.073 m η = 23.0	CUMPLE η = 25.9
N367/N373	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.217 m η = 10.3	x: 0.217 m η = 24.8	x: 0.652 m η = 1.6	x: 0.869 m η = 4.0	x: 0 m η = 7.7	η = 0.6	x: 0 m η = 0.5	x: 0 m η = 4.1	x: 0 m η = 8.3	x: 0 m η = 0.2	x: 0 m η = 0.7	x: 0 m η = 13.4	x: 0.869 m η = 29.2	x: 0.869 m η = 29.7	CUMPLE η = 29.7
N373/N368	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.983 m η = 15.6	x: 0 m η = 11.9	η = 0.4	x: 0 m η = 2.9	x: 0 m η = 28.7	x: 0.246 m η = 2.9	x: 0.983 m η = 0.3	x: 0 m η = 2.9	x: 0 m η = 28.9	x: 0 m η = 0.1	x: 0 m η = 8.4	x: 0 m η = 46.0	x: 0 m η = 33.2	x: 0 m η = 45.0	CUMPLE η = 46.0

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N368/N374	w / t ≤ (w / t)$_{Max}$ Cumple	x: 0.685 m η = 6.8	x: 0.685 m η = 17.1	x: 0.514 m η = 0.8	x: 0 m η = 3.1	x: 1.028 m η = 1.3	η < 0.1	x: 0 m η = 0.3	x: 0 m η = 2.7	x: 1.028 m η = 1.7	x: 0 m η = 0.1	x: 1.028 m η < 0.1	N.P.[1]	x: 0 m η = 20.0	x: 0 m η = 20.2	CUMPLE η = 20.2
N374/N369	w / t ≤ (w / t)$_{Max}$ Cumple	x: 0 m η = 9.7	x: 0 m η = 8.7	x: 0.371 m η = 5.0	x: 0.928 m η = 1.6	x: 1.114 m η = 29.3	η = 2.2	x: 0 m η = 0.1	x: 0 m η = 3.1	x: 1.114 m η = 31.5	x: 0 m η = 0.1	x: 1.114 m η = 9.9	x: 1.114 m η = 50.5	x: 1.114 m η = 41.0	x: 1.114 m η = 45.1	CUMPLE η = 50.5
N372/N370	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.096 m η = 12.7	x: 0 m η = 57.5	x: 0.731 m η = 3.9	x: 0 m η = 3.6	x: 0 m η = 9.4	x: 0.731 m η = 0.5	x: 0 m η = 0.3	x: 0 m η = 3.1	x: 0 m η = 11.0	x: 0 m η = 0.1	x: 0 m η = 1.2	N.P.[1]	x: 0 m η = 62.8	x: 0 m η = 62.2	CUMPLE η = 62.8
N379/N375	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.41 m η = 25.8	x: 1.41 m η = 39.9	x: 1.41 m η = 1.8	x: 0 m η = 1.9	x: 1.41 m η = 18.2	η = 1.6	x: 0 m η = 0.2	x: 0 m η = 2.7	x: 1.41 m η = 19.0	x: 0 m η = 0.1	x: 1.41 m η = 3.6	x: 1.41 m η = 51.6	x: 1.41 m η = 62.1	x: 1.41 m η = 62.6	CUMPLE η = 62.6
N375/N376	w / t ≤ (w / t)$_{Max}$ Cumple	x: 0 m η = 14.0	x: 0 m η = 13.7	x: 0 m η = 0.8	x: 0.7 m η = 1.5	x: 0 m η = 37.2	x: 0.933 m η = 4.8	x: 0 m η = 0.1	x: 0 m η = 1.2	x: 0 m η = 37.5	x: 0.7 m η < 0.1	x: 0 m η = 14.3	x: 0 m η = 62.3	x: 0 m η = 51.6	x: 0 m η = 60.5	CUMPLE η = 62.3
N376/N377	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.35 m η = 13.7	x: 0 m η = 5.3	x: 0.225 m η = 1.1	x: 1.35 m η = 4.7	x: 1.35 m η = 54.6	x: 0.225 m η = 6.4	x: 0 m η = 0.4	x: 1.35 m η = 4.7	x: 1.35 m η = 55.0	x: 1.35 m η = 0.2	x: 1.35 m η = 30.7	x: 1.35 m η = 82.3	x: 1.35 m η = 57.5	x: 1.35 m η = 77.5	CUMPLE η = 82.3
N377/N378	w / t ≤ (w / t)$_{Max}$ Cumple	x: 0.79 m η = 17.0	x: 0 m η = 6.4	η = 6.3	x: 0 m η = 10.1	x: 0 m η = 50.6	x: 0.592 m η = 10.3	x: 0.79 m η = 1.9	x: 0 m η = 10.1	x: 0 m η = 53.4	x: 0 m η = 1.1	x: 0 m η = 29.5	x: 0 m η = 88.1	x: 0 m η = 59.0	x: 0 m η = 74.9	CUMPLE η = 88.1
N383/N375	w / t ≤ (w / t)$_{Max}$ Cumple	x: 0.847 m η = 29.6	x: 0 m η = 21.6	x: 0.847 m η = 0.7	x: 0 m η = 10.9	x: 0 m η = 56.0	x: 0.424 m η = 6.5	x: 0 m η = 1.0	x: 0 m η = 10.9	x: 0 m η = 56.4	x: 0 m η = 1.2	x: 0 m η = 32.2	x: 0 m η = 82.9	x: 0 m η = 30.4	x: 0 m η = 78.2	CUMPLE η = 82.9
N375/N382	w / t ≤ (w / t)$_{Max}$ Cumple	x: 0.217 m η = 11.1	x: 0.217 m η = 25.7	η = 1.5	x: 0.869 m η = 4.1	x: 0 m η = 6.7	η = 0.5	x: 0 m η = 0.5	x: 0 m η = 4.2	x: 0 m η = 7.4	x: 0 m η = 0.2	x: 0 m η = 0.5	x: 0 m η = 12.6	x: 0.869 m η = 30.1	x: 0.869 m η = 30.7	CUMPLE η = 30.7
N382/N376	w / t ≤ (w / t)$_{Max}$ Cumple	x: 0.983 m η = 16.2	x: 0 m η = 12.8	η = 0.2	x: 0 m η = 3.1	x: 0.983 m η = 29.6	x: 0.738 m η = 3.0	x: 0.983 m η = 0.3	x: 0 m η = 3.1	x: 0.983 m η = 29.6	x: 0 m η = 0.1	x: 0.983 m η = 8.9	x: 0.983 m η = 47.5	x: 0.983 m η = 34.1	x: 0.983 m η = 46.5	CUMPLE η = 47.5
N376/N381	w / t ≤ (w / t)$_{Max}$ Cumple	x: 0.685 m η = 7.4	x: 0.685 m η = 17.9	x: 0.171 m η = 0.3	x: 0 m η = 3.0	x: 1.028 m η = 1.6	η < 0.1	x: 0 m η = 0.3	x: 0 m η = 2.7	x: 1.028 m η = 1.8	x: 0 m η = 0.1	x: 1.028 m η < 0.1	N.P.[1]	x: 0 m η = 20.7	x: 0 m η = 20.9	CUMPLE η = 20.9
N381/N377	w / t ≤ (w / t)$_{Max}$ Cumple	x: 0 m η = 10.2	x: 0 m η = 9.5	x: 0.557 m η = 4.9	x: 1.114 m η = 1.7	x: 1.114 m η = 29.1	x: 0 m η = 2.2	x: 0 m η = 0.1	x: 1.114 m η = 3.0	x: 1.114 m η = 31.2	x: 1.114 m η = 0.1	x: 1.114 m η = 9.8	x: 1.114 m η = 50.9	x: 1.114 m η = 41.3	x: 1.114 m η = 45.4	CUMPLE η = 50.9
N377/N380	w / t ≤ (w / t)$_{Max}$ Cumple	x: 0.536 m η = 2.1	x: 0.536 m η = 4.1	x: 0.358 m η = 2.6	x: 1.073 m η = 8.6	x: 1.073 m η = 14.6	x: 0.179 m η = 2.0	x: 1.073 m η = 1.2	x: 1.073 m η = 8.6	x: 1.073 m η = 15.7	x: 1.073 m η = 0.8	x: 1.073 m η = 2.5	x: 1.073 m η = 25.6	x: 1.073 m η = 24.3	x: 1.073 m η = 22.7	CUMPLE η = 25.6
N380/N378	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.096 m η = 14.0	x: 0 m η = 61.5	x: 0.914 m η = 4.0	x: 0 m η = 3.5	x: 0 m η = 10.3	x: 0.914 m η = 0.6	x: 0 m η = 0.4	x: 0 m η = 3.1	x: 0 m η = 12.0	x: 0 m η = 0.1	x: 0 m η = 1.4	N.P.[1]	x: 0 m η = 66.6	x: 0 m η = 66.0	CUMPLE η = 66.6
N372/N384	w / t ≤ (w / t)$_{Max}$ Cumple	x: 0.617 m η = 7.2	x: 0 m η = 26.3	x: 0.617 m η = 4.6	x: 0 m η = 17.5	x: 0 m η = 6.2	η = 0.9	x: 0 m η = 3.3	x: 0 m η = 17.5	x: 0 m η = 8.3	x: 0 m η = 3.2	x: 0 m η = 0.7	x: 0 m η = 10.2	x: 0 m η = 44.3	x: 0 m η = 48.1	CUMPLE η = 48.1
N384/N385	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.081 m η = 9.2	x: 0 m η = 20.8	x: 0.18 m η = 2.0	x: 1.081 m η = 1.8	x: 0 m η = 4.1	x: 0.18 m η = 0.7	x: 1.081 m η = 0.3	x: 1.081 m η = 1.9	x: 0 m η = 5.0	x: 1.081 m η < 0.1	x: 0 m η = 0.3	x: 1.081 m η = 10.7	x: 1.081 m η = 22.8	x: 1.081 m η = 23.1	CUMPLE η = 23.1
N385/N386	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.088 m η = 10.6	x: 0 m η = 16.6	x: 0.544 m η = 1.8	x: 0 m η = 2.2	x: 1.088 m η = 0.9	x: 0.363 m η = 0.1	x: 0 m η = 0.3	x: 0 m η = 2.2	x: 1.088 m η = 1.7	x: 0 m η < 0.1	x: 1.088 m η < 0.1	x: 0.544 m η = 12.1	x: 0 m η = 18.9	x: 0 m η = 19.3	CUMPLE η = 19.3
N386/N387	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.08 m η = 11.0	x: 0 m η = 12.1	x: 0.9 m η = 0.9	x: 0 m η = 1.1	x: 0 m η = 3.3	η = 0.4	x: 0 m η = 0.2	x: 0 m η = 1.1	x: 0 m η = 3.7	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 5.9	x: 0 m η = 13.3	x: 0 m η = 13.5	CUMPLE η = 13.5
N387/N388	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.085 m η = 11.7	x: 1.085 m η = 9.1	η = 0.3	x: 1.085 m η = 1.7	x: 1.085 m η = 4.7	x: 1.085 m η = 0.7	x: 0 m η = 0.2	x: 1.085 m η = 1.7	x: 1.085 m η = 4.8	x: 1.085 m η < 0.1	x: 1.085 m η = 0.2	x: 0.904 m η = 13.7	x: 0 m η = 10.3	x: 1.085 m η = 13.2	CUMPLE η = 13.7
N388/N389	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.082 m η = 11.9	x: 1.082 m η = 6.4	η = 0.6	x: 1.082 m η = 1.7	x: 0 m η = 1.6	η = 0.1	x: 0 m η = 0.1	x: 1.082 m η = 1.7	x: 0 m η = 1.8	x: 1.082 m η < 0.1	x: 0 m η < 0.1	x: 0.541 m η = 13.6	x: 0 m η = 7.0	x: 0.541 m η = 13.3	CUMPLE η = 13.6
N389/N390	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.085 m η = 13.6	x: 1.085 m η = 3.6	x: 0 m η = 0.8	x: 0.904 m η = 1.8	x: 0 m η = 1.0	x: 0.362 m η = 0.1	x: 0 m η = 0.1	x: 0.904 m η = 1.8	x: 0 m η = 1.4	x: 0.904 m η < 0.1	x: 0 m η < 0.1	x: 1.085 m η = 16.0	x: 1.085 m η = 4.3	x: 0.904 m η = 15.8	CUMPLE η = 16.0
N390/N391	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.081 m η = 15.5	x: 0 m η = 0.8	η = 0.5	x: 0.901 m η = 2.0	x: 0 m η = 1.0	x: 0.36 m η = 0.1	x: 0 m η = 0.1	x: 0.18 m η = 1.2	x: 0 m η = 1.1	x: 0.901 m η < 0.1	x: 0 m η < 0.1	x: 1.081 m η = 18.2	x: 1.081 m η = 2.3	x: 0.901 m η = 18.0	CUMPLE η = 18.2
N392/N391	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.08 m η = 16.0	N.P.[2]	x: 0 m η = 1.0	x: 0.72 m η = 2.0	x: 1.08 m η = 2.0	x: 0.36 m η = 0.3	x: 0 m η = 0.1	x: 0.54 m η = 1.3	x: 1.08 m η = 2.4	x: 0.54 m η < 0.1	x: 1.08 m η = 0.1	x: 0.72 m η = 18.7	N.P.[3]	x: 0.72 m η = 18.6	CUMPLE η = 18.7
N393/N392	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.084 m η = 15.0	N.P.[2]	η = 1.3	x: 0.722 m η = 2.0	x: 0 m η = 1.8	η = 0.3	x: 0 m η = 0.1	x: 0.722 m η = 2.0	x: 0 m η = 1.9	x: 0.722 m η < 0.1	x: 0 m η < 0.1	x: 0.903 m η = 17.6	N.P.[3]	x: 0.903 m η = 17.5	CUMPLE η = 17.6
N394/N393	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.08 m η = 12.7	x: 0 m η = 0.9	x: 0.54 m η = 0.8	x: 0 m η = 2.0	x: 1.08 m η = 2.6	x: 0.54 m η = 0.3	x: 0 m η = 0.2	x: 0 m η = 2.2	x: 1.08 m η = 3.0	x: 0 m η < 0.1	x: 1.08 m η = 0.1	x: 1.08 m η = 15.2	x: 0 m η = 4.2	x: 1.08 m η = 15.0	CUMPLE η = 15.2
N395/N394	w / t ≤ (w / t)$_{Max}$ Cumple	x: 0.361 m η = 10.6	x: 0.361 m η = 6.5	η = 0.4	x: 1.083 m η = 1.9	x: 0 m η = 3.1	η = 0.5	x: 0 m η = 0.2	x: 1.083 m η = 1.9	x: 0 m η = 3.1	x: 1.083 m η < 0.1	x: 0 m η = 0.1	x: 1.083 m η = 13.8	x: 0 m η = 8.5	x: 1.083 m η = 12.8	CUMPLE η = 13.8
N396/N395	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.087 m η = 10.0	x: 0 m η = 9.7	η = 0.7	x: 1.087 m η = 1.3	x: 0 m η = 2.7	x: 0.543 m η = 0.3	x: 0 m η = 0.2	x: 1.087 m η = 1.4	x: 0 m η = 3.0	x: 1.087 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 5.4	x: 0 m η = 11.3	x: 0.724 m η = 11.3	CUMPLE η = 11.3
N397/N396	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.085 m η = 9.4	x: 0 m η = 13.7	η = 1.3	x: 0 m η = 1.9	x: 0 m η = 1.3	x: 0.723 m η = 0.2	x: 0 m η = 0.3	x: 0 m η = 2.1	x: 0 m η = 1.8	x: 0 m η < 0.1	x: 0 m η < 0.1	x: 0 m η = 3.5	x: 0 m η = 16.2	x: 0 m η = 16.1	CUMPLE η = 16.2
N398/N397	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.077 m η = 8.4	x: 0 m η = 18.1	η = 1.4	x: 1.077 m η = 1.5	x: 0 m η = 3.1	x: 0.18 m η = 0.5	x: 1.077 m η = 0.2	x: 1.077 m η = 1.6	x: 0 m η = 3.7	x: 1.077 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 1.077 m η = 20.2	x: 1.077 m η = 20.0	CUMPLE η = 20.2
N380/N398	w / t ≤ (w / t)$_{Max}$ Cumple	x: 0.801 m η = 6.8	x: 0 m η = 24.1	x: 0.801 m η = 3.7	x: 0 m η = 14.9	x: 0 m η = 5.9	η = 0.7	x: 0 m η = 2.1	x: 0 m η = 15.0	x: 0 m η = 7.5	x: 0 m η = 2.3	x: 0 m η = 0.6	x: 0 m η = 13.0	x: 0 m η = 39.7	x: 0 m η = 42.8	CUMPLE η = 42.8
N400/N399	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.128 m η = 2.1	x: 0 m η = 16.5	η = 1.1	x: 1.128 m η = 2.3	x: 0 m η = 10.9	η = 1.6	x: 0 m η = 0.3	x: 1.128 m η = 2.3	x: 0 m η = 11.4	x: 1.128 m η = 0.1	x: 0 m η = 1.3	x: 0 m η = 8.1	x: 0 m η = 19.1	x: 0 m η = 20.7	CUMPLE η = 20.7
N401/N400	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.126 m η = 6.6	x: 0 m η = 11.8	x: 0.188 m η = 2.3	x: 1.126 m η = 1.8	x: 1.126 m η = 8.2	x: 0.188 m η = 1.1	x: 0 m η = 0.3	x: 0 m η = 1.9	x: 1.126 m η = 9.2	x: 0 m η < 0.1	x: 1.126 m η = 0.9	x: 0 m η = 11.4	x: 0 m η = 14.6	x: 0 m η = 14.1	CUMPLE η = 14.6
N402/N401	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.126 m η = 11.2	x: 0 m η = 11.0	η = 1.1	x: 0 m η = 1.2	x: 0 m η = 2.1	x: 0.188 m η = 0.2	x: 0 m η = 0.3	x: 1.126 m η = 1.3	x: 0 m η = 2.5	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 6.8	x: 1.126 m η = 13.3	x: 0 m η = 13.0	CUMPLE η = 13.3
N403/N402	w / t ≤ (w / t)$_{Max}$ Cumple	x: 0.373 m η = 16.4	x: 0.373 m η = 9.8	x: 1.12 m η = 1.2	x: 0 m η = 8.2	x: 1.12 m η = 3.7	x: 1.12 m η = 0.5	x: 0 m η = 1.0	x: 0 m η = 8.3	x: 1.12 m η = 4.2	x: 0 m η = 0.7	x: 1.12 m η = 0.2	x: 0 m η = 25.0	x: 0 m η = 12.0	x: 0 m η = 24.0	CUMPLE η = 25.0
N378/N403	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.187 m η = 22.4	x: 0.594 m η = 8.6	x: 0.989 m η = 6.0	x: 1.187 m η = 7.1	x: 0 m η = 13.6	x: 0.989 m η = 1.6	x: 1.187 m η = 1.0	x: 1.187 m η = 7.1	x: 0 m η = 16.3	x: 1.187 m η = 0.5	x: 0 m η = 2.7	x: 0 m η = 33.7	x: 1.187 m η = 11.4	x: 1.187 m η = 31.3	CUMPLE η = 33.7
N394/N399	w / t ≤ (w / t)$_{Max}$ Cumple	x: 0.701 m η = 12.1	x: 0.701 m η = 9.0	x: 0.701 m η = 1.2	x: 0 m η = 2.1	x: 0.934 m η = 2.9	x: 0.701 m η = 0.2	x: 0 m η = 0.2	x: 0 m η = 2.2	x: 0.934 m η = 3.4	x: 0 m η < 0.1	x: 0.934 m η = 0.1	N.P.[1]	x: 0 m η = 12.4	x: 0 m η = 15.5	CUMPLE η = 15.5
N395/N399	w / t ≤ (w / t)$_{Max}$ Cumple	x: 1.006 m η = 1.5	x: 0 m η = 17.4	x: 0 m η = 0.4	x: 0 m η = 1.9	x: 1.006 m η = 3.1	x: 0 m η = 0.2	x: 1.006 m η = 0.2	x: 1.006 m η = 1.8	x: 1.006 m η = 3.2	x: 0 m η < 0.1	x: 1.006 m η = 0.1	N.P.[1]	x: 0 m η = 19.4	x: 0 m η = 19.8	CUMPLE η = 19.8
N395/N400	w / t ≤ (w / t)$_{Max}$ Cumple	x: 0.94 m η = 12.5	N.P.[2]	η = 0.1	x: 0.94 m η = 1.6	x: 0.94 m η = 7.6	x: 0.94 m η = 0.7	x: 0 m η = 0.2	x: 0 m η = 1.3	x: 0.94 m η = 7.7	x: 0.94 m η < 0.1	x: 0.94 m η = 0.6	x: 0.94 m η = 16.1	N.P.[3]	x: 0.94 m η = 15.2	CUMPLE η = 16.1

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N396/N400	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 0.4	x: 0 m η = 21.9	x: 0.338 m η = 0.1	x: 0 m η = 2.2	x: 1.014 m η = 5.0	x: 0.507 m η = 0.5	x: 1.014 m η = 0.2	x: 1.014 m η = 1.2	x: 1.014 m η = 5.0	x: 0 m η < 0.1	x: 1.014 m η = 0.3	N.P.(1)	x: 0 m η = 24.5	x: 0 m η = 24.7	CUMPLE η = 24.7
N396/N401	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.935 m η = 14.2	N.P.(2)	η = 0.1	x: 0 m η = 2.3	x: 0.935 m η = 4.6	η = 0.2	x: 0 m η = 0.3	x: 0 m η = 1.6	x: 0.935 m η = 4.6	x: 0 m η = 0.1	x: 0.935 m η = 0.2	N.P.(1)	N.P.(3)	x: 0 m η = 17.1	CUMPLE η = 17.1
N397/N401	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 27.0	x: 0.508 m η = 1.2	x: 1.015 m η = 1.5	x: 1.015 m η = 0.6	x: 1.015 m η = 0.1	x: 1.015 m η = 0.2	x: 1.015 m η = 1.3	x: 0 m η = 0.9	x: 1.015 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 1.015 m η = 28.9	x: 1.015 m η = 28.8	CUMPLE η = 28.9
N397/N402	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.932 m η = 16.3	N.P.(2)	x: 0.699 m η = 0.6	x: 0 m η = 2.9	x: 0 m η = 2.8	x: 0.233 m η = 0.1	x: 0 m η = 0.3	x: 0 m η = 1.7	x: 0 m η = 3.1	x: 0 m η = 0.1	x: 0 m η = 0.1	N.P.(1)	N.P.(3)	x: 0 m η = 20.0	CUMPLE η = 20.0
N398/N402	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 31.4	x: 0.847 m η = 0.4	x: 0 m η = 4.1	x: 0 m η = 1.3	η = 0.1	x: 1.017 m η = 0.4	x: 1.017 m η = 2.5	x: 0 m η = 1.5	x: 0 m η = 0.2	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 36.1	x: 0 m η = 36.5	CUMPLE η = 36.5
N398/N403	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.932 m η = 16.4	N.P.(2)	η = 0.6	x: 0 m η = 4.1	x: 0 m η = 1.1	x: 0.932 m η = 0.1	x: 0 m η = 0.3	x: 0 m η = 2.3	x: 0 m η = 1.3	x: 0 m η = 0.2	x: 0 m η < 0.1	N.P.(1)	N.P.(3)	x: 0 m η = 21.5	CUMPLE η = 21.5
N380/N403	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 32.0	x: 0.653 m η = 2.5	x: 0 m η = 5.5	x: 0 m η = 10.9	η = 1.1	x: 0.871 m η = 0.5	x: 0 m η = 5.5	x: 0 m η = 12.0	x: 0 m η = 0.3	x: 0 m η = 1.5	N.P.(1)	x: 0 m η = 38.1	x: 0 m η = 38.5	CUMPLE η = 38.5
N379/N383	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.189 m η = 26.1	x: 0.189 m η = 58.8	x: 0.378 m η = 5.0	x: 0.755 m η = 10.8	x: 0 m η = 19.7	x: 0.378 m η = 1.8	x: 0.755 m η = 1.1	x: 0.755 m η = 12.9	x: 0 m η = 21.8	x: 0.755 m η = 1.7	x: 0 m η = 4.8	x: 0 m η = 14.9	x: 0.755 m η = 66.0	x: 0.755 m η = 65.1	CUMPLE η = 66.0
N404/N367	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.847 m η = 26.6	x: 0 m η = 20.1	η = 0.7	x: 0 m η = 10.5	x: 0 m η = 57.1	η = 6.6	x: 0 m η = 0.9	x: 0 m η = 10.5	x: 0 m η = 57.4	x: 0 m η = 1.1	x: 0 m η = 33.4	x: 0 m η = 83.4	x: 0 m η = 28.3	x: 0 m η = 79.0	CUMPLE η = 83.4
N371/N404	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.189 m η = 24.2	x: 0.189 m η = 56.6	x: 0.378 m η = 5.1	x: 0.755 m η = 10.9	x: 0 m η = 20.3	x: 0.378 m η = 1.8	x: 0.755 m η = 1.1	x: 0.755 m η = 13.1	x: 0 m η = 22.5	x: 0.755 m η = 1.7	x: 0 m η = 5.1	x: 0 m η = 14.2	x: 0.755 m η = 64.3	x: 0.755 m η = 63.1	CUMPLE η = 64.3
N404/N337	$w/t \leq (w/t)_{Máx.}$ Cumple	η < 0.1	η < 0.1	η = 3.5	x: 0 m η = 25.3	x: 0.3 m η = 2.5	η = 1.0	x: 0 m η = 51.5	x: 0 m η = 26.8	x: 0.3 m η = 4.0	x: 0 m η = 87.2	x: 0.3 m η = 0.2	x: 0 m η = 63.4	x: 0.3 m η = 30.6	x: 0 m η = 45.2	CUMPLE η = 45.2
N367/N330	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.1	η = 0.1	x: 0.15 m η = 0.4	x: 0.3 m η = 26.9	x: 0.3 m η = 30.4	x: 0.15 m η = 12.5	x: 0 m η = 52.2	x: 0.3 m η = 27.1	x: 0.3 m η = 30.6	x: 0.3 m η = 88.7	x: 0.3 m η = 10.9	x: 0.3 m η = 97.2	x: 0.3 m η = 57.6	x: 0.3 m η = 65.9	CUMPLE η = 65.9
N373/N336	$w/t \leq (w/t)_{Máx.}$ Cumple	η < 0.1	η < 0.1	η < 0.1	x: 0 m η = 60.6	x: 0 m η = 4.0	η = 1.7	x: 0 m η = 66.4	x: 0 m η = 60.6	x: 0 m η = 4.0	x: 0 m η = 34.8	x: 0 m η = 0.2	x: 0 m η = 05.8	x: 0 m η = 64.6	x: 0 m η = 43.0	CUMPLE η = 43.0
N368/N331	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.15 m η < 0.1	x: 0.15 m η < 0.1	x: 0.15 m η = 1.1	x: 0 m η = 51.2	x: 0 m η = 30.8	x: 0.15 m η = 13.1	x: 0 m η = 64.3	x: 0 m η = 51.7	x: 0 m η = 31.2	x: 0 m η = 71.6	x: 0 m η = 11.5	x: 0 m η = 28.5	x: 0 m η = 82.7	x: 0 m η = 72.0	CUMPLE η = 72.0
N374/N335	$w/t \leq (w/t)_{Máx.}$ Cumple	η < 0.1	η < 0.1	x: 0.15 m η = 1.5	x: 0 m η = 40.1	x: 0 m η = 15.6	x: 0.15 m η = 5.2	x: 0 m η = 46.9	x: 0 m η = 40.8	x: 0 m η = 16.3	x: 0 m η = 20.2	x: 0 m η = 2.9	x: 0 m η = 96.3	x: 0.3 m η = 56.7	x: 0 m η = 38.8	CUMPLE η = 38.8
N369/N332	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 1.2	η = 1.6	η = 1.0	x: 0 m η = 14.9	x: 0.3 m η = 24.6	x: 0.3 m η = 8.2	x: 0 m η = 4.8	x: 0 m η = 15.3	x: 0.3 m η = 25.1	x: 0 m η = 2.6	x: 0.3 m η = 6.9	x: 0 m η = 51.3	x: 0 m η = 41.0	x: 0 m η = 36.8	CUMPLE η = 51.3
N372/N334	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.3	η = 0.2	η = 0.6	x: 0 m η = 35.6	x: 0.3 m η = 13.6	x: 0 m η = 4.5	x: 0 m η = 11.9	x: 0 m η = 35.8	x: 0.3 m η = 13.9	x: 0 m η = 14.2	x: 0.3 m η = 2.1	x: 0.3 m η = 62.1	x: 0.3 m η = 15.0	x: 0.3 m η = 47.6	CUMPLE η = 62.1
N370/N333	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 4.4	η = 3.5	x: 0.15 m η = 0.8	x: 0.3 m η = 76.1	x: 0.3 m η = 33.2	x: 0.3 m η = 11.0	x: 0.3 m η = 25.3	x: 0.3 m η = 76.4	x: 0.3 m η = 33.5	x: 0.3 m η = 64.7	x: 0.3 m η = 12.4	x: 0.3 m η = 41.1	x: 0.3 m η = 12.6	x: 0.3 m η = 15.6	CUMPLE η = 41.1
N384/N347	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.15 m η = 0.1	x: 0.15 m η = 0.1	η = 0.6	x: 0 m η = 20.0	x: 0.3 m η = 12.9	η = 4.3	x: 0 m η = 6.7	x: 0 m η = 20.3	x: 0.3 m η = 13.2	x: 0 m η = 4.6	x: 0.3 m η = 1.9	x: 0 m η = 41.6	x: 0 m η = 32.5	x: 0 m η = 29.7	CUMPLE η = 41.6
N385/N348	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.15 m η = 0.3	x: 0.15 m η = 0.4	η = 0.6	x: 0 m η = 11.4	x: 0.3 m η = 15.5	η = 5.2	x: 0 m η = 3.7	x: 0 m η = 11.7	x: 0.3 m η = 15.8	x: 0 m η = 1.5	x: 0.3 m η = 2.8	x: 0 m η = 34.5	x: 0 m η = 26.5	x: 0 m η = 24.2	CUMPLE η = 34.5
N386/N349	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.15 m η = 0.1	x: 0.15 m η = 0.1	η = 0.5	x: 0 m η = 3.4	x: 0.3 m η = 14.7	η = 4.9	x: 0 m η = 1.1	x: 0 m η = 3.6	x: 0.3 m η = 14.9	x: 0 m η = 0.1	x: 0.3 m η = 2.5	x: 0 m η = 22.8	x: 0 m η = 17.0	x: 0.3 m η = 18.8	CUMPLE η = 22.8
N387/N350	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.15 m η < 0.1	x: 0.15 m η < 0.1	η = 0.2	x: 0.3 m η = 2.9	x: 0 m η = 23.5	x: 0.15 m η = 7.9	x: 0 m η = 0.9	x: 0.3 m η = 3.0	x: 0 m η = 23.6	x: 0.3 m η = 0.1	x: 0 m η = 6.2	x: 0.3 m η = 32.2	x: 0.3 m η = 26.6	x: 0.3 m η = 29.5	CUMPLE η = 32.2
N388/N351	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.5	η = 0.6	η = 0.2	x: 0.3 m η = 4.2	x: 0 m η = 15.1	η = 5.0	x: 0 m η = 1.2	x: 0.3 m η = 4.2	x: 0 m η = 15.1	x: 0.3 m η = 0.2	x: 0 m η = 2.5	x: 0.3 m η = 23.8	x: 0.3 m η = 19.8	x: 0.3 m η = 19.9	CUMPLE η = 23.8
N389/N352	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.1	η = 0.1	η = 0.3	x: 0.3 m η = 2.0	x: 0.3 m η = 2.9	x: 0.3 m η = 1.0	x: 0 m η = 0.4	x: 0.3 m η = 2.1	x: 0.3 m η = 2.9	x: 0.3 m η < 0.1	x: 0.3 m η = 0.1	N.P.(1)	x: 0.3 m η = 2.6	x: 0.3 m η = 3.7	CUMPLE η = 3.7
N390/N353	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.1	η = 0.1	η = 0.2	x: 0 m η = 4.2	x: 0.3 m η = 5.8	η = 1.9	x: 0 m η = 1.1	x: 0 m η = 4.3	x: 0.3 m η = 5.8	x: 0 m η = 0.2	x: 0.3 m η = 0.4	x: 0.3 m η = 7.6	x: 0 m η = 6.9	x: 0.3 m η = 7.2	CUMPLE η = 7.6
N391/N354	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.7	η = 0.8	η = 0.3	x: 0 m η = 7.2	x: 0.3 m η = 10.1	x: 0.3 m η = 3.4	x: 0 m η = 2.3	x: 0 m η = 7.3	x: 0.3 m η = 10.1	x: 0 m η = 0.6	x: 0.3 m η = 1.1	x: 0 m η = 15.6	x: 0 m η = 13.1	x: 0.3 m η = 12.8	CUMPLE η = 15.6
N392/N355	$w/t \leq (w/t)_{Máx.}$ Cumple	η < 0.1	η < 0.1	η = 0.5	x: 0 m η = 2.6	x: 0.3 m η = 12.4	x: 0 m η = 4.1	x: 0 m η = 0.7	x: 0 m η = 2.8	x: 0.3 m η = 12.4	x: 0 m η = 0.1	x: 0.3 m η = 1.7	x: 0.3 m η = 16.2	x: 0.3 m η = 11.8	x: 0.3 m η = 15.5	CUMPLE η = 16.2
N393/N356	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.1	η = 0.1	x: 0.3 m η = 0.5	x: 0.3 m η = 4.4	x: 0 m η = 12.5	η = 4.2	x: 0 m η = 1.2	x: 0.3 m η = 4.6	x: 0 m η = 12.7	x: 0.3 m η = 0.2	x: 0 m η = 1.8	x: 0.3 m η = 19.7	x: 0.3 m η = 16.4	x: 0 m η = 15.7	CUMPLE η = 19.7
N394/N357	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.2	η = 0.2	x: 0 m η = 0.3	x: 0.3 m η = 6.5	x: 0 m η = 19.7	x: 0.3 m η = 6.5	x: 0 m η = 1.8	x: 0.3 m η = 6.6	x: 0 m η = 19.9	x: 0.3 m η = 0.5	x: 0 m η = 4.4	x: 0.3 m η = 31.6	x: 0.3 m η = 26.0	x: 0.3 m η = 25.5	CUMPLE η = 31.6
N399/N362	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 3.2	x: 0 m η = 3.5	η = 0.3	x: 0 m η = 16.6	x: 0.3 m η = 28.0	x: 0 m η = 8.9	x: 0.3 m η = 3.0	x: 0 m η = 16.7	x: 0.3 m η = 28.1	x: 0 m η = 2.9	x: 0.3 m η = 8.7	x: 0 m η = 54.6	x: 0 m η = 44.8	x: 0 m η = 40.5	CUMPLE η = 54.6
N395/N358	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.1	η = 0.1	η = 0.4	x: 0.3 m η = 4.1	x: 0 m η = 21.1	x: 0.15 m η = 7.0	x: 0 m η = 1.1	x: 0.3 m η = 4.2	x: 0 m η = 21.1	x: 0.3 m η = 0.2	x: 0 m η = 5.0	x: 0.3 m η = 30.4	x: 0.3 m η = 25.1	x: 0.3 m η = 26.5	CUMPLE η = 30.4
N400/N363	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 2.0	η = 2.5	η = 0.4	x: 0.3 m η = 5.4	x: 0.3 m η = 13.4	x: 0.3 m η = 4.4	x: 0.3 m η = 0.7	x: 0.3 m η = 5.5	x: 0.3 m η = 13.6	x: 0.3 m η = 0.3	x: 0.3 m η = 2.0	x: 0.3 m η = 24.3	x: 0.3 m η = 19.4	x: 0.3 m η = 18.9	CUMPLE η = 24.3
N396/N359	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.1	η = 0.1	η = 0.4	x: 0.3 m η = 5.3	x: 0 m η = 13.6	x: 0 m η = 4.4	x: 0 m η = 1.4	x: 0.3 m η = 5.4	x: 0 m η = 13.8	x: 0.3 m η = 0.3	x: 0 m η = 2.1	x: 0.3 m η = 21.5	x: 0.3 m η = 18.5	x: 0 m η = 17.6	CUMPLE η = 21.5
N401/N364	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.3 m η = 3.1	x: 0.3 m η = 3.5	x: 0.3 m η = 0.4	x: 0 m η = 8.9	x: 0 m η = 14.3	x: 0.3 m η = 4.0	x: 0.3 m η = 1.0	x: 0 m η = 9.1	x: 0 m η = 14.5	x: 0 m η = 0.8	x: 0 m η = 2.3	x: 0 m η = 31.7	x: 0 m η = 26.9	x: 0 m η = 24.4	CUMPLE η = 31.7
N397/N360	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.2	η = 0.2	η = 0.4	x: 0.3 m η = 11.4	x: 0 m η = 13.0	x: 0.3 m η = 4.2	x: 0 m η = 3.4	x: 0.3 m η = 11.6	x: 0 m η = 13.2	x: 0.3 m η = 1.5	x: 0 m η = 1.9	x: 0.3 m η = 26.4	x: 0.3 m η = 24.1	x: 0.3 m η = 20.9	CUMPLE η = 26.4
N402/N365	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.3 m η = 3.5	x: 0.3 m η = 4.0	x: 0.3 m η = 0.4	x: 0 m η = 16.1	x: 0.3 m η = 7.8	η = 2.4	x: 0.3 m η = 2.6	x: 0 m η = 16.2	x: 0.3 m η = 7.9	x: 0 m η = 2.7	x: 0.3 m η = 0.7	x: 0 m η = 25.6	x: 0 m η = 21.6	x: 0 m η = 24.0	CUMPLE η = 25.6
N398/N361	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.1	η = 0.2	η = 0.4	x: 0.3 m η = 17.1	x: 0 m η = 10.3	x: 0.3 m η = 3.3	x: 0 m η = 5.4	x: 0.3 m η = 17.3	x: 0 m η = 10.4	x: 0.3 m η = 3.3	x: 0 m η = 1.2	x: 0.3 m η = 32.8	x: 0.3 m η = 27.0	x: 0.3 m η = 24.5	CUMPLE η = 32.8
N403/N366	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 3.0	x: 0 m η = 3.1	η = 0.2	x: 0.3 m η = 7.4	x: 0.3 m η = 27.8	x: 0 m η = 8.4	x: 0.3 m η = 1.3	x: 0.3 m η = 7.4	x: 0.3 m η = 27.9	x: 0.3 m η = 0.6	x: 0.3 m η = 8.5	x: 0.3 m η = 46.6	x: 0.3 m η = 37.5	x: 0.3 m η = 38.8	CUMPLE η = 46.6

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barra	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N380/N343	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 0.2$	$\eta = 0.1$	$\eta = 0.4$	x: 0.3 m $\eta = 31.9$	x: 0.3 m $\eta = 19.5$	$\eta = 6.4$	x: 0 m $\eta = 10.5$	x: 0.3 m $\eta = 32.1$	x: 0.3 m $\eta = 19.7$	x: 0.3 m $\eta = 11.4$	x: 0.3 m $\eta = 4.3$	x: 0.3 m $\eta = 64.9$	x: 0.3 m $\eta = 51.4$	x: 0.3 m $\eta = 46.9$	CUMPLE $\eta = 64.9$
N378/N341	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 2.5$	$\eta = 1.3$	$\eta = 0.7$	x: 0.3 m $\eta = 83.0$	x: 0.3 m $\eta = 29.4$	$\eta = 9.5$	x: 0.15 m $\eta = 27.5$	x: 0.3 m $\eta = 83.3$	x: 0.3 m $\eta = 29.7$	x: 0.3 m $\eta = 76.9$	x: 0.3 m $\eta = 9.7$	x: 0.3 m $\eta = 43.1$	x: 0.3 m $\eta = 13.3$	x: 0.3 m $\eta = 25.0$	CUMPLE $\eta = 43.1$
N377/N340	$w/t \le (w/t)_{Max}$ Cumple	x: 0.15 m $\eta = 4.4$	x: 0.15 m $\eta = 5.0$	$\eta = 0.9$	x: 0 m $\eta = 19.4$	x: 0 m $\eta = 27.9$	$\eta = 9.3$	x: 0 m $\eta = 6.2$	x: 0 m $\eta = 19.8$	x: 0 m $\eta = 28.3$	x: 0 m $\eta = 4.3$	x: 0 m $\eta = 8.9$	x: 0 m $\eta = 63.5$	x: 0 m $\eta = 52.9$	x: 0 m $\eta = 47.3$	CUMPLE $\eta = 63.5$
N381/N344	$w/t \le (w/t)_{Max}$ Cumple	x: 0.15 m $\eta < 0.1$	x: 0.15 m $\eta < 0.1$	$\eta = 1.6$	x: 0 m $\eta = 31.7$	x: 0.3 m $\eta = 17.1$	$\eta = 5.7$	x: 0 m $\eta = 44.1$	x: 0 m $\eta = 32.4$	x: 0.3 m $\eta = 17.7$	x: 0 m $\eta = 94.7$	x: 0.3 m $\eta = 3.5$	x: 0 m $\eta = 87.7$	x: 0 m $\eta = 49.8$	x: 0 m $\eta = 74.8$	CUMPLE $\eta = 74.8$
N376/N339	$w/t \le (w/t)_{Max}$ Cumple	x: 0.15 m $\eta < 0.1$	x: 0.15 m $\eta < 0.1$	x: 0.15 m $\eta = 1.1$	x: 0 m $\eta = 28.6$	x: 0 m $\eta = 26.5$	x: 0.15 m $\eta = 10.9$	x: 0 m $\eta = 52.8$	x: 0 m $\eta = 29.1$	x: 0 m $\eta = 27.0$	x: 0 m $\eta = 94.4$	x: 0 m $\eta = 8.5$	x: 0 m $\eta = 94.9$	x: 0 m $\eta = 55.9$	x: 0 m $\eta = 69.1$	CUMPLE $\eta = 69.1$
N382/N345	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 0.1$	x: 0.3 m $\eta = 54.2$	x: 0.3 m $\eta = 4.1$	x: 0.15 m $\eta = 1.7$	x: 0.15 m $\eta = 65.7$	x: 0.3 m $\eta = 54.2$	x: 0.3 m $\eta = 4.1$	x: 0.3 m $\eta = 80.8$	x: 0.3 m $\eta = 0.2$	x: 0.3 m $\eta = 97.9$	x: 0.3 m $\eta = 58.3$	x: 0.3 m $\eta = 71.4$	CUMPLE $\eta = 71.4$
N375/N338	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	x: 0.15 m $\eta = 0.5$	x: 0.3 m $\eta = 24.7$	x: 0.3 m $\eta = 29.9$	x: 0.15 m $\eta = 12.3$	x: 0.15 m $\eta = 51.3$	x: 0.3 m $\eta = 24.9$	x: 0.3 m $\eta = 30.1$	x: 0.3 m $\eta = 82.2$	x: 0.3 m $\eta = 10.6$	x: 0.3 m $\eta = 93.7$	x: 0.3 m $\eta = 55.0$	x: 0.3 m $\eta = 56.5$	CUMPLE $\eta = 56.5$
N383/N346	$w/t \le (w/t)_{Max}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 3.5$	x: 0 m $\eta = 21.9$	x: 0.3 m $\eta = 2.8$	$\eta = 1.2$	x: 0 m $\eta = 50.1$	x: 0 m $\eta = 23.4$	x: 0.3 m $\eta = 4.3$	x: 0 m $\eta = 77.3$	x: 0.3 m $\eta = 0.2$	x: 0 m $\eta = 59.6$	x: 0.3 m $\eta = 27.6$	x: 0 m $\eta = 32.2$	CUMPLE $\eta = 32.2$
N399/N405	$w/t \le (w/t)_{Max}$ Cumple	x: 0.373 m $\eta = 10.4$	x: 0.373 m $\eta = 25.7$	$\eta = 0.3$	x: 1.118 m $\eta = 2.3$	x: 1.118 m $\eta = 4.4$	x: 0.745 m $\eta = 0.5$	x: 0 m $\eta = 0.3$	x: 0 m $\eta = 2.1$	x: 1.118 m $\eta = 4.5$	x: 1.118 m $\eta = 0.1$	x: 1.118 m $\eta = 0.2$	x: 0 m $\eta = 15.7$	x: 0 m $\eta = 30.2$	x: 0 m $\eta = 29.4$	CUMPLE $\eta = 30.2$
N362/N406	$w/t \le (w/t)_{Max}$ Cumple	x: 1.118 m $\eta = 2.8$	x: 0 m $\eta = 23.8$	x: 0.932 m $\eta = 0.4$	x: 1.118 m $\eta = 2.3$	x: 1.118 m $\eta = 4.5$	x: 0 m $\eta = 0.5$	x: 0 m $\eta = 0.2$	x: 0.559 m $\eta = 1.3$	x: 1.118 m $\eta = 4.7$	x: 1.118 m $\eta = 0.1$	x: 1.118 m $\eta = 0.2$	x: 0 m $\eta = 7.1$	x: 1.118 m $\eta = 26.2$	x: 1.118 m $\eta = 26.7$	CUMPLE $\eta = 26.7$
N394/N405	$w/t \le (w/t)_{Max}$ Cumple	x: 1.006 m $\eta = 8.1$	x: 0 m $\eta = 17.5$	x: 0.839 m $\eta = 1.1$	x: 0 m $\eta = 1.8$	x: 0 m $\eta = 2.0$	x: 0 m $\eta = 0.1$	x: 1.006 m $\eta = 0.2$	x: 1.006 m $\eta = 1.2$	x: 0 m $\eta = 2.5$	x: 0 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	N.P.[1]	x: 0 m $\eta = 19.4$	x: 1.006 m $\eta = 19.1$	CUMPLE $\eta = 19.4$
N393/N405	$w/t \le (w/t)_{Max}$ Cumple	x: 0.953 m $\eta = 9.7$	x: 0 m $\eta = 8.2$	$\eta = 0.8$	x: 0 m $\eta = 2.1$	x: 0 m $\eta = 2.2$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 2.1$	x: 0 m $\eta = 2.6$	x: 0 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	N.P.[1]	x: 0 m $\eta = 11.4$	x: 0 m $\eta = 12.5$	CUMPLE $\eta = 12.5$
N357/N406	$w/t \le (w/t)_{Max}$ Cumple	x: 0.168 m $\eta = 3.6$	x: 0.168 m $\eta = 11.4$	$\eta = 0.4$	x: 0 m $\eta = 1.8$	x: 1.006 m $\eta = 7.5$	$\eta = 0.6$	x: 1.006 m $\eta = 0.2$	x: 1.006 m $\eta = 1.0$	x: 1.006 m $\eta = 7.6$	x: 0 m $\eta < 0.1$	x: 1.006 m $\eta = 0.6$	x: 1.006 m $\eta = 10.0$	x: 1.006 m $\eta = 14.9$	x: 1.006 m $\eta = 15.9$	CUMPLE $\eta = 15.9$
N356/N406	$w/t \le (w/t)_{Max}$ Cumple	x: 0.715 m $\eta = 6.7$	x: 0 m $\eta = 4.1$	$\eta = 0.4$	x: 0 m $\eta = 1.2$	x: 0.953 m $\eta = 6.9$	$\eta = 0.6$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 1.2$	x: 0.953 m $\eta = 7.1$	x: 0 m $\eta < 0.1$	x: 0.953 m $\eta = 0.5$	x: 0.953 m $\eta = 14.5$	x: 0.953 m $\eta = 9.0$	x: 0.953 m $\eta = 13.3$	CUMPLE $\eta = 14.5$
N405/N407	$w/t \le (w/t)_{Max}$ Cumple	x: 1.119 m $\eta = 3.8$	x: 0 m $\eta = 28.2$	x: 0 m $\eta = 1.8$	x: 1.119 m $\eta = 2.0$	x: 0 m $\eta = 2.8$	$\eta = 0.2$	x: 0 m $\eta = 0.2$	x: 1.119 m $\eta = 2.1$	x: 0 m $\eta = 3.6$	x: 1.119 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 6.5$	x: 1.119 m $\eta = 30.5$	x: 1.119 m $\eta = 30.7$	CUMPLE $\eta = 30.7$
N407/N408	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m $\eta = 30.6$	$\eta = 3.0$	x: 1.122 m $\eta = 2.1$	x: 1.122 m $\eta = 6.5$	x: 0.935 m $\eta = 1.1$	x: 0 m $\eta = 0.2$	x: 1.122 m $\eta = 2.3$	x: 1.122 m $\eta = 7.8$	x: 1.122 m $\eta = 0.1$	x: 1.122 m $\eta = 0.6$	N.P.[1]	x: 1.122 m $\eta = 33.2$	x: 1.122 m $\eta = 33.2$	CUMPLE $\eta = 33.2$
N406/N409	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m $\eta = 28.4$	$\eta = 0.6$	x: 1.119 m $\eta = 2.0$	x: 0 m $\eta = 3.2$	$\eta = 0.2$	x: 0 m $\eta = 0.1$	x: 0.373 m $\eta = 1.3$	x: 0 m $\eta = 3.3$	x: 1.119 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	N.P.[1]	x: 1.119 m $\eta = 30.5$	x: 1.119 m $\eta = 30.9$	CUMPLE $\eta = 30.9$
N409/N410	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m $\eta = 30.9$	$\eta = 0.7$	x: 1.122 m $\eta = 2.2$	x: 1.122 m $\eta = 6.5$	$\eta = 1.1$	x: 0 m $\eta = 0.1$	x: 1.122 m $\eta = 2.2$	x: 1.122 m $\eta = 6.5$	x: 1.122 m $\eta < 0.1$	x: 1.122 m $\eta = 0.4$	N.P.[1]	x: 1.122 m $\eta = 33.2$	x: 1.122 m $\eta = 33.6$	CUMPLE $\eta = 33.6$
N405/N406	$w/t \le (w/t)_{Max}$ Cumple	x: 0 m $\eta = 3.3$	x: 0 m $\eta = 3.7$	x: 0 m $\eta = 0.4$	x: 0 m $\eta = 15.8$	x: 0.3 m $\eta = 12.1$	x: 0.3 m $\eta = 4.0$	x: 0.3 m $\eta = 2.5$	x: 0 m $\eta = 15.9$	x: 0.3 m $\eta = 12.3$	x: 0 m $\eta = 2.6$	x: 0.3 m $\eta = 1.7$	x: 0 m $\eta = 29.6$	x: 0 m $\eta = 24.9$	x: 0 m $\eta = 24.4$	CUMPLE $\eta = 29.6$
N407/N409	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 2.1$	$\eta = 2.4$	$\eta = 0.5$	x: 0 m $\eta = 7.9$	x: 0 m $\eta = 17.1$	$\eta = 5.6$	x: 0.3 m $\eta = 0.9$	x: 0 m $\eta = 8.1$	x: 0 m $\eta = 17.3$	x: 0 m $\eta = 0.7$	x: 0 m $\eta = 3.3$	x: 0 m $\eta = 33.1$	x: 0 m $\eta = 27.8$	x: 0 m $\eta = 25.9$	CUMPLE $\eta = 33.1$
N408/N410	$w/t \le (w/t)_{Max}$ Cumple	$\eta = 0.9$	$\eta = 1.6$	$\eta = 0.3$	x: 0 m $\eta = 7.1$	x: 0.3 m $\eta = 14.7$	x: 0 m $\eta = 4.9$	x: 0.3 m $\eta = 1.8$	x: 0 m $\eta = 7.3$	x: 0.3 m $\eta = 14.9$	x: 0 m $\eta = 0.6$	x: 0.3 m $\eta = 2.4$	x: 0 m $\eta = 25.1$	x: 0 m $\eta = 22.5$	x: 0 m $\eta = 20.9$	CUMPLE $\eta = 25.1$
N393/N407	$w/t \le (w/t)_{Max}$ Cumple	x: 0.678 m $\eta = 7.2$	x: 0.678 m $\eta = 13.3$	x: 0.17 m $\eta = 1.2$	x: 0 m $\eta = 1.5$	x: 0 m $\eta = 0.8$	x: 0.17 m $\eta = 0.1$	x: 1.017 m $\eta = 0.1$	x: 0 m $\eta = 1.1$	x: 1.017 m $\eta = 1.3$	x: 0 m $\eta < 0.1$	x: 1.017 m $\eta < 0.1$	N.P.[1]	x: 0 m $\eta = 14.7$	x: 0 m $\eta = 14.7$	CUMPLE $\eta = 14.7$
N392/N407	$w/t \le (w/t)_{Max}$ Cumple	x: 0.487 m $\eta = 7.8$	x: 0.487 m $\eta = 7.9$	$\eta = 0.3$	x: 0 m $\eta = 1.5$	x: 0.974 m $\eta = 3.7$	$\eta = 0.2$	x: 0.974 m $\eta = 0.2$	x: 0 m $\eta = 1.5$	x: 0.974 m $\eta = 3.8$	x: 0 m $\eta < 0.1$	x: 0.974 m $\eta = 0.1$	N.P.[1]	x: 0.974 m $\eta = 10.3$	x: 0.974 m $\eta = 10.1$	CUMPLE $\eta = 10.3$
N392/N408	$w/t \le (w/t)_{Max}$ Cumple	x: 0.681 m $\eta = 6.5$	x: 0 m $\eta = 9.8$	x: 1.021 m $\eta = 0.5$	x: 0 m $\eta = 1.1$	x: 0 m $\eta = 5.4$	x: 0.681 m $\eta = 0.4$	x: 1.021 m $\eta = 0.1$	x: 0 m $\eta = 1.1$	x: 0 m $\eta = 5.6$	x: 0 m $\eta < 0.1$	x: 0 m $\eta = 0.3$	x: 0 m $\eta = 8.4$	x: 0 m $\eta = 11.4$	x: 0 m $\eta = 11.1$	CUMPLE $\eta = 11.4$
N391/N408	$w/t \le (w/t)_{Max}$ Cumple	x: 0.985 m $\eta = 6.2$	x: 0 m $\eta = 8.1$	x: 0.492 m $\eta = 0.6$	x: 0 m $\eta = 1.4$	x: 0.985 m $\eta = 8.0$	x: 0.246 m $\eta = 0.7$	x: 0.985 m $\eta = 0.2$	x: 0 m $\eta = 1.4$	x: 0.985 m $\eta = 8.3$	x: 0 m $\eta < 0.1$	x: 0.985 m $\eta = 0.7$	x: 0.985 m $\eta = 11.5$	x: 0.985 m $\eta = 10.2$	x: 0.985 m $\eta = 10.8$	CUMPLE $\eta = 11.5$
N356/N409	$w/t \le (w/t)_{Max}$ Cumple	x: 0.339 m $\eta = 4.7$	x: 0.339 m $\eta = 9.9$	x: 0 m $\eta = 0.3$	x: 0 m $\eta = 1.5$	x: 1.017 m $\eta = 5.1$	x: 0.17 m $\eta = 0.3$	x: 1.017 m $\eta = 0.1$	x: 0 m $\eta = 1.0$	x: 1.017 m $\eta = 5.2$	x: 0 m $\eta < 0.1$	x: 1.017 m $\eta = 0.3$	N.P.[1]	x: 0 m $\eta = 11.3$	x: 1.017 m $\eta = 11.7$	CUMPLE $\eta = 11.7$
N355/N409	$w/t \le (w/t)_{Max}$ Cumple	x: 0.974 m $\eta = 6.2$	x: 0 m $\eta = 5.5$	x: 0.487 m $\eta = 0.9$	x: 0 m $\eta = 1.1$	x: 0 m $\eta = 2.4$	x: 0.731 m $\eta = 0.2$	x: 0.974 m $\eta = 0.1$	x: 0 m $\eta = 1.1$	x: 0 m $\eta = 2.7$	x: 0 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	N.P.[1]	x: 0.974 m $\eta = 8.5$	x: 0.974 m $\eta = 8.9$	CUMPLE $\eta = 8.9$
N355/N410	$w/t \le (w/t)_{Max}$ Cumple	x: 1.021 m $\eta = 5.1$	x: 0 m $\eta = 8.0$	x: 0 m $\eta = 0.6$	x: 0 m $\eta = 1.1$	x: 0 m $\eta = 6.5$	x: 0.681 m $\eta = 0.6$	x: 1.021 m $\eta = 0.1$	x: 0 m $\eta = 1.0$	x: 0 m $\eta = 6.7$	x: 0 m $\eta < 0.1$	x: 0 m $\eta = 0.5$	x: 0 m $\eta = 10.7$	x: 0 m $\eta = 11.2$	x: 0 m $\eta = 11.7$	CUMPLE $\eta = 11.7$
N354/N410	$w/t \le (w/t)_{Max}$ Cumple	x: 0.985 m $\eta = 5.2$	x: 0 m $\eta = 6.9$	x: 0.492 m $\eta = 0.5$	x: 0 m $\eta = 1.2$	x: 0.985 m $\eta = 9.5$	x: 0.246 m $\eta = 0.9$	x: 0.985 m $\eta = 0.1$	x: 0 m $\eta = 1.2$	x: 0.985 m $\eta = 9.7$	x: 0 m $\eta < 0.1$	x: 0.985 m $\eta = 0.9$	x: 0.985 m $\eta = 14.2$	x: 0.985 m $\eta = 12.2$	x: 0.985 m $\eta = 13.5$	CUMPLE $\eta = 14.2$
N391/N411	$w/t \le (w/t)_{Max}$ Cumple	x: 1.026 m $\eta = 6.4$	x: 0 m $\eta = 6.7$	$\eta = 0.1$	x: 0 m $\eta = 0.8$	x: 1.026 m $\eta = 10.1$	x: 0.684 m $\eta = 0.9$	x: 1.026 m $\eta = 0.1$	x: 0 m $\eta = 0.8$	x: 1.026 m $\eta = 10.2$	x: 0 m $\eta < 0.1$	x: 1.026 m $\eta = 1.0$	x: 1.026 m $\eta = 13.7$	x: 0 m $\eta = 9.3$	x: 1.026 m $\eta = 13.5$	CUMPLE $\eta = 13.7$
N390/N411	$w/t \le (w/t)_{Max}$ Cumple	x: 1.007 m $\eta = 4.5$	x: 0 m $\eta = 8.3$	x: 0.504 m $\eta = 0.7$	x: 0 m $\eta = 1.3$	x: 1.007 m $\eta = 7.7$	x: 0.336 m $\eta = 0.7$	x: 1.007 m $\eta = 0.1$	x: 0 m $\eta = 1.4$	x: 1.007 m $\eta = 8.1$	x: 0 m $\eta < 0.1$	x: 1.007 m $\eta = 0.7$	N.P.[1]	x: 0 m $\eta = 10.6$	x: 1.007 m $\eta = 11.4$	CUMPLE $\eta = 11.4$
N408/N411	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m $\eta = 30.9$	$\eta = 1.1$	x: 0.373 m $\eta = 1.8$	x: 1.12 m $\eta = 3.8$	x: 0.933 m $\eta = 0.6$	x: 1.12 m $\eta = 0.1$	x: 1.12 m $\eta = 1.3$	x: 1.12 m $\eta = 4.2$	x: 0.373 m $\eta < 0.1$	x: 1.12 m $\eta = 0.2$	N.P.[1]	x: 0.373 m $\eta = 33.0$	x: 0.373 m $\eta = 33.2$	CUMPLE $\eta = 33.2$
N412/N411	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m $\eta = 29.2$	$\eta = 1.6$	x: 1.122 m $\eta = 2.1$	x: 1.122 m $\eta = 7.0$	x: 0.561 m $\eta = 1.1$	x: 0 m $\eta = 0.2$	x: 1.122 m $\eta = 2.3$	x: 1.122 m $\eta = 7.6$	x: 1.122 m $\eta = 0.1$	x: 1.122 m $\eta = 0.6$	N.P.[1]	x: 1.122 m $\eta = 31.7$	x: 1.122 m $\eta = 31.8$	CUMPLE $\eta = 31.8$
N413/N412	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m $\eta = 26.2$	$\eta = 0.3$	x: 1.131 m $\eta = 1.7$	x: 0 m $\eta = 3.8$	$\eta = 0.3$	x: 0 m $\eta = 0.1$	x: 1.131 m $\eta = 1.8$	x: 0 m $\eta = 4.0$	x: 1.131 m $\eta < 0.1$	x: 0 m $\eta = 0.2$	N.P.[1]	x: 1.131 m $\eta = 28.2$	x: 1.131 m $\eta = 28.3$	CUMPLE $\eta = 28.3$
N414/N413	$w/t \le (w/t)_{Max}$ Cumple	x: 1.128 m $\eta = 1.8$	x: 0 m $\eta = 21.3$	$\eta = 0.5$	x: 1.128 m $\eta = 2.3$	x: 1.128 m $\eta = 4.3$	x: 0.94 m $\eta = 0.3$	x: 0 m $\eta = 0.2$	x: 0.94 m $\eta = 1.2$	x: 1.128 m $\eta = 4.5$	x: 1.128 m $\eta = 0.1$	x: 1.128 m $\eta = 0.2$	N.P.[1]	x: 1.128 m $\eta = 23.7$	x: 1.128 m $\eta = 24.2$	CUMPLE $\eta = 24.2$
N415/N414	$w/t \le (w/t)_{Max}$ Cumple	x: 1.138 m $\eta = 5.1$	x: 0 m $\eta = 14.3$	x: 1.138 m $\eta = 0.9$	x: 1.138 m $\eta = 1.7$	x: 0 m $\eta = 12.0$	x: 1.138 m $\eta = 1.8$	x: 0 m $\eta = 0.3$	x: 0 m $\eta = 1.1$	x: 0 m $\eta = 12.3$	x: 1.138 m $\eta < 0.1$	x: 0 m $\eta = 1.6$	x: 0 m $\eta = 8.4$	x: 0 m $\eta = 18.1$	x: 0 m $\eta = 19.9$	CUMPLE $\eta = 19.9$
N416/N415	$w/t \le (w/t)_{Max}$ Cumple	x: 1.148 m $\eta = 8.8$	x: 0 m $\eta = 13.5$	$\eta = 0.9$	x: 0 m $\eta = 2.0$	x: 1.148 m $\eta = 9.7$	$\eta = 1.3$	x: 0 m $\eta = 0.4$	x: 0 m $\eta = 2.0$	x: 1.148 m $\eta = 10.1$	x: 0 m $\eta < 0.1$	x: 1.148 m $\eta = 1.0$	x: 0 m $\eta = 11.6$	x: 1.148 m $\eta = 15.2$	x: 1.148 m $\eta = 14.9$	CUMPLE $\eta = 15.2$
N417/N416	$w/t \le (w/t)_{Max}$ Cumple	x: 1.129 m $\eta = 13.2$	x: 0 m $\eta = 12.0$	$\eta = 1.7$	x: 1.129 m $\eta = 1.4$	x: 0 m $\eta = 2.4$	$\eta = 0.1$	x: 0 m $\eta = 0.3$	x: 0 m $\eta = 1.5$	x: 0 m $\eta = 3.2$	x: 0 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 8.8$	x: 1.129 m $\eta = 13.4$	x: 0 m $\eta = 14.7$	CUMPLE $\eta = 14.7$

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N418/N417	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.12 m η = 17.6	x: 0 m η = 9.6	x: 0 m η = 0.6	x: 0 m η = 9.3	x: 1.12 m η = 3.8	x: 0 m η = 0.4	x: 0 m η = 1.1	x: 0 m η = 9.3	x: 1.12 m η = 4.0	x: 0 m η = 0.9	x: 1.12 m η = 0.2	x: 0 m η = 28.2	x: 0 m η = 10.9	x: 0 m η = 27.8	CUMPLE η = 28.2
N370/N418	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.902 m η = 21.4	x: 0.451 m η = 7.6	x: 0.677 m η = 4.6	x: 0.902 m η = 8.3	x: 0 m η = 16.3	x: 0.451 m η = 2.6	x: 0.902 m η = 1.6	x: 0.902 m η = 7.6	x: 0 m η = 18.4	x: 0.902 m η = 0.7	x: 0 m η = 3.5	x: 0 m η = 35.7	x: 0 m η = 11.9	x: 0.902 m η = 31.8	CUMPLE η = 35.7
N390/N412	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.034 m η = 6.0	x: 0 m η = 4.1	η = 0.2	x: 0 m η = 0.7	x: 1.034 m η = 4.9	x: 0.172 m η = 0.3	x: 0 m η = 0.1	x: 0 m η = 0.7	x: 1.034 m η = 5.0	x: 0 m η < 0.1	x: 1.034 m η = 0.3	N.P.(1)	x: 0 m η = 5.5	x: 1.034 m η = 8.5	CUMPLE η = 8.5
N389/N412	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.024 m η = 3.6	x: 0 m η = 8.6	x: 0.512 m η = 1.2	x: 0 m η = 1.6	x: 1.024 m η = 2.5	x: 0.341 m η = 0.2	x: 1.024 m η = 0.1	x: 1.024 m η = 1.1	x: 1.024 m η = 3.0	x: 0 m η < 0.1	x: 1.024 m η = 0.1	N.P.(1)	x: 0 m η = 10.0	x: 0 m η = 9.9	CUMPLE η = 10.0
N389/N413	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.013 m η = 6.8	x: 0 m η = 2.7	x: 0.507 m η = 0.8	x: 0 m η = 0.8	x: 0 m η = 1.2	η < 0.1	x: 0 m η = 0.1	x: 0 m η = 0.8	x: 0 m η = 1.6	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 3.5	x: 1.013 m η = 7.6	CUMPLE η = 7.6
N388/N413	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.003 m η = 2.0	x: 0 m η = 12.5	x: 0.502 m η = 0.9	x: 0 m η = 1.9	x: 1.003 m η = 0.8	x: 0.502 m η < 0.1	x: 1.003 m η = 0.2	x: 1.003 m η = 1.1	x: 1.003 m η = 1.2	x: 0 m η < 0.1	x: 1.003 m η < 0.1	N.P.(1)	x: 0 m η = 14.4	x: 0 m η = 14.8	CUMPLE η = 14.8
N388/N414	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.011 m η = 10.7	N.P.(2)	η = 0.9	x: 1.011 m η = 1.2	x: 1.011 m η = 1.1	x: 0.337 m η = 0.1	x: 0 m η = 0.1	x: 0 m η = 1.1	x: 1.011 m η = 1.5	x: 1.011 m η < 0.1	x: 1.011 m η < 0.1	N.P.(1)	N.P.(3)	x: 1.011 m η = 12.2	CUMPLE η = 12.2
N387/N414	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.169 m η = 1.1	x: 0 m η = 16.7	x: 0.169 m η = 0.1	x: 0 m η = 2.2	x: 1.012 m η = 1.8	x: 0.169 m η = 0.1	x: 1.012 m η = 0.2	x: 1.012 m η = 1.2	x: 1.012 m η = 1.8	x: 0 m η < 0.1	x: 1.012 m η < 0.1	N.P.(1)	x: 0 m η = 19.1	x: 0 m η = 19.5	CUMPLE η = 19.5
N387/N415	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.999 m η = 12.8	N.P.(2)	η = 0.5	x: 0 m η = 1.3	x: 0.999 m η = 6.9	x: 0.25 m η = 0.7	x: 0 m η = 0.2	x: 0 m η = 1.3	x: 0.999 m η = 7.1	x: 0 m η < 0.1	x: 0.999 m η = 0.5	x: 0.999 m η = 15.6	N.P.(3)	x: 0 m η = 14.4	CUMPLE η = 15.6
N386/N415	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 0.6	x: 0 m η = 21.0	x: 0.993 m η = 0.3	x: 0 m η = 2.3	x: 0 m η = 6.3	η = 0.6	x: 0.993 m η = 0.2	x: 0.993 m η = 1.4	x: 0 m η = 6.4	x: 0 m η = 0.1	x: 0 m η = 0.4	N.P.(1)	x: 0 m η = 23.7	x: 0 m η = 23.9	CUMPLE η = 23.9
N386/N416	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.968 m η = 15.3	N.P.(2)	η = 1.0	x: 0 m η = 2.1	x: 0 m η = 1.9	η = 0.1	x: 0 m η = 0.2	x: 0 m η = 1.5	x: 0 m η = 2.3	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.(1)	N.P.(3)	x: 0 m η = 17.8	CUMPLE η = 17.8
N385/N416	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 25.9	x: 0.235 m η = 0.3	x: 0.941 m η = 2.0	x: 0.941 m η = 5.4	x: 0 m η = 0.4	x: 0.941 m η = 0.2	x: 0.941 m η = 1.2	x: 0.941 m η = 5.5	x: 0.941 m η < 0.1	x: 0.941 m η = 0.3	N.P.(1)	x: 0.941 m η = 28.2	x: 0.941 m η = 28.3	CUMPLE η = 28.3
N385/N417	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.971 m η = 18.0	N.P.(2)	x: 0 m η = 0.3	x: 0 m η = 2.4	x: 0 m η = 3.9	x: 0 m η = 0.4	x: 0 m η = 0.3	x: 0 m η = 1.5	x: 0 m η = 4.0	x: 0 m η = 0.1	x: 0 m η = 0.2	N.P.(1)	N.P.(3)	x: 0 m η = 21.0	CUMPLE η = 21.0
N384/N417	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 29.5	x: 0.71 m η = 0.5	x: 0 m η = 5.4	x: 0.947 m η = 5.6	x: 0.71 m η = 0.4	x: 0.947 m η = 0.6	x: 0.947 m η = 2.8	x: 0.947 m η = 5.8	x: 0 m η = 0.3	x: 0.947 m η = 0.3	N.P.(1)	x: 0 m η = 35.7	x: 0 m η = 36.3	CUMPLE η = 36.3
N384/N418	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.981 m η = 16.4	N.P.(2)	x: 0 m η = 0.4	x: 0 m η = 4.0	x: 0.981 m η = 4.5	x: 0.245 m η = 0.3	x: 0 m η = 0.2	x: 0 m η = 2.0	x: 0.981 m η = 4.7	x: 0 m η = 0.2	x: 0.981 m η = 0.2	N.P.(1)	N.P.(3)	x: 0 m η = 21.4	CUMPLE η = 21.4
N372/N418	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 29.5	x: 0.402 m η = 2.2	x: 0 m η = 4.4	x: 0 m η = 11.5	x: 0.804 m η = 0.9	x: 0.804 m η = 0.6	x: 0 m η = 4.4	x: 0 m η = 12.4	x: 0 m η = 0.2	x: 0 m η = 1.6	N.P.(1)	x: 0.804 m η = 33.2	x: 0.804 m η = 33.2	CUMPLE η = 33.2
N354/N419	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.026 m η = 5.8	x: 0 m η = 5.9	x: 1.026 m η = 0.7	x: 0 m η = 0.8	x: 0 m η = 6.5	x: 0.513 m η = 0.6	x: 1.026 m η = 0.1	x: 0 m η = 0.8	x: 0 m η = 6.8	x: 0 m η < 0.1	x: 0 m η = 0.5	x: 0 m η = 10.5	x: 0 m η = 7.5	x: 0 m η = 9.6	CUMPLE η = 10.5
N353/N419	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.336 m η = 4.1	x: 0.336 m η = 8.1	η = 0.2	x: 0 m η = 1.4	x: 0 m η = 5.8	x: 0.671 m η = 0.5	x: 1.007 m η = 0.1	x: 0 m η = 1.1	x: 0 m η = 5.8	x: 0 m η < 0.1	x: 0 m η = 0.3	x: 0 m η = 8.5	x: 0 m η = 10.4	x: 0 m η = 11.2	CUMPLE η = 11.2
N353/N420	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.034 m η = 6.1	x: 0 m η = 4.1	x: 1.034 m η = 1.0	x: 0 m η = 0.7	x: 1.034 m η = 2.1	x: 0.345 m η = 0.2	x: 0 m η = 0.1	x: 1.034 m η = 0.9	x: 1.034 m η = 2.5	x: 1.034 m η < 0.1	x: 1.034 m η = 0.1	N.P.(1)	x: 1.034 m η = 5.3	x: 1.034 m η = 7.4	CUMPLE η = 7.4
N410/N419	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 31.9	x: 1.12 m η = 1.7	x: 0.373 m η = 1.9	x: 1.12 m η = 3.6	x: 0.933 m η = 0.6	x: 1.12 m η = 0.1	x: 0.56 m η = 1.7	x: 1.12 m η = 3.9	x: 0.373 m η < 0.1	x: 1.12 m η = 0.2	N.P.(1)	x: 0.373 m η = 33.9	x: 0.373 m η = 34.2	CUMPLE η = 34.2
N420/N419	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 29.5	η = 0.3	x: 1.122 m η = 2.1	x: 1.122 m η = 7.1	x: 0.561 m η = 1.2	x: 0 m η = 0.2	x: 1.122 m η = 2.2	x: 1.122 m η = 7.2	x: 1.122 m η < 0.1	x: 1.122 m η = 0.5	N.P.(1)	x: 1.122 m η = 31.8	x: 1.122 m η = 32.2	CUMPLE η = 32.2
N352/N420	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.341 m η = 3.8	x: 0.341 m η = 9.0	η = 0.1	x: 0 m η = 1.6	x: 1.024 m η = 4.6	x: 0.171 m η = 0.3	x: 1.024 m η = 0.1	x: 1.024 m η = 1.1	x: 1.024 m η = 4.7	x: 0 m η < 0.1	x: 1.024 m η = 0.2	N.P.(1)	x: 1.024 m η = 10.3	x: 1.024 m η = 10.7	CUMPLE η = 10.7
N421/N420	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 26.4	η = 0.9	x: 1.131 m η = 1.7	x: 0 m η = 3.8	η = 0.3	x: 0 m η = 0.1	x: 1.131 m η = 1.7	x: 0 m η = 4.2	x: 1.131 m η < 0.1	x: 0 m η = 0.2	N.P.(1)	x: 1.131 m η = 28.2	x: 1.131 m η = 28.6	CUMPLE η = 28.6
N352/N421	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.013 m η = 6.9	x: 0.844 m η = 3.2	η = 0.1	x: 0 m η = 0.9	x: 1.013 m η = 4.4	x: 0.675 m η = 0.4	x: 0 m η = 0.1	x: 0 m η = 0.9	x: 1.013 m η = 4.5	x: 0 m η < 0.1	x: 1.013 m η = 0.2	N.P.(1)	x: 1.013 m η = 5.6	x: 1.013 m η = 10.1	CUMPLE η = 10.1
N351/N421	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.167 m η = 2.2	x: 0 m η = 12.7	η < 0.1	x: 0 m η = 1.9	x: 1.003 m η = 4.7	x: 0.334 m η = 0.4	x: 1.003 m η = 0.2	x: 1.003 m η = 1.1	x: 1.003 m η = 4.7	x: 0 m η < 0.1	x: 1.003 m η = 0.2	N.P.(1)	x: 0 m η = 14.6	x: 0 m η = 15.1	CUMPLE η = 15.1
N351/N422	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.011 m η = 10.9	x: 0 m η = 0.4	x: 0 m η = 0.5	x: 1.011 m η = 1.2	x: 1.011 m η = 0.8	η < 0.1	x: 0 m η = 0.1	x: 0 m η = 1.1	x: 1.011 m η = 1.0	x: 1.011 m η < 0.1	x: 1.011 m η < 0.1	N.P.(1)	x: 0 m η = 1.4	x: 1.011 m η = 12.4	CUMPLE η = 12.4
N422/N421	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.128 m η = 2.3	x: 0 m η = 21.4	η = 1.1	x: 1.128 m η = 2.3	x: 1.128 m η = 4.2	x: 0.94 m η = 0.3	x: 0 m η = 0.2	x: 1.128 m η = 2.3	x: 1.128 m η = 4.6	x: 1.128 m η = 0.1	x: 1.128 m η = 0.2	N.P.(1)	x: 1.128 m η = 23.9	x: 1.128 m η = 24.3	CUMPLE η = 24.3
N350/N422	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 1.4	x: 0 m η = 17.0	x: 0.506 m η = 0.4	x: 0 m η = 2.2	x: 0 m η = 0.5	η < 0.1	x: 1.012 m η = 0.2	x: 1.012 m η = 1.2	x: 0 m η = 0.7	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 19.5	x: 0 m η = 19.7	CUMPLE η = 19.7
N423/N422	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.138 m η = 5.8	x: 0 m η = 14.9	η = 0.3	x: 1.138 m η = 1.7	x: 0 m η = 12.2	x: 0.569 m η = 1.8	x: 0 m η = 0.3	x: 0 m η = 1.2	x: 0 m η = 12.3	x: 1.138 m η < 0.1	x: 0 m η = 1.5	x: 0 m η = 5.0	x: 0 m η = 19.4	x: 0 m η = 21.8	CUMPLE η = 21.8
N350/N423	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.999 m η = 12.9	N.P.(2)	x: 0.25 m η = 0.5	x: 0 m η = 1.4	x: 0.999 m η = 7.5	η = 0.7	x: 0 m η = 0.2	x: 0 m η = 1.4	x: 0.999 m η = 7.7	x: 0 m η < 0.1	x: 0.999 m η = 0.6	x: 0.999 m η = 17.4	N.P.(3)	x: 0.999 m η = 15.8	CUMPLE η = 17.4
N349/N423	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 0.8	x: 0 m η = 21.4	η = 0.2	x: 0 m η = 2.4	x: 0 m η = 6.3	η = 0.6	x: 0.993 m η = 0.2	x: 0.993 m η = 1.4	x: 0 m η = 6.4	x: 0 m η = 0.1	x: 0 m η = 0.4	x: 0.993 m η = 7.1	x: 0 m η = 24.0	x: 0 m η = 24.4	CUMPLE η = 24.4
N349/N424	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.968 m η = 15.5	x: 0.242 m η = 0.4	x: 0 m η = 0.2	x: 0 m η = 2.1	x: 0.968 m η = 4.3	x: 0 m η = 0.2	x: 0 m η = 0.2	x: 0 m η = 1.6	x: 0.968 m η = 4.4	x: 0 m η < 0.1	x: 0.968 m η = 0.2	N.P.(1)	x: 0.968 m η = 4.8	x: 0 m η = 18.1	CUMPLE η = 18.1
N424/N423	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.148 m η = 9.1	x: 0 m η = 14.2	x: 0.957 m η = 2.7	x: 0 m η = 2.0	x: 1.148 m η = 10.0	x: 0.957 m η = 1.4	x: 0 m η = 0.4	x: 1.148 m η = 2.1	x: 1.148 m η = 11.1	x: 1.148 m η < 0.1	x: 1.148 m η = 1.3	x: 0.957 m η = 12.5	x: 1.148 m η = 16.7	x: 1.148 m η = 15.9	CUMPLE η = 16.7
N348/N424	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 26.3	η = 1.2	x: 0.941 m η = 2.0	x: 0 m η = 0.7	η < 0.1	x: 0.941 m η = 0.2	x: 0.941 m η = 1.6	x: 0 m η = 1.2	x: 0.941 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0.941 m η = 28.5	x: 0.941 m η = 28.7	CUMPLE η = 28.7
N425/N424	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.129 m η = 13.5	x: 0 m η = 12.6	η = 0.5	x: 1.129 m η = 1.5	x: 0 m η = 2.4	η = 0.1	x: 0 m η = 0.3	x: 1.129 m η = 1.5	x: 0 m η = 2.7	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 8.6	x: 1.129 m η = 14.1	x: 0 m η = 14.9	CUMPLE η = 14.9
N348/N425	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.971 m η = 18.3	N.P.(2)	η = 0.2	x: 0 m η = 2.4	x: 0 m η = 3.2	x: 0.243 m η = 0.3	x: 0 m η = 0.3	x: 0 m η = 1.6	x: 0 m η = 3.3	x: 0 m η = 0.1	x: 0 m η = 0.1	N.P.(1)	N.P.(3)	x: 0 m η = 21.3	CUMPLE η = 21.3
N347/N425	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 29.9	η = 0.2	x: 0 m η = 5.5	x: 0.947 m η = 3.3	x: 0.71 m η = 0.3	x: 0.947 m η = 0.6	x: 0.947 m η = 2.7	x: 0.947 m η = 3.4	x: 0 m η = 0.3	x: 0.947 m η = 0.1	N.P.(1)	x: 0 m η = 36.2	x: 0 m η = 36.7	CUMPLE η = 36.7
N426/N425	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.187 m η = 17.9	x: 0.187 m η = 10.1	x: 0 m η = 1.3	x: 0 m η = 9.3	x: 1.12 m η = 3.8	x: 0 m η = 0.4	x: 0 m η = 1.1	x: 0 m η = 9.4	x: 1.12 m η = 4.3	x: 0 m η = 0.9	x: 1.12 m η = 0.2	x: 0 m η = 27.9	x: 0 m η = 11.8	x: 0 m η = 27.8	CUMPLE η = 27.9

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N347/N426	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.981 m η = 16.6	N.P.[2]	η = 0.3	x: 0 m η = 4.1	x: 0.981 m η = 3.8	x: 0 m η = 0.2	x: 0 m η = 0.2	x: 0 m η = 2.1	x: 0.981 m η = 3.9	x: 0 m η = 0.2	x: 0.981 m η = 0.2	N.P.[1]	N.P.[3]	x: 0 m η = 21.7	CUMPLE η = 21.7
N334/N426	$w / t \leq (w / t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 29.9	x: 0.803 m η = 2.2	x: 0 m η = 4.4	x: 0 m η = 12.1	η = 1.0	x: 0.804 m η = 0.6	x: 0 m η = 4.4	x: 0 m η = 13.1	x: 0 m η = 0.2	x: 0 m η = 1.7	N.P.[1]	x: 0.804 m η = 33.1	x: 0.804 m η = 33.5	CUMPLE η = 33.5
N333/N426	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.902 m η = 21.4	x: 0 m η = 8.1	x: 0.451 m η = 5.1	x: 0.902 m η = 8.4	x: 0 m η = 16.9	η = 2.7	x: 0.902 m η = 1.7	x: 0.902 m η = 8.4	x: 0 m η = 19.2	x: 0.902 m η = 0.7	x: 0 m η = 3.7	x: 0 m η = 45.6	x: 0 m η = 22.4	x: 0 m η = 35.4	CUMPLE η = 45.6
N411/N419	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.15 m η = 3.3	x: 0.15 m η = 4.1	η = 0.2	x: 0.3 m η = 10.6	x: 0 m η = 14.2	η = 4.7	x: 0 m η = 2.2	x: 0.3 m η = 10.6	x: 0 m η = 14.2	x: 0.3 m η = 1.2	x: 0 m η = 2.2	x: 0.3 m η = 33.5	x: 0.3 m η = 27.6	x: 0.3 m η = 25.1	CUMPLE η = 33.5
N412/N420	$w / t \leq (w / t)_{Máx.}$ Cumple	η = 3.1	η = 3.5	η = 0.3	x: 0 m η = 8.2	x: 0 m η = 20.7	η = 6.7	x: 0.3 m η = 0.4	x: 0 m η = 8.4	x: 0 m η = 20.8	x: 0 m η = 0.7	x: 0 m η = 4.8	x: 0 m η = 39.0	x: 0 m η = 32.7	x: 0 m η = 31.4	CUMPLE η = 39.0
N413/N421	$w / t \leq (w / t)_{Máx.}$ Cumple	η = 2.3	η = 2.5	x: 0.3 m η = 0.2	x: 0 m η = 10.9	x: 0.3 m η = 3.4	x: 0.3 m η = 1.1	x: 0.3 m η = 1.7	x: 0 m η = 11.0	x: 0.3 m η = 3.4	x: 0 m η = 1.2	x: 0.3 m η = 0.1	x: 0 m η = 16.2	x: 0 m η = 13.8	x: 0 m η = 16.1	CUMPLE η = 16.2
N414/N422	$w / t \leq (w / t)_{Máx.}$ Cumple	η = 0.6	η = 0.8	η = 0.1	x: 0 m η = 11.0	x: 0.3 m η = 26.8	x: 0 m η = 8.8	x: 0.3 m η = 2.9	x: 0 m η = 11.0	x: 0.3 m η = 26.8	x: 0 m η = 1.3	x: 0.3 m η = 8.0	x: 0 m η = 46.5	x: 0 m η = 37.6	x: 0 m η = 35.8	CUMPLE η = 46.5
N415/N423	$w / t \leq (w / t)_{Máx.}$ Cumple	η = 2.0	η = 2.5	x: 0.15 m η = 0.3	x: 0 m η = 4.2	x: 0 m η = 11.1	x: 0.3 m η = 3.7	x: 0.3 m η = 1.3	x: 0 m η = 4.4	x: 0 m η = 11.2	x: 0 m η = 0.2	x: 0 m η = 1.4	x: 0 m η = 21.4	x: 0 m η = 16.9	x: 0 m η = 16.7	CUMPLE η = 21.4
N416/N424	$w / t \leq (w / t)_{Máx.}$ Cumple	η = 2.7	η = 2.9	η = 0.6	x: 0 m η = 6.8	x: 0.3 m η = 15.9	η = 4.8	x: 0.3 m η = 0.7	x: 0 m η = 7.1	x: 0.3 m η = 16.2	x: 0 m η = 0.5	x: 0.3 m η = 2.8	x: 0 m η = 27.4	x: 0 m η = 22.4	x: 0.3 m η = 22.8	CUMPLE η = 27.4
N417/N425	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0 m η = 0.6	x: 0 m η = 0.7	η = 0.6	x: 0.3 m η = 6.2	x: 0 m η = 5.2	x: 0.3 m η = 1.5	x: 0.3 m η = 1.4	x: 0.3 m η = 6.5	x: 0 m η = 5.4	x: 0.3 m η = 0.4	x: 0 m η = 0.3	x: 0.3 m η = 13.5	x: 0.3 m η = 11.1	x: 0.3 m η = 9.7	CUMPLE η = 13.5
N418/N426	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.3 m η = 3.1	x: 0.3 m η = 3.3	x: 0.15 m η = 0.2	x: 0 m η = 10.7	x: 0 m η = 33.4	η = 11.1	x: 0.3 m η = 3.4	x: 0 m η = 10.8	x: 0 m η = 33.5	x: 0 m η = 1.3	x: 0 m η = 12.4	x: 0 m η = 58.4	x: 0 m η = 47.2	x: 0 m η = 46.8	CUMPLE η = 58.4
N341/N434	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.315 m η = 10.9	x: 0.315 m η = 12.0	x: 0.315 m η = 1.2	x: 0 m η = 6.6	x: 0 m η = 2.5	x: 0.315 m η = 0.2	x: 0 m η = 0.7	x: 0 m η = 7.0	x: 0 m η = 3.0	x: 0 m η = 0.5	x: 0 m η = 0.1	x: 0 m η = 23.5	x: 0 m η = 19.4	x: 0 m η = 19.7	CUMPLE η = 23.5
N434/N433	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.63 m η = 8.1	x: 0.63 m η = 9.2	η = 0.2	x: 0 m η = 0.9	x: 0.63 m η = 1.4	η = 0.1	x: 0 m η = 0.1	x: 0 m η = 1.0	x: 0.63 m η = 1.5	x: 0 m η < 0.1	x: 0.63 m η < 0.1	N.P.[1]	x: 0 m η = 11.1	x: 0 m η = 10.9	CUMPLE η = 11.1
N433/N432	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.473 m η = 5.7	x: 0.473 m η = 6.6	η = 0.4	x: 0 m η = 0.7	x: 0.63 m η = 1.4	η = 0.1	x: 0 m η = 0.1	x: 0 m η = 0.8	x: 0.63 m η = 1.6	x: 0 m η < 0.1	x: 0.63 m η < 0.1	N.P.[1]	x: 0 m η = 8.0	x: 0.63 m η = 7.6	CUMPLE η = 8.0
N432/N431	$w / t \leq (w / t)_{Máx.}$ Cumple	η = 3.2	η = 3.8	η = 0.5	x: 0 m η = 0.7	x: 0.63 m η = 1.1	η < 0.1	x: 0 m η = 0.1	x: 0 m η = 0.9	x: 0.63 m η = 1.3	x: 0 m η < 0.1	x: 0.63 m η < 0.1	N.P.[1]	x: 0.63 m η = 5.4	x: 0.63 m η = 4.9	CUMPLE η = 5.4
N431/N430	$w / t \leq (w / t)_{Máx.}$ Cumple	η = 1.0	η = 1.3	η = 0.5	x: 0 m η = 0.7	x: 0.63 m η = 1.0	η < 0.1	x: 0.63 m η = 0.1	x: 0 m η = 0.9	x: 0.63 m η = 1.2	x: 0 m η < 0.1	x: 0.63 m η < 0.1	N.P.[1]	x: 0.63 m η = 3.2	x: 0.63 m η = 2.7	CUMPLE η = 3.2
N430/N429	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.315 m η = 1.6	x: 0.315 m η = 1.8	η = 0.5	x: 0 m η = 0.6	x: 0 m η = 1.4	η < 0.1	x: 0.63 m η = 0.1	x: 0 m η = 0.9	x: 0 m η = 1.6	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0.63 m η = 3.1	x: 0 m η = 3.5	CUMPLE η = 3.5
N429/N428	$w / t \leq (w / t)_{Máx.}$ Cumple	η = 4.0	η = 4.4	η = 0.6	x: 0.63 m η = 1.7	x: 0 m η = 1.5	η = 0.1	x: 0.63 m η = 0.2	x: 0.63 m η = 1.9	x: 0 m η = 1.8	x: 0.63 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0.63 m η = 7.5	x: 0.63 m η = 6.7	CUMPLE η = 7.5
N428/N427	$w / t \leq (w / t)_{Máx.}$ Cumple	η = 6.7	η = 7.2	x: 0 m η = 0.3	x: 0.63 m η = 2.0	x: 0 m η = 1.6	x: 0 m η = 0.2	x: 0 m η = 0.2	x: 0.63 m η = 2.1	x: 0 m η = 1.7	x: 0.63 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0.63 m η = 10.1	x: 0.63 m η = 9.6	CUMPLE η = 10.1
N427/N280	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0 m η = 8.3	x: 0 m η = 8.2	η = 1.5	x: 0.49 m η = 8.2	x: 0.49 m η = 5.0	η = 0.5	x: 0.49 m η = 0.9	x: 0.49 m η = 8.9	x: 0.49 m η = 5.6	x: 0.49 m η = 0.8	x: 0.49 m η = 0.3	x: 0.49 m η = 26.3	x: 0.49 m η = 16.4	x: 0.49 m η = 20.2	CUMPLE η = 26.3
N340/N435	$w / t \leq (w / t)_{Máx.}$ Cumple	η = 6.2	η = 7.2	η = 2.3	x: 0 m η = 39.1	x: 0 m η = 15.1	x: 0.49 m η = 1.4	x: 0.49 m η = 5.5	x: 0 m η = 39.7	x: 0 m η = 15.7	x: 0 m η = 16.1	x: 0 m η = 2.5	x: 0 m η = 75.3	x: 0 m η = 59.1	x: 0 m η = 58.5	CUMPLE η = 75.3
N435/N436	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.63 m η = 5.0	x: 0.63 m η = 5.5	η = 0.1	x: 0 m η = 5.7	x: 0 m η = 3.1	η = 0.2	x: 0 m η = 0.6	x: 0 m η = 5.7	x: 0 m η = 3.1	x: 0 m η = 0.3	x: 0 m η = 0.1	x: 0 m η = 15.9	x: 0 m η = 11.5	x: 0 m η = 12.9	CUMPLE η = 15.9
N436/N437	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.63 m η = 2.8	x: 0.63 m η = 2.5	η = 0.4	x: 0 m η = 1.5	x: 0 m η = 1.9	x: 0.63 m η = 0.2	x: 0 m η = 0.2	x: 0 m η = 1.7	x: 0 m η = 2.0	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 6.0	x: 0 m η = 5.6	CUMPLE η = 6.0
N437/N438	$w / t \leq (w / t)_{Máx.}$ Cumple	η = 1.5	η = 0.6	η = 0.5	x: 0.63 m η = 0.6	x: 0 m η = 1.6	x: 0.473 m η = 0.1	x: 0 m η = 0.1	x: 0.63 m η = 0.8	x: 0 m η = 1.8	x: 0.63 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0.473 m η = 1.3	x: 0 m η = 2.6	CUMPLE η = 2.6
N438/N439	$w / t \leq (w / t)_{Máx.}$ Cumple	η = 3.0	η = 2.3	η = 0.5	x: 0.63 m η = 0.6	x: 0.63 m η = 1.5	η = 0.1	x: 0 m η = 0.1	x: 0.63 m η = 0.8	x: 0.63 m η = 1.7	x: 0.63 m η < 0.1	x: 0.63 m η < 0.1	N.P.[1]	x: 0.63 m η = 4.5	x: 0 m η = 4.9	CUMPLE η = 4.9
N439/N440	$w / t \leq (w / t)_{Máx.}$ Cumple	η = 5.3	η = 5.1	η = 0.5	x: 0.63 m η = 0.5	x: 0.63 m η = 1.7	η = 0.1	x: 0.63 m η = 0.1	x: 0.63 m η = 0.8	x: 0.63 m η = 1.9	x: 0.63 m η < 0.1	x: 0.63 m η < 0.1	N.P.[1]	x: 0.63 m η = 7.6	x: 0.63 m η = 7.1	CUMPLE η = 7.6
N440/N441	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.315 m η = 7.6	x: 0.315 m η = 8.0	η = 0.5	x: 0.63 m η = 1.1	x: 0.63 m η = 1.8	η = 0.2	x: 0.63 m η = 0.2	x: 0.63 m η = 1.3	x: 0.63 m η = 2.0	x: 0.63 m η < 0.1	x: 0.63 m η < 0.1	N.P.[1]	x: 0.63 m η = 11.2	x: 0.63 m η = 10.5	CUMPLE η = 11.2
N441/N442	$w / t \leq (w / t)_{Máx.}$ Cumple	η = 9.8	η = 10.8	η = 0.4	x: 0.63 m η = 3.3	x: 0.63 m η = 2.4	η = 0.1	x: 0.63 m η = 0.4	x: 0.63 m η = 3.5	x: 0.63 m η = 2.5	x: 0.63 m η = 0.1	x: 0.63 m η = 0.1	N.P.[1]	x: 0.63 m η = 15.4	x: 0.63 m η = 14.9	CUMPLE η = 15.4
N442/N279	$w / t \leq (w / t)_{Máx.}$ Cumple	η = 12.1	η = 14.0	η = 1.4	x: 0.63 m η = 29.2	x: 0.63 m η = 11.1	η = 0.8	x: 0.63 m η = 3.2	x: 0.63 m η = 29.8	x: 0.63 m η = 11.3	x: 0.63 m η = 9.0	x: 0.63 m η = 1.3	x: 0.63 m η = 61.9	x: 0.63 m η = 52.7	x: 0.63 m η = 51.8	CUMPLE η = 61.9
N279/N427	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.929 m η = 1.8	x: 0 m η = 3.1	x: 0.697 m η = 1.8	x: 0 m η = 18.3	x: 0 m η = 10.4	x: 0.929 m η = 0.7	x: 0.929 m η = 1.4	x: 0 m η = 19.1	x: 0 m η = 10.7	x: 0 m η = 3.7	x: 0 m η = 1.1	x: 0 m η = 38.1	x: 0 m η = 32.0	x: 0 m η = 29.0	CUMPLE η = 38.1
N442/N427	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.802 m η = 2.5	x: 0 m η = 2.4	η = 0.5	x: 0.802 m η = 3.7	x: 0 m η = 4.3	x: 0.602 m η = 0.5	x: 0 m η = 0.5	x: 0.802 m η = 3.8	x: 0 m η = 4.3	x: 0.802 m η = 0.1	x: 0 m η = 0.2	N.P.[1]	x: 0 m η = 9.9	x: 0 m η = 9.4	CUMPLE η = 9.9
N442/N428	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.929 m η = 3.5	x: 0 m η = 5.4	x: 0.929 m η = 0.4	x: 0 m η = 3.0	x: 0 m η = 0.4	η < 0.1	x: 0.929 m η = 0.3	x: 0 m η = 3.2	x: 0 m η = 0.4	x: 0 m η = 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 8.5	x: 0 m η = 9.0	CUMPLE η = 9.0
N441/N428	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.802 m η = 3.3	x: 0 m η = 3.7	η = 0.6	x: 0 m η = 0.3	x: 0.802 m η = 0.5	η < 0.1	x: 0 m η < 0.1	x: 0 m η = 0.6	x: 0.802 m η = 0.7	x: 0 m η < 0.1	x: 0.802 m η < 0.1	N.P.[1]	x: 0.201 m η = 4.7	x: 0.802 m η = 4.2	CUMPLE η = 4.7
N441/N429	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.929 m η = 3.2	x: 0 m η = 4.8	η = 0.2	x: 0.929 m η = 0.7	x: 0 m η = 0.2	η < 0.1	x: 0.929 m η = 0.1	x: 0.929 m η = 0.8	x: 0 m η = 0.2	x: 0.929 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0.929 m η = 5.7	x: 0.929 m η = 5.7	CUMPLE η = 5.7
N440/N429	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.802 m η = 3.1	x: 0 m η = 3.6	x: 0.602 m η = 0.7	x: 0.802 m η = 0.8	x: 0 m η = 0.8	η = 0.1	x: 0 m η = 0.1	x: 0.802 m η = 1.1	x: 0 m η = 1.1	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 5.1	x: 0.802 m η = 4.6	CUMPLE η = 5.1
N440/N430	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.929 m η = 3.4	x: 0 m η = 4.8	η = 0.3	x: 0.929 m η = 0.7	x: 0 m η = 0.5	η < 0.1	x: 0.929 m η = 0.1	x: 0.929 m η = 0.8	x: 0 m η = 0.6	x: 0.929 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 5.6	x: 0.929 m η = 5.6	CUMPLE η = 5.6
N439/N430	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.802 m η = 3.0	x: 0 m η = 3.7	x: 0.602 m η = 0.6	x: 0.802 m η = 0.7	x: 0 m η = 0.6	η < 0.1	x: 0 m η = 0.1	x: 0.802 m η = 0.9	x: 0 m η = 0.9	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 4.9	x: 0 m η = 4.5	CUMPLE η = 4.9
N439/N431	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.929 m η = 3.4	x: 0 m η = 4.6	η = 0.4	x: 0.929 m η = 0.6	x: 0 m η = 0.6	η < 0.1	x: 0 m η = 0.1	x: 0.929 m η = 0.8	x: 0 m η = 0.8	x: 0.929 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 5.4	x: 0.929 m η = 5.4	CUMPLE η = 5.4



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))														Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N438/N431	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 2.9	x: 0 m η = 3.8	x: 0.602 m η = 0.5	x: 0.802 m η = 0.7	x: 0 m η = 0.6	η < 0.1	x: 0 m η = 0.1	x: 0.802 m η = 0.9	x: 0 m η = 0.8	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 4.8	x: 0.802 m η = 4.7	CUMPLE η = 4.8
N438/N432	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 3.5	x: 0 m η = 4.5	η = 0.5	x: 0.929 m η = 0.6	x: 0 m η = 0.7	η < 0.1	x: 0 m η = 0.1	x: 0.929 m η = 0.8	x: 0 m η = 0.9	x: 0.929 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 5.5	x: 0 m η = 5.3	CUMPLE η = 5.5
N437/N432	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 2.9	x: 0 m η = 3.9	x: 0.602 m η = 0.3	x: 0.802 m η = 0.7	x: 0 m η = 0.6	η = 0.1	x: 0.802 m η = 0.1	x: 0.802 m η = 0.9	x: 0 m η = 0.7	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 5.0	x: 0.802 m η = 4.8	CUMPLE η = 5.0
N437/N433	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 3.6	x: 0 m η = 4.4	η = 0.6	x: 0.929 m η = 0.6	x: 0 m η = 0.8	η < 0.1	x: 0 m η = 0.1	x: 0.929 m η = 0.9	x: 0 m η = 1.0	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 5.9	x: 0 m η = 5.4	CUMPLE η = 5.9
N436/N433	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 2.8	x: 0 m η = 4.0	x: 0 m η = 0.1	x: 0.802 m η = 0.6	x: 0 m η = 0.1	η < 0.1	x: 0.802 m η < 0.1	x: 0.802 m η = 0.6	x: 0.802 m η = 0.2	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0.802 m η = 4.7	x: 0.802 m η = 4.7	CUMPLE η = 4.7
N436/N434	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 3.9	x: 0 m η = 4.6	η = 0.7	x: 0 m η = 0.3	x: 0 m η = 0.8	η = 0.1	x: 0 m η = 0.1	x: 0 m η = 0.6	x: 0 m η = 1.1	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 6.2	x: 0 m η = 5.6	CUMPLE η = 6.2
N435/N434	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 2.8	x: 0 m η = 4.2	η = 0.6	x: 0 m η = 4.8	x: 0 m η = 3.1	η = 0.3	x: 0 m η = 0.5	x: 0 m η = 5.0	x: 0 m η = 3.3	x: 0 m η = 0.3	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 11.4	x: 0 m η = 10.5	CUMPLE η = 11.4
N435/N341	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 2.0	x: 0 m η = 1.5	η = 0.5	x: 0 m η = 2.9	x: 0.929 m η = 3.7	η = 0.3	x: 0.929 m η = 0.1	x: 0 m η = 3.1	x: 0.929 m η = 3.9	x: 0 m η = 0.1	x: 0.929 m η = 0.2	N.P.[1]	x: 0.929 m η = 6.6	x: 0.929 m η = 7.6	CUMPLE η = 7.6
N333/N443	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 9.7	η = 10.8	η = 1.1	x: 0 m η = 7.9	x: 0 m η = 16.9	x: 0.158 m η = 0.9	x: 0 m η = 0.9	x: 0 m η = 8.3	x: 0 m η = 17.2	x: 0 m η = 0.7	x: 0 m η = 3.0	x: 0 m η = 27.2	x: 0 m η = 20.8	x: 0 m η = 22.5	CUMPLE η = 27.2
N443/N444	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.315 m η = 6.6	x: 0.315 m η = 7.6	x: 0.315 m η = 0.5	x: 0 m η = 1.1	x: 0 m η = 7.0	x: 0 m η = 0.9	x: 0 m η = 0.2	x: 0 m η = 1.3	x: 0 m η = 7.2	x: 0 m η < 0.1	x: 0 m η = 0.5	x: 0 m η = 10.2	x: 0.63 m η = 9.8	x: 0.63 m η = 9.5	CUMPLE η = 10.2
N444/N445	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 3.7	η = 4.4	x: 0.158 m η = 0.4	x: 0 m η = 0.9	x: 0.63 m η = 6.3	η = 0.3	x: 0 m η = 0.2	x: 0 m η = 1.1	x: 0.63 m η = 6.4	x: 0 m η < 0.1	x: 0.63 m η = 0.4	N.P.[1]	x: 0.63 m η = 8.0	x: 0.63 m η = 8.6	CUMPLE η = 8.6
N445/N446	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.158 m η = 0.9	x: 0.158 m η = 1.3	x: 0.158 m η = 0.5	x: 0.473 m η = 1.1	x: 0.63 m η = 8.0	η = 0.2	x: 0 m η = 0.2	x: 0.473 m η = 1.1	x: 0.63 m η = 8.1	x: 0.473 m η < 0.1	x: 0.63 m η = 0.7	x: 0.63 m η = 10.1	x: 0.63 m η = 10.0	x: 0.63 m η = 10.9	CUMPLE η = 10.9
N446/N447	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.473 m η = 1.8	x: 0.473 m η = 2.4	x: 0.158 m η = 0.5	x: 0.473 m η = 1.3	x: 0.63 m η = 9.3	η = 0.2	x: 0.63 m η = 0.2	x: 0.473 m η = 1.4	x: 0.63 m η = 9.4	x: 0.473 m η < 0.1	x: 0.63 m η = 0.9	x: 0.63 m η = 12.3	x: 0.63 m η = 11.7	x: 0.63 m η = 12.6	CUMPLE η = 12.6
N447/N448	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.473 m η = 4.6	x: 0.473 m η = 5.5	x: 0.158 m η = 0.6	x: 0 m η = 1.2	x: 0 m η = 8.3	η = 0.3	x: 0.63 m η = 0.2	x: 0 m η = 1.4	x: 0 m η = 8.5	x: 0 m η < 0.1	x: 0 m η = 0.7	x: 0 m η = 12.3	x: 0 m η = 10.6	x: 0 m η = 11.2	CUMPLE η = 12.3
N448/N449	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.315 m η = 7.4	x: 0.315 m η = 8.6	x: 0.315 m η = 0.6	x: 0.63 m η = 1.9	x: 0 m η = 4.6	x: 0.315 m η = 0.3	x: 0.63 m η = 0.3	x: 0.63 m η = 2.2	x: 0 m η = 4.7	x: 0.63 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 0.63 m η = 11.8	x: 0.63 m η = 11.0	CUMPLE η = 11.8
N449/N450	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.158 m η = 10.5	x: 0.158 m η = 11.8	x: 0 m η = 0.3	x: 0.63 m η = 1.9	x: 0.63 m η = 10.3	x: 0 m η = 1.0	x: 0 m η = 0.2	x: 0.63 m η = 2.1	x: 0.63 m η = 10.4	x: 0.63 m η < 0.1	x: 0.63 m η = 1.1	x: 0.63 m η = 13.9	x: 0.63 m η = 14.5	x: 0.63 m η = 14.0	CUMPLE η = 14.5
N450/N272	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 12.4	x: 0 m η = 13.0	η = 1.8	x: 0.49 m η = 10.0	x: 0.49 m η = 16.4	x: 0.245 m η = 1.0	x: 0.49 m η = 1.1	x: 0.49 m η = 10.8	x: 0.49 m η = 16.7	x: 0.49 m η = 1.2	x: 0.49 m η = 2.8	x: 0.49 m η = 35.3	x: 0.49 m η = 24.9	x: 0.49 m η = 27.4	CUMPLE η = 35.3
N332/N458	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 11.7	η = 13.6	η = 2.3	x: 0 m η = 38.9	x: 0 m η = 15.2	x: 0.245 m η = 1.4	x: 0.49 m η = 5.5	x: 0 m η = 39.5	x: 0 m η = 15.8	x: 0 m η = 15.9	x: 0 m η = 2.5	x: 0 m η = 80.7	x: 0 m η = 65.5	x: 0 m η = 63.8	CUMPLE η = 80.7
N458/N457	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.158 m η = 10.1	x: 0.158 m η = 11.7	η = 0.6	x: 0 m η = 5.3	x: 0 m η = 9.4	x: 0.473 m η = 0.7	x: 0 m η = 0.6	x: 0 m η = 5.4	x: 0 m η = 9.7	x: 0 m η = 0.3	x: 0 m η = 0.9	x: 0 m η = 20.5	x: 0 m η = 17.3	x: 0 m η = 17.6	CUMPLE η = 20.5
N457/N456	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.315 m η = 7.5	x: 0.315 m η = 8.3	x: 0.315 m η = 0.5	x: 0 m η = 1.8	x: 0.63 m η = 6.5	x: 0 m η = 0.6	x: 0 m η = 0.3	x: 0 m η = 2.0	x: 0.63 m η = 6.6	x: 0 m η < 0.1	x: 0.63 m η = 0.4	x: 0.63 m η = 10.5	x: 0 m η = 12.1	x: 0 m η = 11.3	CUMPLE η = 12.1
N456/N455	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.473 m η = 4.9	x: 0.473 m η = 4.9	x: 0.158 m η = 0.5	x: 0.473 m η = 1.0	x: 0 m η = 6.7	x: 0.473 m η = 0.1	x: 0 m η = 0.1	x: 0.315 m η = 1.1	x: 0 m η = 6.8	x: 0.315 m η < 0.1	x: 0 m η = 0.5	x: 0 m η = 10.6	x: 0 m η = 7.9	x: 0 m η = 9.2	CUMPLE η = 10.6
N455/N454	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.473 m η = 2.2	x: 0.473 m η = 1.6	x: 0.158 m η = 0.5	x: 0.158 m η = 1.1	x: 0 m η = 7.6	x: 0.473 m η = 0.1	x: 0 m η = 0.2	x: 0.158 m η = 1.2	x: 0 m η = 7.6	x: 0.158 m η < 0.1	x: 0 m η = 0.6	x: 0 m η = 11.7	x: 0 m η = 7.2	x: 0 m η = 10.1	CUMPLE η = 11.7
N454/N453	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.158 m η = 1.6	x: 0.158 m η = 0.9	x: 0.158 m η = 0.6	x: 0.158 m η = 1.2	x: 0 m η = 8.1	x: 0.473 m η = 0.1	x: 0.63 m η = 0.1	x: 0.158 m η = 1.3	x: 0 m η = 8.3	x: 0.158 m η < 0.1	x: 0 m η = 0.7	x: 0 m η = 12.5	x: 0.63 m η = 3.8	x: 0 m η = 10.7	CUMPLE η = 12.5
N453/N452	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.158 m η = 4.3	x: 0.158 m η = 4.2	x: 0.315 m η = 0.6	x: 0.63 m η = 1.2	x: 0 m η = 8.4	x: 0.473 m η = 0.6	x: 0.63 m η = 0.2	x: 0.63 m η = 1.5	x: 0 m η = 8.4	x: 0.63 m η < 0.1	x: 0 m η = 0.7	x: 0 m η = 12.2	x: 0.63 m η = 7.6	x: 0 m η = 10.8	CUMPLE η = 12.2
N452/N451	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 6.8	x: 0 m η = 7.5	x: 0.63 m η = 0.4	x: 0.63 m η = 3.3	x: 0.63 m η = 6.4	x: 0.315 m η = 0.6	x: 0.63 m η = 0.4	x: 0.63 m η = 3.4	x: 0.63 m η = 6.5	x: 0.63 m η = 0.1	x: 0.63 m η = 0.4	x: 0.63 m η = 10.7	x: 0.63 m η = 12.7	x: 0.63 m η = 12.3	CUMPLE η = 12.7
N451/N271	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 9.5	η = 11.2	η = 1.4	x: 0.63 m η = 30.0	x: 0.63 m η = 15.4	x: 0.158 m η = 0.8	x: 0.63 m η = 3.3	x: 0.63 m η = 30.6	x: 0.63 m η = 15.7	x: 0.63 m η = 9.5	x: 0.63 m η = 2.5	x: 0.63 m η = 61.1	x: 0.63 m η = 51.2	x: 0.63 m η = 49.8	CUMPLE η = 61.1
N458/N333	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 2.5	x: 0 m η = 2.3	x: 0.929 m η = 4.2	x: 0.929 m η = 3.5	x: 0.929 m η = 5.1	x: 0.465 m η = 0.4	x: 0.929 m η = 0.2	x: 0.929 m η = 4.2	x: 0.929 m η = 6.9	x: 0.929 m η = 0.2	x: 0.929 m η = 0.5	N.P.[1]	x: 0.929 m η = 8.5	x: 0.929 m η = 9.5	CUMPLE η = 9.5
N458/N443	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.602 m η = 3.2	x: 0 m η = 4.8	x: 0.401 m η = 2.2	x: 0 m η = 5.0	x: 0 m η = 3.3	x: 0.602 m η = 0.3	x: 0 m η = 0.5	x: 0 m η = 5.2	x: 0 m η = 3.5	x: 0 m η = 0.3	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 12.5	x: 0 m η = 11.6	CUMPLE η = 12.5
N457/N443	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 4.5	x: 0 m η = 5.4	x: 0.697 m η = 1.0	x: 0 m η = 0.3	x: 0 m η = 0.9	x: 0.929 m η = 0.1	x: 0 m η = 0.1	x: 0 m η = 0.7	x: 0 m η = 1.2	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 7.1	x: 0 m η = 6.5	CUMPLE η = 7.1
N457/N444	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 3.3	x: 0 m η = 4.6	η = 0.2	x: 0.802 m η = 0.8	x: 0 m η = 0.9	η = 0.1	x: 0.802 m η = 0.1	x: 0.802 m η = 0.9	x: 0 m η = 1.0	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0.802 m η = 5.8	x: 0.802 m η = 5.7	CUMPLE η = 5.8
N456/N444	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 4.2	x: 0 m η = 5.1	x: 0 m η = 1.4	x: 0 m η = 0.6	x: 0 m η = 0.8	η < 0.1	x: 0 m η = 0.1	x: 0 m η = 0.9	x: 0 m η = 1.3	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 6.8	x: 0 m η = 6.2	CUMPLE η = 6.8
N456/N445	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 3.4	x: 0 m η = 4.6	x: 0.201 m η = 1.3	x: 0.802 m η = 1.0	x: 0 m η = 0.8	x: 0.401 m η = 0.1	x: 0.802 m η = 0.1	x: 0.802 m η = 1.1	x: 0 m η = 1.0	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 6.1	x: 0.802 m η = 5.9	CUMPLE η = 6.1
N455/N445	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 4.1	x: 0 m η = 5.3	η = 2.3	x: 0.929 m η = 0.5	x: 0 m η = 1.5	x: 0.929 m η < 0.1	x: 0 m η = 0.1	x: 0.465 m η = 1.4	x: 0 m η = 2.5	x: 0.465 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 6.5	x: 0 m η = 6.2	CUMPLE η = 6.5
N455/N446	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 3.4	x: 0 m η = 4.4	x: 0.401 m η = 1.4	x: 0.802 m η = 1.0	x: 0 m η = 0.8	x: 0.602 m η = 0.1	x: 0.802 m η = 0.1	x: 0.802 m η = 1.2	x: 0 m η = 1.0	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 6.0	x: 0.802 m η = 5.7	CUMPLE η = 6.0
N454/N446	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 4.0	x: 0 m η = 5.4	x: 0.697 m η = 2.7	x: 0.929 m η = 0.6	x: 0.929 m η = 1.6	x: 0.232 m η < 0.1	x: 0 m η = 0.1	x: 0.465 m η = 1.6	x: 0.929 m η = 2.8	x: 0.465 m η < 0.1	x: 0.929 m η = 0.1	N.P.[1]	x: 0 m η = 6.4	x: 0 m η = 6.1	CUMPLE η = 6.4
N454/N447	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 3.5	x: 0 m η = 4.3	x: 0.602 m η = 1.8	x: 0.802 m η = 1.0	x: 0 m η = 0.8	x: 0.802 m η = 0.1	x: 0 m η = 0.1	x: 0.802 m η = 1.2	x: 0.802 m η = 1.1	x: 0.802 m η < 0.1	x: 0.802 m η < 0.1	N.P.[1]	x: 0 m η = 6.0	x: 0 m η = 5.6	CUMPLE η = 6.0
N453/N447	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 3.9	x: 0 m η = 5.5	x: 0.232 m η = 2.6	x: 0.929 m η = 0.6	x: 0 m η = 1.4	x: 0 m η < 0.1	x: 0.929 m η = 0.1	x: 0.465 m η = 1.5	x: 0 m η = 2.5	x: 0.465 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 6.4	x: 0.929 m η = 6.3	CUMPLE η = 6.4
N453/N448	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 3.6	x: 0 m η = 4.2	x: 0.401 m η = 1.3	x: 0.802 m η = 1.1	x: 0 m η = 1.1	x: 0.602 m η = 0.1	x: 0 m η = 0.1	x: 0.802 m η = 1.4	x: 0 m η = 1.4	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 6.3	x: 0.802 m η = 5.6	CUMPLE η = 6.3

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N452/N448	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 3.8	x: 0 m η = 5.6	x: 0 m η = 1.3	x: 0.929 m η = 0.7	x: 0.929 m η = 1.0	η < 0.1	x: 0.929 m η = 0.1	x: 0.465 m η = 0.8	x: 0.929 m η = 1.5	x: 0.465 m η < 0.1	x: 0.929 m η < 0.1	N.P.(1)	x: 0.929 m η = 6.5	x: 0.929 m η = 6.4	CUMPLE η = 6.5
N452/N449	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 3.8	x: 0 m η = 4.3	x: 0 m η = 0.6	x: 0.802 m η = 0.3	x: 0 m η = 0.6	x: 0 m η < 0.1	x: 0 m η < 0.1	x: 0.802 m η = 0.5	x: 0 m η = 0.9	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0.201 m η = 5.4	x: 0 m η = 4.9	CUMPLE η = 5.4
N451/N449	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 4.0	x: 0 m η = 6.2	η = 1.2	x: 0 m η = 2.9	x: 0 m η = 1.1	η = 0.1	x: 0.929 m η = 0.3	x: 0 m η = 3.1	x: 0 m η = 1.7	x: 0 m η = 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 9.3	x: 0 m η = 9.7	CUMPLE η = 9.7
N451/N450	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 3.0	x: 0 m η = 3.1	x: 0.401 m η = 1.4	x: 0.802 m η = 4.0	x: 0 m η = 4.6	x: 0.602 m η = 0.5	x: 0 m η = 0.5	x: 0.802 m η = 4.1	x: 0 m η = 4.7	x: 0.802 m η = 0.2	x: 0 m η = 0.2	N.P.(1)	x: 0 m η = 11.2	x: 0 m η = 10.5	CUMPLE η = 11.2
N271/N450	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.697 m η = 2.3	x: 0 m η = 3.8	x: 0.465 m η = 4.9	x: 0 m η = 18.6	x: 0 m η = 10.6	x: 0.929 m η = 0.7	x: 0.929 m η = 1.5	x: 0 m η = 19.4	x: 0 m η = 10.9	x: 0 m η = 3.8	x: 0 m η = 1.2	x: 0 m η = 39.2	x: 0 m η = 33.2	x: 0 m η = 30.1	CUMPLE η = 39.2
N459/N460	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.41 m η = 24.7	x: 1.41 m η = 39.1	x: 0.353 m η = 1.9	x: 0 m η = 1.9	x: 1.41 m η = 18.4	η = 1.7	x: 0 m η = 0.2	x: 0 m η = 2.8	x: 1.41 m η = 19.3	x: 0 m η = 0.1	x: 1.41 m η = 3.7	x: 1.41 m η = 50.7	x: 1.41 m η = 61.5	x: 1.41 m η = 62.1	CUMPLE η = 62.1
N460/N461	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 13.6	x: 0 m η = 13.4	x: 0 m η = 0.6	x: 1.4 m η = 1.5	x: 0 m η = 37.9	x: 1.4 m η = 4.7	x: 0 m η = 0.1	x: 0 m η = 1.1	x: 0 m η = 38.2	x: 1.4 m η < 0.1	x: 0 m η = 14.8	x: 0 m η = 62.5	x: 0 m η = 51.9	x: 0 m η = 60.9	CUMPLE η = 62.5
N461/N462	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.35 m η = 13.4	x: 0 m η = 1.6	x: 0.9 m η = 1.1	x: 1.35 m η = 4.3	x: 1.35 m η = 53.7	η = 6.2	x: 0 m η = 0.3	x: 1.35 m η = 4.4	x: 1.35 m η = 54.2	x: 1.35 m η = 0.2	x: 1.35 m η = 29.7	x: 1.35 m η = 79.3	x: 1.35 m η = 55.0	x: 1.35 m η = 75.0	CUMPLE η = 79.3
N462/N463	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.79 m η = 16.5	x: 0 m η = 3.2	x: 0.395 m η = 7.1	x: 0 m η = 10.7	x: 0 m η = 51.2	x: 0.592 m η = 10.3	x: 0.79 m η = 2.2	x: 0 m η = 10.8	x: 0 m η = 54.3	x: 0 m η = 1.2	x: 0 m η = 30.5	x: 0 m η = 87.8	x: 0 m η = 60.7	x: 0 m η = 74.5	CUMPLE η = 87.8
N462/N464	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.894 m η = 2.5	x: 0.894 m η = 4.6	x: 0.894 m η = 2.2	x: 1.073 m η = 9.6	x: 1.073 m η = 14.6	x: 0.894 m η = 2.0	x: 1.073 m η = 1.4	x: 1.073 m η = 9.7	x: 1.073 m η = 15.6	x: 1.073 m η = 1.0	x: 1.073 m η = 2.5	x: 1.073 m η = 26.0	x: 1.073 m η = 24.8	x: 1.073 m η = 23.3	CUMPLE η = 26.0
N459/N467	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.755 m η = 14.7	x: 0 m η = 46.8	x: 0.378 m η = 5.0	x: 0.755 m η = 11.0	x: 0 m η = 20.2	x: 0.378 m η = 1.9	x: 0.755 m η = 1.2	x: 0.755 m η = 13.1	x: 0 m η = 22.4	x: 0.755 m η = 1.7	x: 0 m η = 5.0	N.P.(1)	x: 0 m η = 53.5	x: 0.755 m η = 49.9	CUMPLE η = 53.5
N467/N460	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.847 m η = 23.1	x: 0 m η = 12.4	η = 0.8	x: 0 m η = 8.4	x: 0 m η = 56.4	x: 0.424 m η = 6.5	x: 0 m η = 0.7	x: 0 m η = 8.4	x: 0 m η = 56.8	x: 0 m η = 0.7	x: 0 m η = 32.6	x: 0 m η = 85.5	x: 0 m η = 18.0	x: 0 m η = 80.0	CUMPLE η = 85.5
N460/N466	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.217 m η = 6.4	x: 0 m η = 19.9	x: 0.652 m η = 1.6	x: 0 m η = 3.8	x: 0 m η = 9.0	η = 0.7	x: 0 m η = 0.4	x: 0 m η = 4.2	x: 0 m η = 9.7	x: 0 m η = 0.2	x: 0 m η = 0.9	x: 0 m η = 15.3	x: 0 m η = 26.5	x: 0 m η = 24.7	CUMPLE η = 26.5
N466/N461	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.983 m η = 12.5	x: 0 m η = 7.4	η = 0.4	x: 0 m η = 2.2	x: 0 m η = 28.1	x: 0.492 m η = 2.8	x: 0.983 m η = 0.2	x: 0 m η = 2.3	x: 0 m η = 28.3	x: 0 m η = 0.1	x: 0 m η = 8.1	x: 0 m η = 44.7	x: 0 m η = 31.7	x: 0 m η = 43.7	CUMPLE η = 44.7
N461/N465	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.685 m η = 4.3	x: 0.685 m η = 13.8	x: 0.514 m η = 0.8	x: 0 m η = 3.1	x: 1.028 m η = 1.2	η < 0.1	x: 0 m η = 0.3	x: 0 m η = 2.2	x: 1.028 m η = 1.6	x: 0 m η = 0.1	x: 1.028 m η < 0.1	N.P.(1)	x: 0 m η = 16.4	x: 0 m η = 17.1	CUMPLE η = 17.1
N465/N462	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.557 m η = 8.6	x: 0.557 m η = 6.8	x: 0.928 m η = 4.9	x: 0.928 m η = 1.5	x: 1.114 m η = 28.9	x: 0.557 m η = 2.2	x: 0 m η = 0.1	x: 0 m η = 3.0	x: 1.114 m η = 31.0	x: 0 m η = 0.1	x: 1.114 m η = 9.7	x: 1.114 m η = 49.8	x: 1.114 m η = 40.0	x: 1.114 m η = 44.5	CUMPLE η = 49.8
N464/N463	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.914 m η = 5.6	x: 0 m η = 57.5	η = 3.9	x: 0 m η = 3.9	x: 0 m η = 9.5	η = 0.5	x: 0 m η = 0.4	x: 0 m η = 3.2	x: 0 m η = 11.2	x: 0 m η = 0.1	x: 0 m η = 1.3	N.P.(1)	x: 0 m η = 62.9	x: 0 m η = 62.3	CUMPLE η = 62.9
N472/N468	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.234 m η = 24.2	x: 1.234 m η = 38.0	x: 0.353 m η = 2.0	x: 0 m η = 1.8	x: 1.41 m η = 16.5	x: 0.353 m η = 1.5	x: 0 m η = 0.2	x: 0 m η = 2.7	x: 1.41 m η = 17.4	x: 0 m η = 0.1	x: 1.41 m η = 3.1	x: 1.41 m η = 46.9	x: 1.41 m η = 57.3	x: 1.41 m η = 57.5	CUMPLE η = 57.5
N468/N469	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.467 m η = 13.9	x: 0.467 m η = 13.7	x: 1.4 m η = 0.4	x: 1.167 m η = 1.5	x: 0 m η = 38.3	x: 1.4 m η = 4.7	x: 0 m η = 0.1	x: 0 m η = 1.2	x: 0 m η = 38.5	x: 1.167 m η < 0.1	x: 0 m η = 15.0	x: 0 m η = 62.7	x: 0 m η = 52.5	x: 0 m η = 61.6	CUMPLE η = 62.7
N469/N470	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.35 m η = 13.2	x: 0 m η = 2.8	x: 0.225 m η = 0.7	x: 1.35 m η = 4.3	x: 1.35 m η = 53.9	x: 0.225 m η = 6.3	x: 0 m η = 0.3	x: 1.35 m η = 4.3	x: 1.35 m η = 54.2	x: 1.35 m η = 0.2	x: 1.35 m η = 29.8	x: 1.35 m η = 79.3	x: 1.35 m η = 55.1	x: 1.35 m η = 75.2	CUMPLE η = 79.3
N470/N471	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.79 m η = 16.2	x: 0 m η = 4.6	η = 6.9	x: 0 m η = 10.0	x: 0 m η = 50.7	η = 9.9	x: 0.79 m η = 1.9	x: 0 m η = 10.0	x: 0 m η = 53.7	x: 0 m η = 1.0	x: 0 m η = 29.8	x: 0 m η = 87.5	x: 0 m η = 60.1	x: 0 m η = 74.1	CUMPLE η = 87.5
N472/N476	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.755 m η = 19.2	x: 0 m η = 49.8	η = 5.0	x: 0.755 m η = 10.2	x: 0 m η = 21.1	x: 0.378 m η = 2.0	x: 0.755 m η = 1.1	x: 0.755 m η = 12.4	x: 0 m η = 23.2	x: 0.755 m η = 1.5	x: 0 m η = 5.4	N.P.(1)	x: 0.755 m η = 57.2	x: 0.755 m η = 55.8	CUMPLE η = 57.2
N476/N468	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.847 m η = 25.2	x: 0 m η = 16.1	η = 0.9	x: 0 m η = 9.5	x: 0 m η = 57.1	x: 0.424 m η = 6.6	x: 0 m η = 0.8	x: 0 m η = 9.5	x: 0 m η = 57.5	x: 0 m η = 0.9	x: 0 m η = 33.5	x: 0 m η = 86.1	x: 0 m η = 23.1	x: 0 m η = 79.8	CUMPLE η = 86.1
N468/N475	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.217 m η = 8.3	x: 0.217 m η = 21.9	x: 0.652 m η = 1.7	x: 0 m η = 3.7	x: 0 m η = 7.2	η = 0.5	x: 0 m η = 0.4	x: 0 m η = 4.4	x: 0 m η = 8.0	x: 0 m η = 0.2	x: 0 m η = 0.6	x: 0 m η = 12.6	x: 0.869 m η = 25.9	x: 0.869 m η = 26.4	CUMPLE η = 26.4
N475/N469	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.983 m η = 13.8	x: 0 m η = 9.6	x: 0.246 m η = 0.4	x: 0 m η = 2.6	x: 0 m η = 29.5	x: 0.246 m η = 3.0	x: 0.983 m η = 0.2	x: 0 m η = 2.6	x: 0 m η = 29.7	x: 0 m η = 0.1	x: 0 m η = 8.9	x: 0 m η = 46.6	x: 0 m η = 33.6	x: 0 m η = 45.6	CUMPLE η = 46.6
N469/N474	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.685 m η = 5.5	x: 0.685 m η = 15.1	x: 0.514 m η = 0.7	x: 0 m η = 2.9	x: 1.028 m η = 1.8	x: 0.343 m η = 0.1	x: 0 m η = 0.3	x: 0 m η = 2.4	x: 1.028 m η = 2.0	x: 0 m η = 0.1	x: 1.028 m η < 0.1	N.P.(1)	x: 0 m η = 17.6	x: 0 m η = 17.9	CUMPLE η = 17.9
N474/N470	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.557 m η = 8.8	x: 0.557 m η = 7.5	x: 1.114 m η = 4.9	x: 1.114 m η = 1.6	x: 1.114 m η = 29.3	x: 1.114 m η = 2.3	x: 0 m η = 0.1	x: 0.371 m η = 2.9	x: 1.114 m η = 31.4	x: 0.371 m η = 0.1	x: 1.114 m η = 9.9	x: 1.114 m η = 50.7	x: 1.114 m η = 40.8	x: 1.114 m η = 45.2	CUMPLE η = 50.7
N470/N473	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.894 m η = 2.7	x: 0.894 m η = 4.8	x: 0.894 m η = 2.7	x: 1.073 m η = 8.3	x: 1.073 m η = 14.6	x: 0.358 m η = 2.0	x: 1.073 m η = 1.2	x: 1.073 m η = 8.3	x: 1.073 m η = 15.7	x: 1.073 m η = 0.7	x: 1.073 m η = 2.5	x: 1.073 m η = 25.9	x: 1.073 m η = 25.0	x: 1.073 m η = 23.3	CUMPLE η = 25.9
N473/N471	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.365 m η = 8.9	x: 0 m η = 59.6	η = 4.3	x: 0 m η = 3.5	x: 0 m η = 10.3	x: 1.096 m η = 0.6	x: 0 m η = 0.4	x: 0 m η = 3.2	x: 0 m η = 12.1	x: 0 m η = 0.1	x: 0 m η = 1.5	N.P.(1)	x: 0 m η = 64.7	x: 0 m η = 64.0	CUMPLE η = 64.7
N464/N477	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.617 m η = 2.9	x: 0 m η = 26.3	η = 4.4	x: 0 m η = 17.4	x: 0 m η = 6.2	x: 0.309 m η = 0.9	x: 0 m η = 3.3	x: 0 m η = 17.4	x: 0 m η = 8.1	x: 0 m η = 3.1	x: 0 m η = 0.7	x: 0 m η = 3.6	x: 0 m η = 44.0	x: 0 m η = 48.0	CUMPLE η = 48.0
N477/N478	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.081 m η = 5.1	x: 0 m η = 17.7	x: 0.18 m η = 2.0	x: 0 m η = 1.6	x: 0 m η = 4.2	x: 0.18 m η = 0.6	x: 1.081 m η = 0.3	x: 0 m η = 1.6	x: 0 m η = 5.0	x: 0 m η < 0.1	x: 0 m η = 0.3	N.P.(1)	x: 0 m η = 19.4	x: 0 m η = 19.7	CUMPLE η = 19.7
N478/N479	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.088 m η = 7.0	x: 0 m η = 12.5	x: 0.544 m η = 1.8	x: 0 m η = 1.9	x: 1.088 m η = 2.7	η = 0.4	x: 0 m η = 0.3	x: 0 m η = 1.9	x: 1.088 m η = 3.5	x: 0 m η < 0.1	x: 1.088 m η = 0.1	N.P.(1)	x: 0 m η = 14.3	x: 0 m η = 14.7	CUMPLE η = 14.7
N479/N480	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.08 m η = 7.9	x: 0 m η = 8.7	x: 0.9 m η = 0.5	x: 1.08 m η = 1.0	x: 0 m η = 1.4	x: 0.9 m η = 0.2	x: 0 m η = 0.2	x: 1.08 m η = 1.0	x: 0 m η = 1.7	x: 1.08 m η < 0.1	x: 0 m η < 0.1	x: 0 m η = 3.6	x: 0 m η = 9.7	x: 0 m η = 9.8	CUMPLE η = 9.8
N480/N481	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.085 m η = 8.9	x: 1.085 m η = 6.2	x: 0.904 m η = 0.2	x: 1.085 m η = 1.6	x: 1.085 m η = 2.8	η = 0.5	x: 0 m η = 0.2	x: 1.085 m η = 1.6	x: 1.085 m η = 2.9	x: 1.085 m η < 0.1	x: 1.085 m η = 0.1	x: 1.085 m η = 8.9	x: 0 m η = 6.9	x: 0.904 m η = 10.1	CUMPLE η = 10.1
N481/N482	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.082 m η = 10.6	x: 1.082 m η = 3.9	x: 0 m η = 0.1	x: 1.082 m η = 1.7	x: 1.082 m η = 4.2	η = 0.4	x: 0 m η = 0.1	x: 1.082 m η = 1.7	x: 1.082 m η = 4.2	x: 1.082 m η < 0.1	x: 1.082 m η = 0.2	x: 1.082 m η = 13.1	x: 1.082 m η = 5.2	x: 1.082 m η = 12.7	CUMPLE η = 13.1
N482/N483	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.085 m η = 13.1	x: 1.085 m η = 1.7	η = 0.4	x: 0.904 m η = 1.7	x: 0 m η = 4.7	x: 0 m η = 0.6	x: 0 m η = 0.1	x: 0.362 m η = 1.0	x: 0 m η = 4.8	x: 0.904 m η < 0.1	x: 0 m η = 0.2	x: 1.085 m η = 15.5	x: 0 m η = 5.2	x: 0.904 m η = 15.3	CUMPLE η = 15.5
N483/N484	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.081 m η = 15.0	N.P.(2)	η = 0.7	x: 0.901 m η = 2.0	x: 1.081 m η = 3.1	x: 0 m η = 0.4	x: 0 m η = 0.1	x: 0.54 m η = 1.2	x: 1.081 m η = 3.2	x: 0.901 m η < 0.1	x: 1.081 m η = 0.1	x: 1.081 m η = 17.7	N.P.(3)	x: 0.901 m η = 17.4	CUMPLE η = 17.7
N485/N484	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.08 m η = 15.6	N.P.(2)	x: 1.08 m η = 1.2	x: 0.54 m η = 2.0	x: 1.08 m η = 1.2	η = 0.1	x: 0 m η = 0.1	x: 0.36 m η = 1.4	x: 1.08 m η = 1.7	x: 0.54 m η < 0.1	x: 1.08 m η < 0.1	x: 0.72 m η = 18.2	N.P.(3)	x: 0.54 m η = 18.1	CUMPLE η = 18.2

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))														Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N486/N485	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.084 m η = 14.6	N.P.[2]	x: 0.903 m η = 1.4	x: 0.722 m η = 1.9	x: 1.084 m η = 1.1	x: 0.361 m η = 0.2	x: 0 m η = 0.1	x: 0.542 m η = 1.5	x: 1.084 m η = 1.4	x: 0.722 m η < 0.1	x: 1.084 m η < 0.1	x: 0.903 m η = 17.2	N.P.[3]	x: 0.722 m η = 17.0	CUMPLE η = 17.2
N487/N486	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.08 m η = 12.4	N.P.[2]	x: 0 m η = 0.5	x: 1.08 m η = 1.9	x: 1.08 m η = 2.2	x: 0 m η = 0.3	x: 0 m η = 0.1	x: 1.08 m η = 1.9	x: 1.08 m η = 2.5	x: 0.9 m η < 0.1	x: 1.08 m η = 0.1	x: 1.08 m η = 14.8	N.P.[3]	x: 1.08 m η = 14.7	CUMPLE η = 14.8
N488/N487	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.083 m η = 8.5	x: 0 m η = 3.3	η = 0.5	x: 1.083 m η = 1.8	x: 0 m η = 2.6	η = 0.5	x: 0 m η = 0.2	x: 1.083 m η = 1.9	x: 0 m η = 2.6	x: 1.083 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 11.2	x: 0 m η = 5.8	x: 1.083 m η = 10.8	CUMPLE η = 11.2
N489/N488	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.087 m η = 8.1	x: 1.087 m η = 7.5	x: 1.087 m η = 0.5	x: 1.087 m η = 1.3	x: 0 m η = 2.6	x: 1.087 m η = 0.3	x: 0 m η = 0.2	x: 1.087 m η = 1.4	x: 0 m η = 2.8	x: 1.087 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 11.5	x: 0 m η = 10.3	x: 0 m η = 10.4	CUMPLE η = 11.5
N490/N489	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.181 m η = 8.0	x: 0.181 m η = 11.9	x: 0.904 m η = 1.2	x: 0 m η = 1.8	x: 0 m η = 1.0	η = 0.1	x: 0 m η = 0.3	x: 0 m η = 2.1	x: 0 m η = 1.5	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 14.8	x: 0 m η = 14.3	CUMPLE η = 14.8
N491/N490	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.539 m η = 7.0	x: 0.539 m η = 16.2	x: 0.18 m η = 1.2	x: 1.077 m η = 1.3	x: 0 m η = 2.6	x: 0.18 m η = 0.4	x: 1.077 m η = 0.2	x: 1.077 m η = 1.8	x: 0 m η = 3.1	x: 1.077 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 5.3	x: 1.077 m η = 18.6	x: 1.077 m η = 17.8	CUMPLE η = 18.6
N473/N491	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.801 m η = 5.2	x: 0 m η = 23.4	η = 3.1	x: 0 m η = 14.5	x: 0 m η = 5.7	η = 0.7	x: 0 m η = 2.1	x: 0 m η = 14.6	x: 0 m η = 7.0	x: 0 m η = 2.2	x: 0 m η = 0.5	x: 0 m η = 12.2	x: 0 m η = 38.3	x: 0 m η = 41.5	CUMPLE η = 41.5
N493/N492	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.128 m η = 4.2	x: 0 m η = 16.7	η = 0.6	x: 1.128 m η = 2.3	x: 0 m η = 12.0	η = 1.7	x: 0 m η = 0.3	x: 1.128 m η = 2.3	x: 0 m η = 12.3	x: 1.128 m η = 0.1	x: 0 m η = 1.5	x: 0 m η = 8.8	x: 0 m η = 19.6	x: 0 m η = 21.7	CUMPLE η = 21.7
N494/N493	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.375 m η = 7.9	x: 0.375 m η = 13.6	η = 0.2	x: 1.126 m η = 1.8	x: 1.126 m η = 9.4	x: 0.375 m η = 1.3	x: 0 m η = 0.3	x: 1.126 m η = 1.9	x: 1.126 m η = 9.4	x: 1.126 m η < 0.1	x: 1.126 m η = 0.9	x: 0 m η = 12.6	x: 0 m η = 16.5	x: 0 m η = 16.5	CUMPLE η = 16.5
N495/N494	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.126 m η = 11.1	x: 0 m η = 11.1	x: 0.188 m η = 1.0	x: 0 m η = 1.2	x: 0 m η = 2.5	x: 0.188 m η = 0.3	x: 0 m η = 0.3	x: 1.126 m η = 1.6	x: 0 m η = 2.8	x: 1.126 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 15.8	x: 1.126 m η = 14.8	x: 0 m η = 13.7	CUMPLE η = 15.8
N496/N495	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.12 m η = 14.9	x: 0 m η = 8.4	η = 0.9	x: 0 m η = 8.0	x: 1.12 m η = 4.3	η = 0.5	x: 0 m η = 1.0	x: 0 m η = 8.1	x: 1.12 m η = 4.4	x: 0 m η = 0.7	x: 1.12 m η = 0.2	x: 0 m η = 23.9	x: 1.12 m η = 11.3	x: 0 m η = 23.2	CUMPLE η = 23.9
N471/N496	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.187 m η = 21.8	x: 0.594 m η = 6.1	x: 0.791 m η = 3.7	x: 1.187 m η = 6.9	x: 0 m η = 14.7	x: 0.791 m η = 1.9	x: 1.187 m η = 1.0	x: 1.187 m η = 6.9	x: 0 m η = 16.3	x: 1.187 m η = 0.5	x: 0 m η = 2.7	x: 0 m η = 32.2	x: 0 m η = 10.7	x: 1.187 m η = 30.4	CUMPLE η = 32.2
N487/N492	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.934 m η = 9.2	x: 0.701 m η = 2.1	η = 0.2	x: 0 m η = 1.2	x: 0.934 m η = 7.6	x: 0.467 m η = 0.6	x: 0 m η = 0.2	x: 0 m η = 1.3	x: 0.934 m η = 7.7	x: 0 m η < 0.1	x: 0.934 m η = 0.6	x: 0.934 m η = 15.6	x: 0.934 m η = 3.7	x: 0.934 m η = 14.5	CUMPLE η = 15.6
N488/N492	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.168 m η = 1.9	x: 0 m η = 16.9	x: 0.503 m η = 1.4	x: 0 m η = 1.9	x: 1.006 m η = 5.1	x: 0.503 m η = 0.4	x: 1.006 m η = 0.2	x: 0 m η = 1.5	x: 1.006 m η = 5.7	x: 0 m η < 0.1	x: 1.006 m η = 0.3	N.P.[1]	x: 0 m η = 18.9	x: 0 m η = 19.2	CUMPLE η = 19.2
N488/N493	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.94 m η = 12.1	x: 0.705 m η = 0.3	x: 0.94 m η = 1.0	x: 0.94 m η = 1.5	x: 0 m η = 5.2	x: 0.94 m η = 0.5	x: 0 m η = 0.2	x: 0 m η = 1.6	x: 0 m η = 5.6	x: 0 m η < 0.1	x: 0 m η = 0.3	N.P.[1]	x: 0 m η = 3.3	x: 0.94 m η = 14.2	CUMPLE η = 14.2
N489/N493	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.014 m η = 0.8	x: 0 m η = 21.5	x: 0.845 m η = 0.9	x: 0 m η = 2.1	x: 0 m η = 4.0	η = 0.3	x: 1.014 m η = 0.2	x: 0 m η = 1.3	x: 0 m η = 4.3	x: 0 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 0 m η = 24.0	x: 0 m η = 24.1	CUMPLE η = 24.1
N489/N494	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.935 m η = 13.9	N.P.[2]	x: 0.468 m η = 1.6	x: 0 m η = 2.2	x: 0.935 m η = 5.5	x: 0.234 m η = 0.5	x: 0 m η = 0.2	x: 0 m η = 1.8	x: 0.935 m η = 6.2	x: 0 m η < 0.1	x: 0.935 m η = 0.4	x: 0.935 m η = 15.1	N.P.[3]	x: 0 m η = 16.7	CUMPLE η = 16.7
N490/N494	$w/t \leq (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m η = 26.4	x: 0.169 m η = 0.5	x: 1.015 m η = 1.5	x: 1.015 m η = 8.5	x: 0.169 m η = 0.6	x: 1.015 m η = 0.2	x: 1.015 m η = 1.0	x: 1.015 m η = 8.7	x: 1.015 m η < 0.1	x: 1.015 m η = 0.8	N.P.[1]	x: 1.015 m η = 28.2	x: 1.015 m η = 28.2	CUMPLE η = 28.2
N490/N495	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.932 m η = 16.0	N.P.[2]	x: 0.466 m η = 1.0	x: 0 m η = 2.9	x: 0.932 m η = 10.4	x: 0.233 m η = 0.9	x: 0 m η = 0.3	x: 0 m η = 1.8	x: 0.932 m η = 10.8	x: 0 m η = 0.1	x: 0.932 m η = 1.2	x: 0.932 m η = 22.8	N.P.[3]	x: 0.932 m η = 20.3	CUMPLE η = 22.8
N491/N495	$w/t \leq (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m η = 30.8	x: 0.339 m η = 1.3	x: 0 m η = 4.0	x: 1.017 m η = 9.6	x: 0.339 m η = 0.8	x: 1.017 m η = 0.4	x: 1.017 m η = 2.5	x: 1.017 m η = 10.1	x: 0 m η = 0.2	x: 1.017 m η = 1.0	N.P.[1]	x: 0 m η = 35.5	x: 0 m η = 35.8	CUMPLE η = 35.8
N491/N496	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.932 m η = 16.2	N.P.[2]	x: 0.932 m η = 0.6	x: 0 m η = 4.0	x: 0.932 m η = 8.4	x: 0.932 m η = 0.6	x: 0 m η = 0.2	x: 0 m η = 2.3	x: 0.932 m η = 8.7	x: 0 m η = 0.2	x: 0.932 m η = 0.8	x: 0.932 m η = 20.3	N.P.[3]	x: 0 m η = 21.2	CUMPLE η = 21.2
N473/N496	$w/t \leq (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m η = 31.6	x: 0.871 m η = 3.4	x: 0 m η = 5.0	x: 0 m η = 6.1	η = 0.3	x: 0.871 m η = 0.5	x: 0 m η = 4.8	x: 0 m η = 7.5	x: 0 m η = 0.3	x: 0 m η = 0.6	N.P.[1]	x: 0 m η = 37.6	x: 0 m η = 37.9	CUMPLE η = 37.9
N501/N497	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.41 m η = 21.7	x: 1.41 m η = 35.5	x: 1.41 m η = 1.9	x: 0 m η = 1.8	x: 1.41 m η = 18.5	x: 1.41 m η = 1.7	x: 0 m η = 0.1	x: 0 m η = 2.7	x: 1.41 m η = 19.3	x: 0 m η = 0.1	x: 1.41 m η = 3.8	x: 1.41 m η = 48.2	x: 1.41 m η = 58.0	x: 1.41 m η = 58.6	CUMPLE η = 58.6
N497/N498	$w/t \leq (w/t)_{Max}$ Cumple	x: 0 m η = 13.7	x: 0 m η = 13.7	x: 0 m η = 0.6	x: 1.167 m η = 1.5	x: 0 m η = 37.9	x: 0 m η = 4.7	x: 0 m η = 0.1	x: 0.233 m η = 1.2	x: 0 m η = 38.2	x: 1.167 m η < 0.1	x: 0 m η = 14.8	x: 0 m η = 62.9	x: 0 m η = 52.3	x: 0 m η = 61.0	CUMPLE η = 62.9
N498/N499	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.35 m η = 13.3	x: 0 m η = 1.7	η = 1.1	x: 1.35 m η = 4.5	x: 1.35 m η = 54.6	η = 6.3	x: 0 m η = 0.3	x: 1.35 m η = 4.5	x: 1.35 m η = 55.1	x: 1.35 m η = 0.2	x: 1.35 m η = 30.8	x: 1.35 m η = 78.2	x: 1.35 m η = 5.8	x: 1.35 m η = 74.8	CUMPLE η = 78.2
N499/N500	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.79 m η = 16.8	x: 0 m η = 2.9	η = 7.0	x: 0 m η = 10.6	x: 0 m η = 49.5	η = 10.0	x: 0.79 m η = 2.2	x: 0 m η = 8.0	x: 0 m η = 52.6	x: 0 m η = 1.2	x: 0 m η = 28.6	x: 0 m η = 80.5	x: 0 m η = 5.8	x: 0 m η = 69.0	CUMPLE η = 80.5
N499/N502	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.073 m η = 1.9	x: 0 m η = 4.0	η = 2.5	x: 1.073 m η = 9.7	x: 1.073 m η = 14.8	η = 2.0	x: 1.073 m η = 1.4	x: 1.073 m η = 9.8	x: 1.073 m η = 15.9	x: 1.073 m η = 1.0	x: 1.073 m η = 2.6	x: 1.073 m η = 28.5	x: 1.073 m η = 22.8	x: 1.073 m η = 22.6	CUMPLE η = 28.5
N497/N503	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.869 m η = 6.3	x: 0 m η = 19.9	x: 0.652 m η = 1.6	x: 0 m η = 3.8	x: 0 m η = 9.1	x: 0.652 m η = 0.8	x: 0 m η = 0.4	x: 0 m η = 3.4	x: 0 m η = 9.7	x: 0 m η = 0.1	x: 0 m η = 1.0	N.P.[1]	x: 0 m η = 24.0	x: 0 m η = 24.6	CUMPLE η = 24.6
N503/N498	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.983 m η = 12.4	x: 0 m η = 7.3	η = 0.4	x: 0 m η = 2.2	x: 0 m η = 28.1	x: 0.492 m η = 2.8	x: 0.983 m η = 0.2	x: 0 m η = 2.3	x: 0 m η = 28.2	x: 0 m η < 0.1	x: 0 m η = 8.0	x: 0 m η = 42.4	x: 0 m η = 10.0	x: 0 m η = 40.9	CUMPLE η = 42.4
N498/N504	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.685 m η = 4.1	x: 0.685 m η = 13.4	x: 0.514 m η = 0.8	x: 0 m η = 3.1	x: 1.028 m η = 1.2	η < 0.1	x: 0 m η = 0.3	x: 0 m η = 2.2	x: 1.028 m η = 1.6	x: 0 m η = 0.1	x: 1.028 m η < 0.1	N.P.[1]	x: 0 m η = 16.4	x: 0 m η = 17.2	CUMPLE η = 17.2
N504/N499	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.186 m η = 7.5	x: 0.186 m η = 5.3	x: 0.743 m η = 5.0	x: 1.114 m η = 1.6	x: 1.114 m η = 29.6	x: 0.371 m η = 2.3	x: 0 m η = 0.1	x: 1.114 m η = 3.3	x: 1.114 m η = 31.7	x: 1.114 m η = 0.1	x: 1.114 m η = 10.1	x: 1.114 m η = 50.0	x: 1.114 m η = 39.6	x: 1.114 m η = 44.2	CUMPLE η = 50.0
N502/N500	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.365 m η = 6.3	x: 0 m η = 58.2	η = 3.8	x: 0 m η = 3.8	x: 0 m η = 9.4	η = 0.5	x: 0 m η = 0.3	x: 0 m η = 3.8	x: 0 m η = 11.0	x: 0 m η = 0.1	x: 0 m η = 1.2	N.P.[1]	x: 0 m η = 63.6	x: 0 m η = 62.9	CUMPLE η = 63.6
N509/N505	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.41 m η = 20.5	x: 1.41 m η = 33.5	x: 1.41 m η = 2.0	x: 0 m η = 1.7	x: 1.41 m η = 16.6	x: 1.41 m η = 1.5	x: 0 m η = 0.1	x: 0 m η = 2.6	x: 1.41 m η = 17.5	x: 0 m η = 0.1	x: 1.41 m η = 3.1	x: 1.41 m η = 44.5	x: 1.41 m η = 53.7	x: 1.41 m η = 54.2	CUMPLE η = 54.2
N505/N506	$w/t \leq (w/t)_{Max}$ Cumple	x: 0 m η = 14.1	x: 0 m η = 14.1	x: 0 m η = 0.4	x: 0.7 m η = 1.5	x: 0 m η = 38.3	x: 0 m η = 4.7	x: 0 m η = 0.1	x: 0.7 m η = 1.5	x: 0 m η = 38.4	x: 0.7 m η < 0.1	x: 0 m η = 15.0	x: 0 m η = 63.3	x: 0 m η = 52.8	x: 0 m η = 61.9	CUMPLE η = 63.3
N506/N507	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.35 m η = 13.1	x: 0 m η = 3.3	x: 0 m η = 0.8	x: 1.35 m η = 4.5	x: 1.35 m η = 55.2	x: 0 m η = 6.4	x: 0 m η = 0.3	x: 1.35 m η = 4.5	x: 1.35 m η = 55.5	x: 1.35 m η = 0.2	x: 1.35 m η = 31.2	x: 1.35 m η = 76.5	x: 0 m η = 6.3	x: 1.35 m η = 74.0	CUMPLE η = 76.5
N507/N508	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.79 m η = 16.5	x: 0 m η = 3.9	η = 6.4	x: 0 m η = 9.8	x: 0 m η = 49.6	η = 10.0	x: 0.79 m η = 1.9	x: 0 m η = 7.9	x: 0 m η = 52.4	x: 0 m η = 1.0	x: 0 m η = 28.5	x: 0 m η = 80.4	x: 0 m η = 7.9	x: 0 m η = 68.5	CUMPLE η = 80.4
N513/N505	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.424 m η = 25.7	x: 0.424 m η = 16.8	x: 0.847 m η = 0.9	x: 0 m η = 9.6	x: 0 m η = 57.1	x: 0.847 m η = 6.6	x: 0 m η = 0.8	x: 0 m η = 9.6	x: 0 m η = 57.5	x: 0 m η = 0.9	x: 0 m η = 33.5	x: 0 m η = 92.8	x: 0 m η = 62.2	x: 0 m η = 87.3	CUMPLE η = 92.8
N505/N512	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.869 m η = 8.3	x: 0 m η = 21.8	x: 0.652 m η = 1.7	x: 0 m η = 3.7	x: 0 m η = 7.3	x: 0.652 m η = 0.6	x: 0 m η = 0.4	x: 0.869 m η = 3.5	x: 0 m η = 8.0	x: 0 m η = 0.1	x: 0 m η = 0.6	N.P.[1]	x: 0.869 m η = 25.8	x: 0.869 m η = 26.2	CUMPLE η = 26.2

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N512/N506	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.963 m η = 13.8	x: 0 m η = 9.7	η = 0.5	x: 0 m η = 2.7	x: 0 m η = 29.4	x: 0.492 m η = 3.0	x: 0.983 m η = 0.3	x: 0 m η = 2.7	x: 0 m η = 29.7	x: 0 m η = 0.1	x: 0 m η = 8.9	x: 0 m η = 43.9	x: 0 m η = 12.6	x: 0 m η = 41.4	CUMPLE η = 43.9
N506/N511	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.685 m η = 5.4	x: 0.685 m η = 15.0	η = 0.7	x: 0 m η = 3.0	x: 1.028 m η = 1.9	x: 0.514 m η = 0.1	x: 0 m η = 0.3	x: 0 m η = 2.3	x: 1.028 m η = 2.2	x: 0 m η = 0.1	x: 1.028 m η < 0.1	N.P.[1]	x: 0 m η = 17.5	x: 0 m η = 17.7	CUMPLE η = 17.7
N511/N507	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.186 m η = 8.5	x: 0.186 m η = 6.9	x: 0.371 m η = 5.0	x: 1.114 m η = 1.7	x: 1.114 m η = 30.1	x: 0.371 m η = 2.3	x: 0 m η = 0.1	x: 1.114 m η = 3.4	x: 1.114 m η = 32.2	x: 1.114 m η = 0.1	x: 1.114 m η = 10.4	x: 1.114 m η = 50.3	x: 1.114 m η = 39.8	x: 1.114 m η = 44.5	CUMPLE η = 50.3
N507/N510	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.073 m η = 2.5	x: 0 m η = 4.5	x: 0.715 m η = 2.7	x: 1.073 m η = 8.4	x: 1.073 m η = 14.5	η = 2.0	x: 1.073 m η = 1.2	x: 1.073 m η = 8.4	x: 1.073 m η = 15.7	x: 1.073 m η = 0.7	x: 1.073 m η = 2.5	x: 1.073 m η = 28.6	x: 1.073 m η = 22.7	x: 1.073 m η = 22.7	CUMPLE η = 28.6
N510/N508	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.365 m η = 9.2	x: 0 m η = 60.4	η = 4.0	x: 0 m η = 3.4	x: 0 m η = 10.3	η = 0.6	x: 0 m η = 0.4	x: 0 m η = 3.9	x: 0 m η = 12.0	x: 0 m η = 0.2	x: 0 m η = 1.5	N.P.[1]	x: 0 m η = 65.4	x: 0 m η = 64.7	CUMPLE η = 65.4
N502/N514	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.617 m η = 2.9	x: 0 m η = 26.6	x: 0.617 m η = 4.4	x: 0 m η = 17.5	x: 0 m η = 6.2	η = 0.9	x: 0 m η = 3.3	x: 0 m η = 17.5	x: 0 m η = 8.1	x: 0 m η = 3.2	x: 0 m η = 0.7	x: 0 m η = 3.9	x: 0 m η = 44.5	x: 0 m η = 48.5	CUMPLE η = 48.5
N514/N515	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.081 m η = 5.3	x: 0 m η = 18.1	η = 2.0	x: 0 m η = 1.6	x: 0 m η = 4.2	x: 0.721 m η = 0.6	x: 1.081 m η = 0.3	x: 0 m η = 1.6	x: 0 m η = 5.1	x: 0 m η < 0.1	x: 0 m η = 0.3	N.P.[1]	x: 0 m η = 19.8	x: 0 m η = 20.1	CUMPLE η = 20.1
N515/N516	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.088 m η = 7.3	x: 1.088 m η = 13.0	x: 0.907 m η = 1.9	x: 0 m η = 1.9	x: 1.088 m η = 2.8	x: 0.907 m η = 0.4	x: 0 m η = 0.3	x: 0 m η = 2.0	x: 1.088 m η = 3.6	x: 0 m η < 0.1	x: 1.088 m η = 0.1	x: 1.088 m η = 6.5	x: 0 m η = 14.9	x: 0 m η = 15.2	CUMPLE η = 15.2
N516/N517	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.08 m η = 8.3	x: 0 m η = 9.4	x: 0.9 m η = 0.8	x: 1.08 m η = 1.0	x: 0 m η = 1.6	η = 0.2	x: 0 m η = 0.2	x: 1.08 m η = 1.1	x: 0 m η = 1.9	x: 1.08 m η < 0.1	x: 0 m η < 0.1	x: 0 m η = 6.5	x: 0 m η = 10.3	x: 0 m η = 10.4	CUMPLE η = 10.4
N517/N518	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.085 m η = 9.4	x: 0 m η = 7.0	η = 0.1	x: 1.085 m η = 1.6	x: 1.085 m η = 2.9	x: 0.542 m η = 0.5	x: 0 m η = 0.2	x: 1.085 m η = 1.6	x: 1.085 m η = 2.9	x: 1.085 m η < 0.1	x: 1.085 m η = 0.1	x: 1.085 m η = 10.4	x: 0 m η = 7.7	x: 0.904 m η = 10.7	CUMPLE η = 10.7
N518/N519	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.082 m η = 10.2	x: 1.082 m η = 4.8	η = 0.3	x: 1.082 m η = 1.7	x: 1.082 m η = 4.3	η = 0.4	x: 0 m η = 0.1	x: 1.082 m η = 1.7	x: 1.082 m η = 4.4	x: 1.082 m η < 0.1	x: 1.082 m η = 0.2	x: 1.082 m η = 13.2	x: 0 m η = 5.6	x: 1.082 m η = 12.3	CUMPLE η = 13.2
N519/N520	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.085 m η = 12.7	x: 1.085 m η = 3.1	η = 0.3	x: 0.904 m η = 1.7	x: 0 m η = 4.8	x: 0.181 m η = 0.6	x: 0 m η = 0.1	x: 0.904 m η = 1.7	x: 0 m η = 4.9	x: 0.904 m η < 0.1	x: 0 m η = 0.2	x: 1.085 m η = 15.1	x: 0 m η = 5.6	x: 0.904 m η = 14.9	CUMPLE η = 15.1
N520/N521	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.081 m η = 14.5	x: 0.901 m η = 1.5	η = 0.7	x: 1.081 m η = 2.0	x: 1.081 m η = 3.3	x: 0.18 m η = 0.4	x: 0 m η = 0.1	x: 0.36 m η = 1.2	x: 1.081 m η = 3.5	x: 1.081 m η < 0.1	x: 1.081 m η = 0.1	x: 1.081 m η = 17.3	x: 1.081 m η = 5.0	x: 1.081 m η = 17.1	CUMPLE η = 17.3
N522/N521	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.08 m η = 15.2	x: 0 m η = 1.1	η = 1.2	x: 0.72 m η = 2.0	x: 1.08 m η = 1.0	η = 0.1	x: 0 m η = 0.1	x: 0.72 m η = 1.5	x: 1.08 m η = 1.5	x: 0.72 m η < 0.1	x: 1.08 m η < 0.1	x: 0.72 m η = 17.9	x: 0.36 m η = 3.3	x: 0.72 m η = 17.7	CUMPLE η = 17.9
N523/N522	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.084 m η = 14.2	x: 0 m η = 0.1	x: 0.722 m η = 1.1	x: 0.722 m η = 1.9	x: 0 m η = 1.1	x: 0.361 m η = 0.2	x: 0 m η = 0.1	x: 0.722 m η = 2.0	x: 0 m η = 1.4	x: 0.722 m η < 0.1	x: 0 m η < 0.1	x: 1.084 m η = 16.9	x: 0 m η = 2.2	x: 0.722 m η = 16.7	CUMPLE η = 16.9
N524/N523	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.08 m η = 12.0	N.P.[2]	η = 0.5	x: 1.08 m η = 1.9	x: 1.08 m η = 2.2	x: 0.9 m η = 0.2	x: 0 m η = 0.1	x: 1.08 m η = 1.9	x: 1.08 m η = 2.4	x: 1.08 m η < 0.1	x: 1.08 m η = 0.1	x: 1.08 m η = 14.5	N.P.[3]	x: 1.08 m η = 14.4	CUMPLE η = 14.5
N525/N524	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.083 m η = 8.2	x: 0.902 m η = 1.4	η = 0.5	x: 1.083 m η = 1.8	x: 0 m η = 2.9	η = 0.5	x: 0 m η = 0.2	x: 1.083 m η = 1.9	x: 0 m η = 2.9	x: 1.083 m η < 0.1	x: 0 m η = 0.1	x: 1.083 m η = 10.5	x: 1.083 m η = 4.2	x: 1.083 m η = 10.4	CUMPLE η = 10.5
N526/N525	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.087 m η = 6.1	x: 1.087 m η = 5.4	x: 0.906 m η = 0.5	x: 0 m η = 1.9	x: 0 m η = 2.4	x: 0.906 m η = 0.3	x: 0 m η = 0.2	x: 0 m η = 2.0	x: 0 m η = 2.6	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 10.2	x: 0 m η = 8.7	x: 0 m η = 8.9	CUMPLE η = 10.2
N527/N526	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.085 m η = 7.8	x: 0 m η = 11.9	x: 0.904 m η = 1.2	x: 1.085 m η = 1.8	x: 0 m η = 0.8	x: 0 m η = 0.1	x: 0 m η = 0.3	x: 1.085 m η = 2.1	x: 0 m η = 1.3	x: 1.085 m η < 0.1	x: 0 m η < 0.1	x: 1.085 m η = 11.3	x: 0 m η = 14.7	x: 0 m η = 14.0	CUMPLE η = 14.7
N528/N527	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.077 m η = 5.8	x: 0 m η = 15.0	η = 1.2	x: 1.077 m η = 1.4	x: 0 m η = 2.7	η = 0.4	x: 1.077 m η = 0.2	x: 1.077 m η = 1.8	x: 0 m η = 3.2	x: 1.077 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 1.077 m η = 17.9	x: 1.077 m η = 16.9	CUMPLE η = 17.9
N510/N528	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.801 m η = 3.5	x: 0 m η = 23.8	x: 0.801 m η = 3.5	x: 0 m η = 14.6	x: 0 m η = 5.7	x: 0.801 m η = 0.7	x: 0 m η = 2.1	x: 0 m η = 14.6	x: 0 m η = 7.2	x: 0 m η = 2.2	x: 0 m η = 0.5	N.P.[1]	x: 0 m η = 38.8	x: 0 m η = 42.0	CUMPLE η = 42.0
N530/N529	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.128 m η = 9.1	x: 0 m η = 20.5	η = 1.9	x: 1.128 m η = 2.3	x: 0 m η = 12.2	x: 0.564 m η = 1.8	x: 0 m η = 0.3	x: 1.128 m η = 2.3	x: 0 m η = 13.1	x: 1.128 m η = 0.1	x: 0 m η = 1.7	x: 0 m η = 12.5	x: 0 m η = 23.1	x: 0 m η = 24.1	CUMPLE η = 24.1
N531/N530	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.126 m η = 16.6	x: 0 m η = 24.1	x: 0.939 m η = 2.6	x: 0 m η = 2.8	x: 1.126 m η = 9.7	x: 0.939 m η = 1.3	x: 0 m η = 0.3	x: 0 m η = 2.9	x: 1.126 m η = 10.8	x: 0 m η = 0.1	x: 1.126 m η = 1.2	x: 0 m η = 23.2	x: 0 m η = 28.6	x: 0 m η = 27.7	CUMPLE η = 28.6
N532/N531	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.126 m η = 9.0	x: 1.126 m η = 8.9	x: 0.188 m η = 1.0	x: 1.126 m η = 2.2	x: 0 m η = 2.0	x: 0.188 m η = 0.3	x: 0 m η = 0.3	x: 1.126 m η = 2.6	x: 0 m η = 2.4	x: 1.126 m η = 0.1	x: 0 m η = 0.1	x: 1.126 m η = 14.2	x: 1.126 m η = 13.6	x: 1.126 m η = 12.4	CUMPLE η = 14.2
N533/N532	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.12 m η = 13.2	x: 0 m η = 6.7	x: 0.747 m η = 1.5	x: 0 m η = 8.0	x: 1.12 m η = 3.8	x: 0.187 m η = 0.5	x: 0 m η = 1.0	x: 0 m η = 8.0	x: 1.12 m η = 4.5	x: 0 m η = 0.7	x: 1.12 m η = 0.2	x: 0 m η = 23.7	x: 1.12 m η = 9.5	x: 0 m η = 22.9	CUMPLE η = 23.7
N508/N533	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.187 m η = 21.3	x: 0 m η = 4.9	x: 0.594 m η = 6.8	x: 1.187 m η = 6.9	x: 0 m η = 15.0	x: 0.594 m η = 1.8	x: 1.187 m η = 1.0	x: 1.187 m η = 7.0	x: 0 m η = 18.0	x: 1.187 m η = 0.5	x: 0 m η = 3.3	x: 0 m η = 43.8	x: 0 m η = 22.4	x: 0 m η = 33.2	CUMPLE η = 43.8
N524/N529	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.934 m η = 9.2	x: 0 m η = 4.1	x: 0 m η = 1.6	x: 0 m η = 1.7	x: 0.934 m η = 3.8	x: 0 m η = 0.2	x: 0 m η = 0.2	x: 0 m η = 1.7	x: 0.934 m η = 4.4	x: 0 m η < 0.1	x: 0.934 m η = 0.2	N.P.[1]	x: 0 m η = 5.4	x: 0.934 m η = 10.6	CUMPLE η = 10.6
N525/N529	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.006 m η = 3.9	x: 0 m η = 16.9	x: 0.503 m η = 0.6	x: 0 m η = 1.9	x: 1.006 m η = 4.6	x: 0.503 m η = 0.3	x: 1.006 m η = 0.2	x: 1.006 m η = 1.1	x: 1.006 m η = 4.8	x: 0 m η < 0.1	x: 1.006 m η = 0.2	N.P.[1]	x: 0 m η = 19.2	x: 0 m η = 19.4	CUMPLE η = 19.4
N525/N530	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.94 m η = 12.1	x: 0 m η = 3.9	η = 0.1	x: 0 m η = 2.5	x: 0.94 m η = 8.5	x: 0 m η = 0.8	x: 0 m η = 0.3	x: 0 m η = 2.5	x: 0.94 m η = 8.5	x: 0 m η = 0.1	x: 0.94 m η = 0.7	x: 0.94 m η = 18.8	x: 0.94 m η = 6.7	x: 0.94 m η = 17.3	CUMPLE η = 18.8
N526/N530	$w/t \leq (w/t)_{Max}$ Cumple	x: 1.014 m η = 5.1	x: 0 m η = 21.6	x: 0.338 m η = 0.2	x: 0 m η = 2.2	x: 1.014 m η = 6.0	x: 0.507 m η = 0.6	x: 1.014 m η = 0.2	x: 1.014 m η = 1.3	x: 1.014 m η = 6.1	x: 0 m η < 0.1	x: 1.014 m η = 0.4	x: 1.014 m η = 8.3	x: 0 m η = 24.2	x: 0 m η = 24.3	CUMPLE η = 24.3
N526/N531	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.935 m η = 14.0	x: 0.701 m η = 5.9	η = 0.2	x: 0 m η = 2.4	x: 0.935 m η = 6.1	x: 0 m η = 0.4	x: 0 m η = 0.2	x: 0 m η = 2.5	x: 0.935 m η = 6.2	x: 0 m η = 0.1	x: 0.935 m η = 0.4	x: 0.935 m η = 17.9	x: 0 m η = 9.0	x: 0 m η = 16.7	CUMPLE η = 17.9
N527/N531	$w/t \leq (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m η = 26.6	η = 1.6	x: 1.015 m η = 1.5	x: 1.015 m η = 1.5	x: 0.508 m η = 0.1	x: 1.015 m η = 0.2	x: 1.015 m η = 1.6	x: 1.015 m η = 1.8	x: 1.015 m η < 0.1	x: 1.015 m η < 0.1	N.P.[1]	x: 1.015 m η = 28.5	x: 1.015 m η = 28.4	CUMPLE η = 28.5
N527/N532	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.932 m η = 16.1	N.P.[2]	x: 0.932 m η = 0.9	x: 0 m η = 2.9	x: 0 m η = 2.7	η = 0.1	x: 0 m η = 0.3	x: 0 m η = 2.1	x: 0 m η = 3.1	x: 0 m η = 0.1	x: 0 m η = 0.1	N.P.[1]	N.P.[3]	x: 0 m η = 19.6	CUMPLE η = 19.6
N528/N532	$w/t \leq (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m η = 30.9	x: 0.169 m η = 0.7	x: 0 m η = 4.0	x: 0 m η = 1.4	η < 0.1	x: 1.017 m η = 0.4	x: 1.017 m η = 2.0	x: 0 m η = 1.7	x: 0 m η = 0.2	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 35.6	x: 0 m η = 35.9	CUMPLE η = 35.9
N528/N533	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.932 m η = 16.1	N.P.[2]	x: 0 m η = 0.8	x: 0 m η = 4.0	x: 0 m η = 0.8	η = 0.1	x: 0 m η = 0.2	x: 0 m η = 2.4	x: 0 m η = 1.1	x: 0 m η = 0.2	x: 0 m η < 0.1	N.P.[1]	N.P.[3]	x: 0 m η = 21.1	CUMPLE η = 21.1
N510/N533	$w/t \leq (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m η = 31.3	x: 0.218 m η = 2.3	x: 0 m η = 5.0	x: 0 m η = 10.3	x: 0.218 m η = 1.1	x: 0.871 m η = 0.5	x: 0 m η = 4.9	x: 0 m η = 11.3	x: 0 m η = 0.3	x: 0 m η = 1.3	N.P.[1]	x: 0 m η = 37.2	x: 0 m η = 37.6	CUMPLE η = 37.6
N509/N513	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.566 m η = 19.9	x: 0.566 m η = 50.6	η = 5.0	x: 0.755 m η = 10.9	x: 0 m η = 21.1	x: 0.189 m η = 2.0	x: 0.755 m η = 1.1	x: 0.755 m η = 13.0	x: 0 m η = 23.2	x: 0.755 m η = 1.7	x: 0 m η = 5.4	x: 0 m η = 15.9	x: 0.755 m η = 58.7	x: 0.755 m η = 57.7	CUMPLE η = 58.7
N534/N497	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.847 m η = 22.9	x: 0.424 m η = 12.5	x: 0.424 m η = 0.8	x: 0 m η = 8.3	x: 0 m η = 56.4	x: 0.847 m η = 6.5	x: 0 m η = 0.7	x: 0 m η = 8.3	x: 0 m η = 56.8	x: 0 m η = 0.7	x: 0 m η = 32.7	x: 0 m η = 85.6	x: 0 m η = 22.2	x: 0 m η = 81.7	CUMPLE η = 85.6

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_z	M_y	V_z	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N501/N534	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.755 m η = 14.6	x: 0 m η = 46.6	η = 5.0	x: 0.755 m η = 11.1	x: 0 m η = 20.2	η = 1.9	x: 0.755 m η = 1.1	x: 0.755 m η = 13.2	x: 0 m η = 22.4	x: 0.755 m η = 1.8	x: 0 m η = 5.0	N.P.[1]	x: 0 m η = 50.7	x: 0.755 m η = 49.9	CUMPLE η = 50.7
N534/N467	w / t ≤ (w / t)$_{Máx.}$ Cumple	η < 0.1	η < 0.1	η = 3.6	x: 0.3 m η = 26.4	x: 0.3 m η = 2.5	η = 1.0	x: 0.3 m η = 52.0	x: 0.3 m η = 27.9	x: 0.3 m η = 4.0	x: 0.3 m η = 90.6	x: 0.3 m η = 0.2	x: 0.3 m η = 64.9	x: 0.3 m η = 31.9	x: 0.3 m η = 49.6	CUMPLE η = 49.6
N497/N460	w / t ≤ (w / t)$_{Máx.}$ Cumple	η < 0.1	η < 0.1	η = 0.4	x: 0.3 m η = 27.3	x: 0.3 m η = 30.0	η = 12.3	x: 0 m η = 52.4	x: 0.3 m η = 27.5	x: 0.3 m η = 30.2	x: 0 m η = 90.1	x: 0.3 m η = 10.6	x: 0.3 m η = 97.1	x: 0.3 m η = 57.7	x: 0.3 m η = 67.2	CUMPLE η = 67.2
N503/N466	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 0.1	η = 0.1	η < 0.1	x: 0.3 m η = 60.9	x: 0 m η = 3.7	η = 1.6	x: 0.3 m η = 66.5	x: 0.3 m η = 60.9	x: 0 m η = 3.7	x: 0.3 m η = 305.8	x: 0 m η = 0.2	x: 0 m η = 25.7	x: 0.3 m η = 64.7	x: 0.3 m η = 44.9	CUMPLE η = 44.9
N498/N461	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.15 m η < 0.1	x: 0.15 m η < 0.1	η = 1.0	x: 0 m η = 52.0	x: 0.3 m η = 30.9	x: 0.15 m η = 13.1	x: 0.15 m η = 64.6	x: 0 m η = 52.5	x: 0.3 m η = 31.4	x: 0 m η = 74.3	x: 0.3 m η = 11.6	x: 0 m η = 29.6	x: 0 m η = 83.7	x: 0 m η = 75.9	CUMPLE η = 75.9
N504/N465	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.15 m η < 0.1	x: 0.15 m η < 0.1	η = 1.4	x: 0.3 m η = 37.3	x: 0 m η = 16.1	x: 0.15 m η = 5.4	x: 0.15 m η = 46.0	x: 0.3 m η = 37.9	x: 0 m η = 16.7	x: 0.3 m η = 11.4	x: 0 m η = 3.1	x: 0 m η = 93.2	x: 0 m η = 13.6	x: 0.3 m η = 97.1	CUMPLE η = 97.1
N499/N462	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 0.9	η = 1.9	x: 0.15 m η = 1.0	x: 0 m η = 15.8	x: 0.3 m η = 26.0	x: 0 m η = 8.5	x: 0 m η = 5.2	x: 0 m η = 16.2	x: 0.3 m η = 26.4	x: 0 m η = 2.9	x: 0.3 m η = 7.7	x: 0 m η = 52.7	x: 0 m η = 43.4	x: 0 m η = 38.7	CUMPLE η = 52.7
N502/N464	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.15 m η = 0.3	x: 0.15 m η = 0.3	η = 0.5	x: 0 m η = 33.2	x: 0 m η = 14.6	x: 0.15 m η = 4.9	x: 0.3 m η = 11.1	x: 0 m η = 33.4	x: 0 m η = 14.8	x: 0 m η = 12.4	x: 0 m η = 2.4	x: 0 m η = 60.2	x: 0 m η = 47.7	x: 0 m η = 45.2	CUMPLE η = 60.2
N500/N463	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 2.4	x: 0.15 m η = 0.7	x: 0.15 m η = 0.7	x: 0 m η = 76.0	x: 0.3 m η = 32.9	x: 0.3 m η = 11.0	x: 0.15 m η = 25.4	x: 0 m η = 76.3	x: 0.3 m η = 33.2	x: 0 m η = 64.7	x: 0.3 m η = 12.2	x: 0 m η = 37.6	x: 0 m η = 19.8	x: 0.3 m η = 19.9	CUMPLE η = 37.6
N514/N477	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 0.1	η = 0.1	x: 0.15 m η = 0.6	x: 0 m η = 18.9	x: 0.3 m η = 12.4	η = 4.1	x: 0.3 m η = 6.3	x: 0 m η = 19.2	x: 0.3 m η = 12.7	x: 0 m η = 4.1	x: 0.3 m η = 1.8	x: 0 m η = 38.9	x: 0.3 m η = 31.6	x: 0 m η = 28.1	CUMPLE η = 38.9
N515/N476	w / t ≤ (w / t)$_{Máx.}$ Cumple	η < 0.1	η < 0.1	η = 0.7	x: 0 m η = 11.9	x: 0 m η = 18.3	η = 6.1	x: 0.3 m η = 4.0	x: 0 m η = 12.2	x: 0 m η = 18.6	x: 0 m η = 1.6	x: 0 m η = 3.8	x: 0 m η = 37.9	x: 0 m η = 30.9	x: 0 m η = 27.4	CUMPLE η = 37.9
N516/N479	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.15 m η = 0.5	x: 0.15 m η = 0.5	η = 0.4	x: 0.3 m η = 2.7	x: 0.3 m η = 15.7	x: 0.15 m η = 5.3	x: 0.3 m η = 0.9	x: 0.3 m η = 2.9	x: 0.3 m η = 15.9	x: 0.3 m η = 0.1	x: 0.3 m η = 2.8	x: 0.3 m η = 23.3	x: 0.3 m η = 19.3	x: 0.3 m η = 20.5	CUMPLE η = 23.3
N517/N480	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 0.1	η = 0.1	x: 0 m η = 0.1	x: 0.3 m η = 2.1	x: 0 m η = 19.1	x: 0.15 m η = 6.4	x: 0.3 m η = 0.5	x: 0.3 m η = 2.1	x: 0 m η = 19.1	x: 0.3 m η < 0.1	x: 0 m η = 4.1	x: 0.3 m η = 26.4	x: 0.3 m η = 20.6	x: 0 m η = 23.9	CUMPLE η = 26.4
N518/N481	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 0.1	η = 0.1	η = 0.1	x: 0.3 m η = 4.8	x: 0 m η = 16.4	η = 5.4	x: 0.3 m η = 1.2	x: 0.3 m η = 4.8	x: 0 m η = 16.4	x: 0.3 m η = 0.2	x: 0 m η = 3.0	x: 0.3 m η = 26.1	x: 0.3 m η = 20.5	x: 0.3 m η = 20.9	CUMPLE η = 26.1
N519/N482	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 0.6	η = 0.6	x: 0.3 m η = 0.1	x: 0 m η = 1.8	x: 0.3 m η = 4.3	η = 1.4	x: 0.3 m η = 0.3	x: 0 m η = 1.9	x: 0.3 m η = 4.3	x: 0 m η < 0.1	x: 0.3 m η = 0.2	N.P.[1]	x: 0 m η = 5.9	x: 0.3 m η = 6.1	CUMPLE η = 6.1
N520/N483	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 0.2	η = 0.2	η = 0.2	x: 0 m η = 5.0	x: 0.3 m η = 17.9	x: 0 m η = 6.0	x: 0.3 m η = 1.2	x: 0 m η = 5.0	x: 0.3 m η = 18.0	x: 0 m η = 0.3	x: 0.3 m η = 3.6	x: 0 m η = 28.1	x: 0 m η = 23.0	x: 0 m η = 23.2	CUMPLE η = 28.1
N521/N484	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 0.1	η = 0.1	η = 0.3	x: 0 m η = 5.6	x: 0.3 m η = 9.5	x: 0 m η = 3.2	x: 0.3 m η = 1.5	x: 0 m η = 5.7	x: 0.3 m η = 9.6	x: 0 m η = 0.4	x: 0.3 m η = 1.0	x: 0 m η = 18.7	x: 0 m η = 15.1	x: 0 m η = 13.5	CUMPLE η = 18.7
N522/N485	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.3 m η = 0.1	x: 0.3 m η = 0.1	x: 0.3 m η = 0.5	x: 0 m η = 2.0	x: 0.3 m η = 7.9	x: 0 m η = 2.6	x: 0.3 m η = 0.6	x: 0 m η = 2.2	x: 0.3 m η = 8.0	x: 0 m η < 0.1	x: 0.3 m η = 0.7	x: 0.3 m η = 12.0	x: 0.3 m η = 9.2	x: 0.3 m η = 10.1	CUMPLE η = 12.0
N523/N486	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0 m η = 0.2	x: 0 m η = 0.2	x: 0.3 m η = 0.4	x: 0.3 m η = 5.4	x: 0 m η = 9.6	x: 0 m η = 3.2	x: 0.3 m η = 1.3	x: 0.3 m η = 5.6	x: 0 m η = 9.7	x: 0.3 m η = 0.3	x: 0 m η = 1.0	x: 0.3 m η = 15.1	x: 0.3 m η = 11.8	x: 0.3 m η = 12.2	CUMPLE η = 15.1
N524/N487	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 0.2	η = 0.2	x: 0 m η = 0.3	x: 0.3 m η = 6.9	x: 0 m η = 16.3	η = 5.3	x: 0.3 m η = 1.8	x: 0.3 m η = 7.0	x: 0 m η = 16.3	x: 0.3 m η = 0.5	x: 0 m η = 3.0	x: 0.3 m η = 28.6	x: 0.3 m η = 22.7	x: 0.3 m η = 21.6	CUMPLE η = 28.6
N529/N492	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.3 m η = 4.6	x: 0.3 m η = 5.0	x: 0.3 m η = 0.2	x: 0 m η = 21.1	x: 0.3 m η = 29.8	x: 0 m η = 9.2	x: 0 m η = 3.4	x: 0 m η = 21.1	x: 0.3 m η = 29.8	x: 0 m η = 4.6	x: 0.3 m η = 9.7	x: 0 m η = 62.2	x: 0 m η = 50.8	x: 0 m η = 45.5	CUMPLE η = 62.2
N525/N488	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 0.1	η = 0.1	η = 0.3	x: 0.3 m η = 3.9	x: 0 m η = 18.2	x: 0.3 m η = 6.0	x: 0.3 m η = 0.8	x: 0.3 m η = 3.9	x: 0 m η = 18.2	x: 0.3 m η = 0.2	x: 0 m η = 3.7	x: 0.3 m η = 27.2	x: 0.3 m η = 21.5	x: 0 m η = 22.8	CUMPLE η = 27.2
N530/N493	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 1.3	η = 1.8	η = 0.3	x: 0.3 m η = 7.7	x: 0.3 m η = 13.1	η = 4.0	x: 0 m η = 0.8	x: 0.3 m η = 7.8	x: 0.3 m η = 13.1	x: 0.3 m η = 0.6	x: 0.3 m η = 1.9	x: 0.3 m η = 26.6	x: 0.3 m η = 21.3	x: 0.3 m η = 19.9	CUMPLE η = 26.6
N526/N489	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 0.1	η = 0.2	x: 0 m η = 0.2	x: 0.3 m η = 5.0	x: 0 m η = 10.4	x: 0.3 m η = 3.3	x: 0.3 m η = 1.6	x: 0.3 m η = 5.1	x: 0 m η = 10.5	x: 0.3 m η = 0.3	x: 0 m η = 1.2	x: 0.3 m η = 17.6	x: 0.3 m η = 13.7	x: 0 m η = 13.3	CUMPLE η = 17.6
N531/N494	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.3 m η = 4.5	x: 0.3 m η = 5.0	x: 0 m η = 0.4	x: 0 m η = 12.2	x: 0 m η = 18.2	x: 0 m η = 5.7	x: 0 m η = 0.7	x: 0 m η = 12.3	x: 0 m η = 18.3	x: 0 m η = 1.5	x: 0 m η = 3.6	x: 0 m η = 42.5	x: 0 m η = 35.6	x: 0 m η = 32.3	CUMPLE η = 42.5
N527/N490	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 0.2	η = 0.2	η = 0.7	x: 0.3 m η = 11.7	x: 0 m η = 10.3	x: 0.3 m η = 3.2	x: 0.3 m η = 3.4	x: 0.3 m η = 11.9	x: 0 m η = 10.4	x: 0.3 m η = 1.5	x: 0 m η = 1.2	x: 0.3 m η = 26.4	x: 0.3 m η = 20.7	x: 0.3 m η = 18.6	CUMPLE η = 26.4
N532/N495	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 4.6	η = 5.1	x: 0.3 m η = 0.7	x: 0 m η = 19.9	x: 0.3 m η = 11.8	x: 0.3 m η = 3.9	x: 0 m η = 3.0	x: 0 m η = 20.0	x: 0.3 m η = 12.1	x: 0 m η = 4.1	x: 0.3 m η = 1.6	x: 0 m η = 31.8	x: 0 m η = 26.3	x: 0 m η = 29.9	CUMPLE η = 31.8
N528/N491	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 0.2	η = 0.2	η = 0.6	x: 0.3 m η = 18.5	x: 0 m η = 9.3	η = 3.0	x: 0.3 m η = 5.8	x: 0.3 m η = 18.6	x: 0 m η = 9.4	x: 0.3 m η = 3.8	x: 0 m η = 1.0	x: 0.3 m η = 34.0	x: 0.3 m η = 26.7	x: 0.3 m η = 25.5	CUMPLE η = 34.0
N533/N496	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 4.1	η = 4.4	x: 0 m η = 0.4	x: 0 m η = 12.1	x: 0.3 m η = 31.8	η = 9.3	x: 0.3 m η = 2.4	x: 0 m η = 12.1	x: 0.3 m η = 31.9	x: 0 m η = 1.5	x: 0.3 m η = 11.0	x: 0.3 m η = 49.6	x: 0.3 m η = 40.6	x: 0.3 m η = 44.5	CUMPLE η = 49.6
N510/N473	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 0.2	η = 0.2	η = 0.3	x: 0.3 m η = 35.6	x: 0.3 m η = 19.0	η = 6.3	x: 0.3 m η = 11.7	x: 0.3 m η = 35.7	x: 0.3 m η = 19.1	x: 0.3 m η = 14.1	x: 0.3 m η = 4.0	x: 0.3 m η = 68.1	x: 0.3 m η = 54.7	x: 0.3 m η = 50.1	CUMPLE η = 68.1
N508/N471	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 2.6	η = 0.1	x: 0.15 m η = 0.6	x: 0.3 m η = 77.4	x: 0.3 m η = 31.9	x: 0 m η = 10.3	x: 0 m η = 25.7	x: 0.3 m η = 77.7	x: 0.3 m η = 32.2	x: 0.3 m η = 66.9	x: 0.3 m η = 11.4	x: 0.3 m η = 37.3	x: 0.3 m η = 19.2	x: 0.3 m η = 11.5	CUMPLE η = 37.3
N507/N470	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 0.9	η = 1.6	η = 0.8	x: 0 m η = 12.8	x: 0.3 m η = 28.1	η = 9.2	x: 0.15 m η = 4.1	x: 0 m η = 13.2	x: 0.3 m η = 28.4	x: 0 m η = 1.9	x: 0.3 m η = 8.9	x: 0 m η = 51.4	x: 0 m η = 42.1	x: 0 m η = 38.9	CUMPLE η = 51.4
N511/N474	w / t ≤ (w / t)$_{Máx.}$ Cumple	η = 0.1	η < 0.1	η = 1.3	x: 0 m η = 36.7	x: 0.3 m η = 17.4	η = 5.8	x: 0.3 m η = 45.8	x: 0 m η = 37.3	x: 0.3 m η = 18.0	x: 0 m η = 29.4	x: 0.3 m η = 3.6	x: 0 m η = 94.2	x: 0 m η = 55.3	x: 0 m η = 95.8	CUMPLE η = 95.8
N506/N469	w / t ≤ (w / t)$_{Máx.}$ Cumple	η < 0.1	η < 0.1	η = 0.9	x: 0 m η = 53.5	x: 0 m η = 32.2	η = 13.7	x: 0 m η = 65.2	x: 0 m η = 53.8	x: 0 m η = 32.6	x: 0 m η = 79.2	x: 0 m η = 12.5	x: 0 m η = 32.9	x: 0 m η = 86.3	x: 0 m η = 84.1	CUMPLE η = 84.1
N512/N475	w / t ≤ (w / t)$_{Máx.}$ Cumple	η < 0.1	η < 0.1	η = 0.2	x: 0.3 m η = 58.4	x: 0.3 m η = 4.7	η = 2.0	x: 0.15 m η = 67.4	x: 0.3 m η = 58.5	x: 0.3 m η = 4.8	x: 0.3 m η = 96.5	x: 0.3 m η = 0.3	x: 0.3 m η = 24.1	x: 0.3 m η = 63.2	x: 0.3 m η = 91.9	CUMPLE η = 91.9
N505/N468	w / t ≤ (w / t)$_{Máx.}$ Cumple	η < 0.1	η < 0.1	x: 0.15 m η = 0.4	x: 0.3 m η = 23.7	x: 0.3 m η = 30.8	η = 12.7	x: 0 m η = 50.9	x: 0.3 m η = 23.9	x: 0.3 m η = 31.0	x: 0.3 m η = 79.3	x: 0.3 m η = 11.2	x: 0.3 m η = 93.5	x: 0.3 m η = 54.6	x: 0.3 m η = 53.4	CUMPLE η = 53.4
N513/N476	w / t ≤ (w / t)$_{Máx.}$ Cumple	η < 0.1	η < 0.1	η = 3.8	x: 0.3 m η = 18.5	x: 0.3 m η = 4.6	η = 1.9	x: 0.3 m η = 48.7	x: 0.3 m η = 20.1	x: 0.3 m η = 6.2	x: 0.3 m η = 68.1	x: 0 m η = 0.4	x: 0.3 m η = 57.9	x: 0.3 m η = 26.4	x: 0.3 m η = 19.7	CUMPLE η = 19.7
N529/N535	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.118 m η = 3.6	x: 0 m η = 24.2	η = 0.5	x: 1.118 m η = 2.3	x: 1.118 m η = 4.2	x: 0 m η = 0.4	x: 0 m η = 0.2	x: 1.118 m η = 2.3	x: 1.118 m η = 4.2	x: 1.118 m η = 0.1	x: 1.118 m η = 0.2	x: 1.118 m η = 5.4	x: 1.118 m η = 26.7	x: 1.118 m η = 27.0	CUMPLE η = 27.0

Listados

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N492/N536	$w/t \le (w/t)_{Max}$ Cumple	x: 1.118 m η = 0.6	x: 0 m η = 23.7	η = 0.5	x: 1.118 m η = 2.3	x: 1.118 m η = 4.3	η = 0.4	x: 0 m η = 0.2	x: 1.118 m η = 2.3	x: 1.118 m η = 4.4	x: 1.118 m η = 0.1	x: 1.118 m η = 0.2	N.P.[1]	x: 1.118 m η = 26.2	x: 1.118 m η = 26.5	CUMPLE η = 26.5
N524/N535	$w/t \le (w/t)_{Max}$ Cumple	x: 0.335 m η = 4.1	x: 0.335 m η = 11.8	x: 0.503 m η = 1.4	x: 0 m η = 1.8	x: 0 m η = 2.0	x: 0 m η = 0.1	x: 1.006 m η = 0.2	x: 0 m η = 1.3	x: 0 m η = 2.6	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 1.006 m η = 13.3	x: 1.006 m η = 13.1	CUMPLE η = 13.3
N523/N535	$w/t \le (w/t)_{Max}$ Cumple	x: 0.953 m η = 6.8	x: 0 m η = 4.4	x: 0.953 m η = 1.2	x: 0 m η = 1.2	x: 0 m η = 2.2	η < 0.1	x: 0 m η = 0.2	x: 0 m η = 1.3	x: 0 m η = 2.7	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 5.9	x: 0 m η = 8.4	CUMPLE η = 8.4
N487/N536	$w/t \le (w/t)_{Max}$ Cumple	x: 0.168 m η = 3.0	x: 0 m η = 10.6	x: 0.503 m η = 0.7	x: 0 m η = 1.8	x: 1.006 m η = 9.1	x: 0.335 m η = 0.7	x: 1.006 m η = 0.1	x: 0 m η = 1.0	x: 1.006 m η = 9.4	x: 0 m η < 0.1	x: 1.006 m η = 0.9	N.P.[1]	x: 1.006 m η = 15.1	x: 1.006 m η = 16.4	CUMPLE η = 16.4
N486/N536	$w/t \le (w/t)_{Max}$ Cumple	x: 0.953 m η = 6.0	x: 0 m η = 3.3	x: 0.715 m η = 0.6	x: 0 m η = 0.9	x: 0.953 m η = 9.5	x: 0.476 m η = 0.8	x: 0 m η = 0.1	x: 0 m η = 1.0	x: 0.953 m η = 9.7	x: 0 m η < 0.1	x: 0.953 m η = 1.0	x: 0.953 m η = 15.3	x: 0 m η = 4.4	x: 0.953 m η = 14.3	CUMPLE η = 15.3
N535/N537	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m η = 28.5	η = 1.4	x: 1.119 m η = 2.0	x: 0 m η = 2.7	x: 0.373 m η = 0.1	x: 0 m η = 0.1	x: 1.119 m η = 1.4	x: 0 m η = 3.3	x: 1.119 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 1.119 m η = 30.8	x: 1.119 m η = 31.0	CUMPLE η = 31.0
N537/N538	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m η = 30.8	x: 0.374 m η = 3.0	x: 1.122 m η = 2.1	x: 1.122 m η = 8.5	η = 1.4	x: 0 m η = 0.1	x: 1.122 m η = 2.4	x: 1.122 m η = 9.8	x: 1.122 m η = 0.1	x: 1.122 m η = 1.0	N.P.[1]	x: 1.122 m η = 33.4	x: 1.122 m η = 33.5	CUMPLE η = 33.5
N536/N539	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m η = 28.1	η = 0.6	x: 1.119 m η = 2.0	x: 0 m η = 3.2	η = 0.2	x: 0 m η = 0.1	x: 1.119 m η = 2.1	x: 0 m η = 3.3	x: 1.119 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 1.119 m η = 30.4	x: 1.119 m η = 30.6	CUMPLE η = 30.6
N539/N540	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m η = 30.3	η = 0.7	x: 1.122 m η = 2.1	x: 1.122 m η = 8.3	η = 1.4	x: 0 m η = 0.1	x: 1.122 m η = 2.2	x: 1.122 m η = 8.3	x: 1.122 m η = 0.1	x: 1.122 m η = 0.7	N.P.[1]	x: 1.122 m η = 33.1	x: 1.122 m η = 32.9	CUMPLE η = 33.1
N535/N536	$w/t \le (w/t)_{Max}$ Cumple	x: 0 m η = 4.4	x: 0 m η = 4.9	η = 0.3	x: 0 m η = 20.1	x: 0.3 m η = 6.3	x: 0.3 m η = 1.9	x: 0 m η = 2.9	x: 0 m η = 20.2	x: 0.3 m η = 6.4	x: 0 m η = 4.2	x: 0.3 m η = 0.4	x: 0 m η = 33.4	x: 0 m η = 27.9	x: 0 m η = 30.2	CUMPLE η = 33.4
N537/N539	$w/t \le (w/t)_{Max}$ Cumple	η = 3.5	η = 4.0	η = 0.4	x: 0 m η = 13.4	x: 0 m η = 20.8	x: 0.3 m η = 6.7	x: 0 m η = 1.5	x: 0 m η = 13.5	x: 0 m η = 21.0	x: 0 m η = 1.9	x: 0 m η = 4.8	x: 0 m η = 46.4	x: 0 m η = 38.4	x: 0 m η = 34.8	CUMPLE η = 46.4
N538/N540	$w/t \le (w/t)_{Max}$ Cumple	x: 0 m η = 2.2	x: 0 m η = 3.0	η = 0.4	x: 0.3 m η = 6.1	x: 0 m η = 15.6	η = 5.2	x: 0 m η = 1.3	x: 0.3 m η = 6.2	x: 0 m η = 15.7	x: 0.3 m η = 0.4	x: 0 m η = 2.7	x: 0.3 m η = 29.1	x: 0.3 m η = 22.9	x: 0.3 m η = 22.9	CUMPLE η = 29.1
N523/N537	$w/t \le (w/t)_{Max}$ Cumple	x: 0.339 m η = 4.0	x: 0.339 m η = 8.8	η = 1.5	x: 0 m η = 1.5	x: 0 m η = 0.8	x: 0 m η = 0.1	x: 1.017 m η = 0.1	x: 0 m η = 1.3	x: 0 m η = 1.5	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 9.8	x: 0 m η = 9.8	CUMPLE η = 9.8
N522/N537	$w/t \le (w/t)_{Max}$ Cumple	x: 0.974 m η = 5.4	x: 0 m η = 4.6	x: 0 m η = 0.3	x: 0 m η = 1.0	x: 0.974 m η = 3.6	η = 0.1	x: 0.974 m η = 0.1	x: 0 m η = 1.0	x: 0.974 m η = 3.7	x: 0 m η < 0.1	x: 0.974 m η = 0.1	N.P.[1]	x: 0.974 m η = 6.8	x: 0.974 m η = 8.6	CUMPLE η = 8.6
N522/N538	$w/t \le (w/t)_{Max}$ Cumple	x: 0.51 m η = 3.9	x: 0.51 m η = 6.2	x: 0.51 m η = 0.5	x: 0 m η = 1.1	x: 0 m η = 4.2	x: 0.681 m η = 0.4	x: 1.021 m η = 0.1	x: 0 m η = 0.8	x: 0 m η = 4.4	x: 0 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 0 m η = 8.5	x: 0 m η = 8.6	CUMPLE η = 8.6
N521/N538	$w/t \le (w/t)_{Max}$ Cumple	x: 0.985 m η = 4.0	x: 0 m η = 5.3	x: 0.492 m η = 0.6	x: 0 m η = 1.2	x: 0.985 m η = 6.7	x: 0.246 m η = 0.5	x: 0.985 m η = 0.1	x: 0 m η = 1.0	x: 0.985 m η = 6.9	x: 0 m η < 0.1	x: 0.985 m η = 0.5	x: 0.985 m η = 11.1	x: 0.985 m η = 9.9	x: 0.985 m η = 10.5	CUMPLE η = 11.1
N486/N539	$w/t \le (w/t)_{Max}$ Cumple	x: 1.017 m η = 3.4	x: 0 m η = 7.8	η = 0.1	x: 0 m η = 1.5	x: 1.017 m η = 7.5	η = 0.5	x: 1.017 m η = 0.1	x: 0 m η = 0.9	x: 1.017 m η = 7.6	x: 0 m η < 0.1	x: 1.017 m η = 0.6	x: 1.017 m η = 9.4	x: 1.017 m η = 10.7	x: 1.017 m η = 12.1	CUMPLE η = 12.1
N485/N539	$w/t \le (w/t)_{Max}$ Cumple	x: 0.974 m η = 4.9	x: 0 m η = 3.9	η = 1.1	x: 0 m η = 0.8	x: 0.974 m η = 5.2	x: 0.244 m η = 0.5	x: 0.974 m η = 0.1	x: 0 m η = 0.8	x: 0.974 m η = 5.6	x: 0 m η < 0.1	x: 0.974 m η = 0.3	N.P.[1]	x: 0 m η = 5.2	x: 0.974 m η = 8.3	CUMPLE η = 8.3
N485/N540	$w/t \le (w/t)_{Max}$ Cumple	x: 0.681 m η = 3.5	x: 0.681 m η = 5.5	η = 0.2	x: 0 m η = 1.0	x: 0 m η = 4.5	η = 0.4	x: 1.021 m η = 0.1	x: 0 m η = 1.1	x: 0 m η = 4.6	x: 0 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 1.021 m η = 8.3	x: 0 m η = 8.6	CUMPLE η = 8.6
N484/N540	$w/t \le (w/t)_{Max}$ Cumple	x: 0.985 m η = 3.5	x: 0 m η = 4.6	x: 0.492 m η = 1.0	x: 0 m η = 1.1	x: 0.985 m η = 5.3	x: 0 m η = 0.5	x: 0.985 m η = 0.1	x: 0 m η = 1.1	x: 0.985 m η = 5.8	x: 0 m η < 0.1	x: 0.985 m η = 0.3	x: 0.985 m η = 8.6	x: 0 m η = 6.8	x: 0.985 m η = 7.5	CUMPLE η = 8.6
N521/N541	$w/t \le (w/t)_{Max}$ Cumple	x: 1.026 m η = 4.3	x: 0.513 m η = 3.7	η = 0.2	x: 0.171 m η = 0.7	x: 1.026 m η = 8.5	η = 0.7	x: 1.026 m η = 0.1	x: 0 m η = 0.6	x: 1.026 m η = 8.5	x: 0.171 m η < 0.1	x: 1.026 m η = 0.7	x: 1.026 m η = 12.6	x: 0 m η = 5.4	x: 1.026 m η = 12.1	CUMPLE η = 12.6
N520/N541	$w/t \le (w/t)_{Max}$ Cumple	x: 0.336 m η = 2.6	x: 0.336 m η = 6.0	x: 0.168 m η = 0.7	x: 0 m η = 1.4	x: 1.007 m η = 8.5	x: 0.504 m η = 0.7	x: 1.007 m η = 0.1	x: 0 m η = 1.1	x: 1.007 m η = 8.8	x: 0 m η < 0.1	x: 1.007 m η = 0.8	x: 1.007 m η = 11.6	x: 1.007 m η = 11.7	x: 1.007 m η = 13.0	CUMPLE η = 13.0
N538/N541	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m η = 31.8	x: 0 m η = 1.3	x: 0.373 m η = 1.8	x: 0 m η = 4.0	x: 0 m η = 0.7	x: 1.12 m η = 0.1	x: 0.933 m η = 1.4	x: 0 m η = 4.6	x: 0.373 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 0.187 m η = 33.9	x: 0.373 m η = 34.1	CUMPLE η = 34.1
N542/N541	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m η = 29.4	η = 0.8	x: 1.122 m η = 2.1	x: 1.122 m η = 6.7	x: 0.187 m η = 1.1	x: 0 m η = 0.2	x: 1.122 m η = 2.1	x: 1.122 m η = 7.0	x: 1.122 m η < 0.1	x: 1.122 m η = 0.5	N.P.[1]	x: 1.122 m η = 31.8	x: 1.122 m η = 32.0	CUMPLE η = 32.0
N543/N542	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m η = 26.3	η = 0.2	x: 1.131 m η = 1.7	x: 0 m η = 3.8	η = 0.3	x: 0 m η = 0.1	x: 1.131 m η = 1.7	x: 0 m η = 3.8	x: 1.131 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 1.131 m η = 28.2	x: 1.131 m η = 28.4	CUMPLE η = 28.4
N544/N543	$w/t \le (w/t)_{Max}$ Cumple	x: 1.128 m η = 0.7	x: 0 m η = 21.4	x: 0.752 m η = 0.6	x: 1.128 m η = 2.3	x: 1.128 m η = 4.5	x: 0.752 m η = 0.4	x: 0 m η = 0.2	x: 1.128 m η = 2.3	x: 1.128 m η = 4.7	x: 1.128 m η = 0.1	x: 1.128 m η = 0.2	N.P.[1]	x: 1.128 m η = 24.1	x: 1.128 m η = 24.2	CUMPLE η = 24.2
N545/N544	$w/t \le (w/t)_{Max}$ Cumple	x: 1.138 m η = 3.2	x: 0 m η = 14.5	η = 1.6	x: 1.138 m η = 1.7	x: 0 m η = 12.1	η = 1.8	x: 0 m η = 0.3	x: 1.138 m η = 1.7	x: 0 m η = 12.8	x: 1.138 m η < 0.1	x: 0 m η = 1.7	N.P.[1]	x: 0 m η = 20.4	x: 0 m η = 21.5	CUMPLE η = 21.5
N546/N545	$w/t \le (w/t)_{Max}$ Cumple	x: 0.957 m η = 6.7	x: 0.957 m η = 11.1	x: 0.766 m η = 1.2	x: 1.148 m η = 1.8	x: 1.148 m η = 9.3	x: 0.383 m η = 1.2	x: 0 m η = 0.4	x: 1.148 m η = 1.8	x: 1.148 m η = 9.8	x: 1.148 m η < 0.1	x: 1.148 m η = 1.0	x: 0.957 m η = 10.1	x: 1.148 m η = 14.4	x: 1.148 m η = 14.7	CUMPLE η = 14.7
N547/N546	$w/t \le (w/t)_{Max}$ Cumple	x: 1.129 m η = 10.2	x: 0 m η = 8.5	η = 2.0	x: 0 m η = 1.5	x: 0 m η = 3.3	η = 0.3	x: 0 m η = 0.3	x: 0 m η = 1.7	x: 0 m η = 4.2	x: 0 m η < 0.1	x: 0 m η = 0.2	x: 0 m η = 10.6	x: 1.129 m η = 9.6	x: 0 m η = 11.4	CUMPLE η = 11.4
N548/N547	$w/t \le (w/t)_{Max}$ Cumple	x: 1.12 m η = 16.0	x: 0 m η = 5.3	x: 1.12 m η = 0.9	x: 0 m η = 9.3	x: 1.12 m η = 4.5	x: 1.12 m η = 0.5	x: 0 m η = 1.1	x: 0 m η = 9.3	x: 1.12 m η = 4.9	x: 0 m η = 0.9	x: 1.12 m η = 0.2	x: 0 m η = 28.4	x: 1.12 m η = 6.2	x: 0 m η = 27.6	CUMPLE η = 28.4
N500/N548	$w/t \le (w/t)_{Max}$ Cumple	x: 0.902 m η = 21.1	x: 0 m η = 3.4	x: 0.677 m η = 5.3	x: 0.902 m η = 8.4	x: 0 m η = 16.8	x: 0.226 m η = 2.7	x: 0.902 m η = 1.6	x: 0.902 m η = 8.4	x: 0 m η = 19.2	x: 0.902 m η = 0.7	x: 0 m η = 3.8	x: 0 m η = 44.5	x: 0 m η = 21.4	x: 0 m η = 34.6	CUMPLE η = 44.5
N520/N542	$w/t \le (w/t)_{Max}$ Cumple	x: 1.034 m η = 5.4	x: 0.862 m η = 1.8	x: 0.345 m η = 0.8	x: 0.689 m η = 0.5	x: 1.034 m η = 5.6	x: 0.172 m η = 0.4	x: 0 m η = 0.1	x: 1.034 m η = 0.7	x: 1.034 m η = 5.9	x: 0.862 m η < 0.1	x: 1.034 m η = 0.4	x: 1.034 m η = 11.9	x: 1.034 m η = 6.9	x: 1.034 m η = 10.6	CUMPLE η = 11.9
N519/N542	$w/t \le (w/t)_{Max}$ Cumple	x: 0.171 m η = 2.1	x: 0.171 m η = 6.6	η = 1.5	x: 0 m η = 1.6	x: 1.024 m η = 5.7	x: 0.341 m η = 0.5	x: 1.024 m η = 0.1	x: 0 m η = 1.4	x: 1.024 m η = 6.3	x: 0 m η < 0.1	x: 1.024 m η = 0.4	x: 1.024 m η = 8.9	x: 1.024 m η = 11.6	x: 1.024 m η = 11.3	CUMPLE η = 11.6
N519/N543	$w/t \le (w/t)_{Max}$ Cumple	x: 1.013 m η = 6.8	x: 1.013 m η = 0.8	x: 0.338 m η = 1.1	x: 1.013 m η = 0.6	x: 1.013 m η = 3.9	x: 0.169 m η = 0.3	x: 0 m η = 0.1	x: 0.844 m η = 0.8	x: 1.013 m η = 4.4	x: 0.844 m η < 0.1	x: 1.013 m η = 0.2	N.P.[1]	x: 1.013 m η = 4.9	x: 1.013 m η = 8.9	CUMPLE η = 8.9
N518/N543	$w/t \le (w/t)_{Max}$ Cumple	x: 0.167 m η = 0.4	x: 0 m η = 12.5	x: 0.167 m η = 1.2	x: 0 m η = 1.9	x: 1.003 m η = 2.0	x: 0.502 m η = 0.1	x: 1.003 m η = 0.2	x: 0 m η = 1.3	x: 1.003 m η = 2.5	x: 0 m η < 0.1	x: 1.003 m η = 0.1	N.P.[1]	x: 0 m η = 14.6	x: 0 m η = 14.9	CUMPLE η = 14.9
N518/N544	$w/t \le (w/t)_{Max}$ Cumple	x: 1.011 m η = 10.6	N.P.[2]	x: 0.337 m η = 1.1	x: 1.011 m η = 1.1	x: 1.011 m η = 2.3	x: 0.169 m η = 0.2	x: 0 m η = 0.1	x: 0 m η = 1.1	x: 1.011 m η = 2.7	x: 1.011 m η < 0.1	x: 1.011 m η = 0.1	N.P.[1]	N.P.[3]	x: 1.011 m η = 12.1	CUMPLE η = 12.1
N517/N544	$w/t \le (w/t)_{Max}$ Cumple	N.P.[4]	x: 0 m η = 16.6	η < 0.1	x: 0 m η = 2.2	x: 1.012 m η = 3.6	x: 0.169 m η = 0.2	x: 1.012 m η = 0.2	x: 1.012 m η = 1.0	x: 1.012 m η = 3.8	x: 0 m η < 0.1	x: 1.012 m η = 0.1	N.P.[1]	x: 0 m η = 19.2	x: 0 m η = 19.4	CUMPLE η = 19.4
N517/N545	$w/t \le (w/t)_{Max}$ Cumple	x: 0.999 m η = 12.6	N.P.[2]	η = 0.3	x: 0 m η = 1.3	x: 0.999 m η = 7.6	η = 0.7	x: 0 m η = 0.2	x: 0 m η = 1.1	x: 0.999 m η = 7.7	x: 0 m η < 0.1	x: 0.999 m η = 0.6	x: 0.999 m η = 17.1	N.P.[3]	x: 0.999 m η = 15.8	CUMPLE η = 17.1

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N516/N545	$w / t \leq (w / t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 21.0	x: 0.497 m η = 0.2	x: 0 m η = 2.3	x: 0 m η = 7.8	x: 0.745 m η = 0.7	x: 0.993 m η = 0.2	x: 0 m η = 1.2	x: 0 m η = 7.9	x: 0 m η = 0.1	x: 0 m η = 0.6	N.P.[1]	x: 0 m η = 23.7	x: 0 m η = 23.9	CUMPLE η = 23.9
N516/N548	$w / t \leq (w / t)_{Máx}$ Cumple	x: 0.968 m η = 15.1	x: 0.242 m η = 0.4	x: 0 m η = 0.8	x: 0 m η = 2.1	x: 0.968 m η = 2.4	x: 0 m η = 0.1	x: 0 m η = 0.2	x: 0 m η = 1.6	x: 0.968 m η = 2.8	x: 0 m η < 0.1	x: 0.968 m η = 0.1	N.P.[1]	x: 0.968 m η = 3.6	x: 0 m η = 17.7	CUMPLE η = 17.7
N515/N546	$w / t \leq (w / t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 25.8	η = 0.6	x: 0.941 m η = 2.0	x: 0.941 m η = 4.1	x: 0.235 m η = 0.2	x: 0.941 m η = 0.2	x: 0.941 m η = 1.4	x: 0.941 m η = 4.4	x: 0.941 m η < 0.1	x: 0.941 m η = 0.2	N.P.[1]	x: 0.941 m η = 28.2	x: 0.941 m η = 28.2	CUMPLE η = 28.2
N515/N547	$w / t \leq (w / t)_{Máx}$ Cumple	x: 0.971 m η = 17.9	N.P.[2]	x: 0.243 m η = 0.1	x: 0 m η = 2.4	x: 0 m η = 4.4	x: 0.728 m η = 0.4	x: 0 m η = 0.3	x: 0 m η = 1.5	x: 0 m η = 4.4	x: 0 m η = 0.1	x: 0 m η = 0.2	N.P.[1]	N.P.[3]	x: 0 m η = 20.8	CUMPLE η = 20.8
N514/N547	$w / t \leq (w / t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 29.3	η = 0.3	x: 0 m η = 5.4	x: 0.947 m η = 5.0	x: 0.237 m η = 0.4	x: 0.947 m η = 0.6	x: 0 m η = 2.5	x: 0.947 m η = 5.2	x: 0 m η = 0.3	x: 0.947 m η = 0.3	N.P.[1]	x: 0 m η = 35.5	x: 0 m η = 36.1	CUMPLE η = 36.1
N514/N548	$w / t \leq (w / t)_{Máx}$ Cumple	x: 0.981 m η = 16.2	N.P.[2]	η = 0.2	x: 0 m η = 4.0	x: 0.981 m η = 4.2	x: 0 m η = 0.2	x: 0 m η = 0.2	x: 0 m η = 2.1	x: 0.981 m η = 4.3	x: 0 m η = 0.2	x: 0.981 m η = 0.2	N.P.[1]	N.P.[3]	x: 0 m η = 21.1	CUMPLE η = 21.1
N502/N548	$w / t \leq (w / t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 29.2	x: 0.603 m η = 2.3	x: 0 m η = 3.5	x: 0 m η = 11.5	x: 0.402 m η = 0.9	x: 0.804 m η = 0.4	x: 0 m η = 3.7	x: 0 m η = 12.5	x: 0 m η = 0.1	x: 0 m η = 1.6	N.P.[1]	x: 0.804 m η = 32.9	x: 0.804 m η = 33.0	CUMPLE η = 33.0
N484/N549	$w / t \leq (w / t)_{Máx}$ Cumple	x: 1.026 m η = 3.9	x: 0 m η = 3.1	x: 0.855 m η = 1.1	x: 0.171 m η = 0.7	x: 0 m η = 3.1	x: 0.855 m η = 0.2	x: 1.026 m η = 0.1	x: 0.171 m η = 0.7	x: 0 m η = 3.5	x: 0.171 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 4.4	x: 0 m η = 5.5	CUMPLE η = 5.5
N483/N549	$w / t \leq (w / t)_{Máx}$ Cumple	x: 1.007 m η = 2.4	x: 0 m η = 5.5	x: 0.839 m η = 0.6	x: 0 m η = 1.3	x: 0 m η = 3.6	x: 0.839 m η = 0.3	x: 1.007 m η = 0.1	x: 0 m η = 1.4	x: 0 m η = 3.9	x: 0 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 1.007 m η = 7.7	x: 1.007 m η = 7.6	CUMPLE η = 7.7
N483/N550	$w / t \leq (w / t)_{Máx}$ Cumple	x: 1.034 m η = 5.3	x: 0 m η = 1.5	x: 1.034 m η = 0.8	x: 0.689 m η = 0.5	x: 1.034 m η = 3.8	x: 0.172 m η = 0.3	x: 0 m η = 0.1	x: 0.689 m η = 0.6	x: 1.034 m η = 4.2	x: 0.689 m η < 0.1	x: 1.034 m η = 0.2	N.P.[1]	x: 0 m η = 2.7	x: 1.034 m η = 7.0	CUMPLE η = 7.0
N540/N549	$w / t \leq (w / t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 30.6	x: 1.12 m η = 1.8	x: 0.373 m η = 1.8	x: 0 m η = 4.3	x: 0 m η = 0.7	x: 1.12 m η = 0.1	x: 0.373 m η = 1.6	x: 0 m η = 5.1	x: 0.373 m η < 0.1	x: 0 m η = 0.3	N.P.[1]	x: 0.187 m η = 32.8	x: 0.373 m η = 32.9	CUMPLE η = 32.9
N550/N549	$w / t \leq (w / t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 28.8	η = 0.5	x: 1.122 m η = 2.1	x: 1.122 m η = 6.7	η = 1.1	x: 0 m η = 0.2	x: 1.122 m η = 2.2	x: 1.122 m η = 6.9	x: 1.122 m η < 0.1	x: 1.122 m η = 0.5	N.P.[1]	x: 1.122 m η = 31.4	x: 1.122 m η = 31.4	CUMPLE η = 31.4
N482/N550	$w / t \leq (w / t)_{Máx}$ Cumple	x: 1.024 m η = 1.9	x: 0 m η = 6.4	x: 0.341 m η = 0.1	x: 0 m η = 1.6	x: 1.024 m η = 3.9	η = 0.2	x: 1.024 m η = 0.1	x: 1.024 m η = 0.8	x: 1.024 m η = 3.9	x: 0 m η < 0.1	x: 1.024 m η = 0.2	N.P.[1]	x: 1.024 m η = 8.3	x: 0 m η = 8.4	CUMPLE η = 8.4
N551/N550	$w / t \leq (w / t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 25.9	η = 0.6	x: 1.131 m η = 1.7	x: 0 m η = 3.9	η = 0.3	x: 0 m η = 0.1	x: 1.131 m η = 1.8	x: 0 m η = 4.1	x: 1.131 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 1.131 m η = 27.9	x: 1.131 m η = 28.0	CUMPLE η = 28.0
N482/N551	$w / t \leq (w / t)_{Máx}$ Cumple	x: 1.013 m η = 6.7	x: 0 m η = 0.7	x: 0 m η = 0.3	x: 1.013 m η = 0.7	x: 1.013 m η = 4.1	x: 0.169 m η = 0.3	x: 0 m η = 0.1	x: 0 m η = 0.6	x: 1.013 m η = 4.2	x: 1.013 m η < 0.1	x: 1.013 m η = 0.2	N.P.[1]	x: 1.013 m η = 1.8	x: 1.013 m η = 8.3	CUMPLE η = 8.3
N481/N551	$w / t \leq (w / t)_{Máx}$ Cumple	x: 0.167 m η = 0.5	x: 0 m η = 12.4	η = 0.1	x: 0 m η = 1.9	x: 1.003 m η = 6.0	η = 0.4	x: 1.003 m η = 0.2	x: 1.003 m η = 0.9	x: 1.003 m η = 6.0	x: 0 m η < 0.1	x: 1.003 m η = 0.4	N.P.[1]	x: 0 m η = 14.4	x: 0 m η = 14.7	CUMPLE η = 14.7
N481/N552	$w / t \leq (w / t)_{Máx}$ Cumple	x: 1.011 m η = 10.6	N.P.[2]	η = 0.2	x: 1.011 m η = 1.1	x: 1.011 m η = 2.8	η = 0.2	x: 0 m η = 0.1	x: 0 m η = 0.9	x: 1.011 m η = 2.9	x: 1.011 m η < 0.1	x: 1.011 m η = 0.1	N.P.[1]	N.P.[3]	x: 1.011 m η = 12.0	CUMPLE η = 12.0
N552/N551	$w / t \leq (w / t)_{Máx}$ Cumple	x: 1.128 m η = 1.1	x: 0 m η = 21.0	η = 0.7	x: 1.128 m η = 2.2	x: 1.128 m η = 4.5	η = 0.4	x: 0 m η = 0.2	x: 1.128 m η = 1.2	x: 1.128 m η = 4.8	x: 1.128 m η = 0.1	x: 1.128 m η = 0.2	N.P.[1]	x: 1.128 m η = 23.5	x: 1.128 m η = 23.8	CUMPLE η = 23.8
N480/N552	$w / t \leq (w / t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 16.6	x: 0.337 m η = 0.8	x: 0 m η = 2.2	x: 1.012 m η = 1.7	x: 0.337 m η = 0.1	x: 1.012 m η = 0.2	x: 0 m η = 1.2	x: 1.012 m η = 2.0	x: 0 m η < 0.1	x: 1.012 m η < 0.1	N.P.[1]	x: 0 m η = 18.9	x: 0 m η = 19.3	CUMPLE η = 19.3
N553/N552	$w / t \leq (w / t)_{Máx}$ Cumple	x: 0.948 m η = 3.7	x: 0 m η = 14.0	x: 0 m η = 0.5	x: 1.138 m η = 1.7	x: 0 m η = 12.2	η = 1.8	x: 0 m η = 0.3	x: 1.138 m η = 1.7	x: 0 m η = 12.4	x: 1.138 m η < 0.1	x: 0 m η = 1.6	x: 0 m η = 7.6	x: 0 m η = 18.0	x: 0 m η = 20.6	CUMPLE η = 20.6
N480/N553	$w / t \leq (w / t)_{Máx}$ Cumple	x: 0.999 m η = 12.6	N.P.[2]	x: 0.5 m η = 0.4	x: 0 m η = 1.3	x: 0 m η = 7.3	η = 0.7	x: 0 m η = 0.2	x: 0 m η = 1.1	x: 0 m η = 7.5	x: 0 m η < 0.1	x: 0 m η = 0.6	x: 0 m η = 16.6	N.P.[3]	x: 0 m η = 15.1	CUMPLE η = 16.6
N479/N553	$w / t \leq (w / t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 20.9	x: 0.248 m η = 0.3	x: 0 m η = 2.3	x: 0 m η = 7.5	x: 0.745 m η = 0.7	x: 0.993 m η = 0.2	x: 0.993 m η = 1.1	x: 0 m η = 7.6	x: 0 m η = 0.1	x: 0 m η = 0.6	N.P.[1]	x: 0 m η = 23.6	x: 0 m η = 23.7	CUMPLE η = 23.7
N479/N554	$w / t \leq (w / t)_{Máx}$ Cumple	x: 0.968 m η = 15.1	N.P.[2]	x: 0 m η = 0.5	x: 0 m η = 2.1	x: 0.968 m η = 4.7	x: 0 m η = 0.3	x: 0 m η = 0.2	x: 0 m η = 1.3	x: 0.968 m η = 4.9	x: 0 m η < 0.1	x: 0.968 m η = 0.2	N.P.[1]	N.P.[3]	x: 0 m η = 17.7	CUMPLE η = 17.7
N554/N553	$w / t \leq (w / t)_{Máx}$ Cumple	x: 1.148 m η = 6.6	x: 0 m η = 10.8	x: 0.383 m η = 2.4	x: 1.148 m η = 1.8	x: 1.148 m η = 9.3	x: 0.383 m η = 1.2	x: 0 m η = 0.4	x: 1.148 m η = 1.9	x: 1.148 m η = 10.3	x: 1.148 m η < 0.1	x: 1.148 m η = 1.1	x: 1.148 m η = 14.3	x: 1.148 m η = 14.8	x: 1.148 m η = 14.5	CUMPLE η = 14.8
N478/N554	$w / t \leq (w / t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 25.6	x: 0 m η = 1.0	x: 0.941 m η = 1.9	x: 0.941 m η = 1.8	η = 0.1	x: 0.941 m η = 0.2	x: 0.941 m η = 1.3	x: 0.941 m η = 2.2	x: 0.941 m η < 0.1	x: 0.941 m η = 0.1	N.P.[1]	x: 0.941 m η = 27.8	x: 0.941 m η = 28.0	CUMPLE η = 28.0
N555/N554	$w / t \leq (w / t)_{Máx}$ Cumple	x: 1.129 m η = 10.4	x: 0 m η = 8.5	x: 0.753 m η = 1.1	x: 0 m η = 1.4	x: 0 m η = 3.3	η = 0.3	x: 0 m η = 0.3	x: 0 m η = 1.5	x: 0 m η = 3.7	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 8.9	x: 1.129 m η = 9.6	x: 0 m η = 11.6	CUMPLE η = 11.6
N478/N555	$w / t \leq (w / t)_{Máx}$ Cumple	x: 0.971 m η = 17.8	N.P.[2]	x: 0 m η = 0.1	x: 0 m η = 2.4	x: 0 m η = 4.3	x: 0.971 m η = 0.4	x: 0 m η = 0.3	x: 0 m η = 1.3	x: 0 m η = 4.3	x: 0 m η = 0.1	x: 0 m η = 0.2	N.P.[1]	N.P.[3]	x: 0 m η = 20.8	CUMPLE η = 20.8
N477/N555	$w / t \leq (w / t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 29.3	η = 0.3	x: 0 m η = 5.4	x: 0.947 m η = 4.8	x: 0.237 m η = 0.4	x: 0.947 m η = 0.6	x: 0 m η = 2.4	x: 0.947 m η = 4.9	x: 0 m η = 0.3	x: 0.947 m η = 0.2	N.P.[1]	x: 0 m η = 35.4	x: 0 m η = 36.0	CUMPLE η = 36.0
N556/N555	$w / t \leq (w / t)_{Máx}$ Cumple	x: 1.12 m η = 16.3	x: 0 m η = 5.6	η = 0.2	x: 0 m η = 9.3	x: 1.12 m η = 4.4	x: 0 m η = 0.5	x: 0 m η = 1.1	x: 0 m η = 9.3	x: 1.12 m η = 4.5	x: 0 m η = 0.9	x: 1.12 m η = 0.2	x: 0 m η = 28.5	x: 1.12 m η = 6.4	x: 0 m η = 27.9	CUMPLE η = 28.5
N477/N556	$w / t \leq (w / t)_{Máx}$ Cumple	x: 0.981 m η = 16.2	N.P.[2]	η = 0.3	x: 0 m η = 4.0	x: 0.981 m η = 1.6	x: 0.245 m η = 0.1	x: 0 m η = 0.2	x: 0 m η = 2.0	x: 0.981 m η = 1.7	x: 0 m η = 0.2	x: 0.981 m η < 0.1	N.P.[1]	N.P.[3]	x: 0 m η = 21.2	CUMPLE η = 21.2
N464/N556	$w / t \leq (w / t)_{Máx}$ Cumple	N.P.[4]	x: 0 m η = 29.5	η = 2.3	x: 0 m η = 3.4	x: 0 m η = 13.3	x: 0.603 m η = 1.3	x: 0.804 m η = 0.4	x: 0 m η = 3.4	x: 0 m η = 14.2	x: 0 m η = 0.1	x: 0 m η = 2.0	N.P.[1]	x: 0.804 m η = 32.9	x: 0.804 m η = 33.2	CUMPLE η = 33.2
N463/N556	$w / t \leq (w / t)_{Máx}$ Cumple	x: 0.902 m η = 21.5	x: 0 m η = 3.7	x: 0.677 m η = 6.7	x: 0.902 m η = 8.3	x: 0 m η = 16.7	x: 0.226 m η = 2.6	x: 0.902 m η = 1.6	x: 0.902 m η = 8.4	x: 0 m η = 19.7	x: 0.902 m η = 0.7	x: 0 m η = 3.9	x: 0 m η = 37.9	x: 0 m η = 7.6	x: 0.902 m η = 31.9	CUMPLE η = 37.9
N541/N549	$w / t \leq (w / t)_{Máx}$ Cumple	η = 1.5	η = 2.2	η = 0.3	x: 0.3 m η = 11.7	x: 0 m η = 15.9	x: 0.3 m η = 5.2	x: 0 m η = 1.2	x: 0.3 m η = 11.8	x: 0 m η = 15.9	x: 0.3 m η = 1.4	x: 0 m η = 2.8	x: 0.3 m η = 33.5	x: 0.3 m η = 29.1	x: 0.3 m η = 26.0	CUMPLE η = 33.5
N542/N550	$w / t \leq (w / t)_{Máx}$ Cumple	η = 4.0	η = 4.5	η = 0.2	x: 0.3 m η = 10.9	x: 0 m η = 20.6	η = 6.6	x: 0 m η = 0.4	x: 0.3 m η = 11.0	x: 0 m η = 20.6	x: 0.3 m η = 1.2	x: 0 m η = 4.7	x: 0 m η = 42.2	x: 0 m η = 35.3	x: 0 m η = 33.1	CUMPLE η = 42.2
N543/N551	$w / t \leq (w / t)_{Máx}$ Cumple	x: 0 m η = 3.2	x: 0 m η = 3.4	η = 0.1	x: 0 m η = 12.7	x: 0.3 m η = 4.3	x: 0 m η = 1.0	x: 0 m η = 1.4	x: 0 m η = 12.7	x: 0.3 m η = 4.3	x: 0 m η = 1.6	x: 0.3 m η = 0.2	x: 0 m η = 20.9	x: 0 m η = 17.6	x: 0 m η = 19.4	CUMPLE η = 20.9
N544/N552	$w / t \leq (w / t)_{Máx}$ Cumple	η = 2.2	η = 2.5	η < 0.1	x: 0 m η = 14.5	x: 0.3 m η = 29.0	η = 9.3	x: 0 m η = 3.0	x: 0 m η = 14.5	x: 0.3 m η = 29.1	x: 0 m η = 2.2	x: 0.3 m η = 9.3	x: 0 m η = 53.8	x: 0 m η = 43.5	x: 0 m η = 40.1	CUMPLE η = 53.8
N545/N553	$w / t \leq (w / t)_{Máx}$ Cumple	η = 1.7	η = 2.2	η = 0.2	x: 0.3 m η = 5.7	x: 0.3 m η = 12.9	x: 0.15 m η = 4.2	x: 0 m η = 1.7	x: 0.3 m η = 5.8	x: 0.3 m η = 13.0	x: 0.3 m η = 0.4	x: 0.3 m η = 1.9	x: 0.3 m η = 25.2	x: 0.3 m η = 20.2	x: 0.3 m η = 19.3	CUMPLE η = 25.2
N546/N554	$w / t \leq (w / t)_{Máx}$ Cumple	x: 0.3 m η = 1.4	x: 0.3 m η = 1.5	η = 0.6	x: 0 m η = 5.5	x: 0.3 m η = 14.4	x: 0.3 m η = 4.6	x: 0 m η = 1.2	x: 0 m η = 5.7	x: 0.3 m η = 14.6	x: 0 m η = 0.3	x: 0.3 m η = 2.4	x: 0 m η = 24.9	x: 0 m η = 20.1	x: 0.3 m η = 19.4	CUMPLE η = 24.9

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N547/N555	$w/t \leq (w/t)_{Máx}$ Cumple	$\eta = 0.4$	$\eta = 0.6$	x: 0.15 m $\eta = 0.6$	x: 0.3 m $\eta = 6.6$	x: 0 m $\eta = 3.5$	x: 0.15 m $\eta = 1.1$	x: 0 m $\eta = 2.1$	x: 0.3 m $\eta = 6.9$	x: 0 m $\eta = 3.8$	x: 0.3 m $\eta = 0.5$	x: 0 m $\eta = 0.2$	x: 0.3 m $\eta = 13.2$	x: 0.3 m $\eta = 10.2$	x: 0.3 m $\eta = 9.5$	CUMPLE $\eta = 13.2$
N548/N556	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.3 m $\eta = 1.8$	x: 0.3 m $\eta = 1.9$	$\eta = 0.2$	x: 0 m $\eta = 4.4$	x: 0 m $\eta = 31.4$	x: 0.3 m $\eta = 10.2$	x: 0.3 m $\eta = 1.0$	x: 0 m $\eta = 4.4$	x: 0 m $\eta = 31.5$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 10.9$	x: 0 m $\eta = 45.8$	x: 0 m $\eta = 37.4$	x: 0 m $\eta = 41.2$	CUMPLE $\eta = 45.8$
N560/N566	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.61 m $\eta = 1.4$	x: 0 m $\eta = 3.2$	x: 0 m $\eta = 1.1$	x: 0.61 m $\eta = 33.7$	x: 0.61 m $\eta = 9.0$	$\eta = 2.6$	x: 0 m $\eta = 7.2$	x: 0.61 m $\eta = 34.1$	x: 0.61 m $\eta = 9.2$	x: 0.61 m $\eta = 12.1$	x: 0.61 m $\eta = 0.9$	x: 0.61 m $\eta = 38.6$	x: 0.61 m $\eta = 38.7$	x: 0.61 m $\eta = 45.0$	CUMPLE $\eta = 45.0$
N568/N562	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.463 m $\eta = 2.3$	x: 0 m $\eta = 5.7$	$\eta = 6.5$	x: 0.463 m $\eta = 60.4$	x: 0.463 m $\eta = 10.8$	x: 0.231 m $\eta = 1.6$	x: 0.463 m $\eta = 21.0$	x: 0.463 m $\eta = 60.5$	x: 0.463 m $\eta = 13.6$	x: 0.463 m $\eta = 41.0$	x: 0.463 m $\eta = 1.9$	x: 0.463 m $\eta = 66.4$	x: 0.463 m $\eta = 66.5$	x: 0.463 m $\eta = 80.6$	CUMPLE $\eta = 80.6$
N557/N565	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.378 m $\eta = 14.3$	x: 0.378 m $\eta = 34.6$	x: 0.378 m $\eta = 4.7$	x: 0.755 m $\eta = 10.6$	x: 0 m $\eta = 20.4$	$\eta = 1.9$	x: 0 m $\eta = 1.1$	x: 0.755 m $\eta = 12.6$	x: 0 m $\eta = 22.4$	x: 0.755 m $\eta = 1.6$	x: 0 m $\eta = 5.1$	N.P.[1]	x: 0 m $\eta = 42.9$	x: 0 m $\eta = 39.2$	CUMPLE $\eta = 42.9$
N565/N558	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.424 m $\eta = 17.7$	x: 0.424 m $\eta = 12.3$	x: 0.847 m $\eta = 1.2$	x: 0 m $\eta = 7.5$	x: 0 m $\eta = 56.2$	x: 0.424 m $\eta = 6.5$	x: 0 m $\eta = 0.7$	x: 0 m $\eta = 7.5$	x: 0 m $\eta = 56.7$	x: 0 m $\eta = 0.6$	x: 0 m $\eta = 32.6$	x: 0 m $\eta = 85.5$	x: 0 m $\eta = 59.7$	x: 0 m $\eta = 80.6$	CUMPLE $\eta = 85.5$
N558/N564	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.869 m $\eta = 6.2$	x: 0 m $\eta = 15.3$	x: 0.217 m $\eta = 1.8$	x: 0.869 m $\eta = 2.4$	x: 0 m $\eta = 8.7$	x: 0.217 m $\eta = 0.7$	x: 0 m $\eta = 0.3$	x: 0.869 m $\eta = 3.1$	x: 0 m $\eta = 9.5$	x: 0.869 m $\eta = 0.1$	x: 0 m $\eta = 0.9$	N.P.[1]	x: 0 m $\eta = 18.1$	x: 0.869 m $\eta = 18.3$	CUMPLE $\eta = 18.3$
N564/N559	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.983 m $\eta = 9.9$	x: 0 m $\eta = 7.3$	$\eta = 0.5$	x: 0.983 m $\eta = 2.5$	x: 0 m $\eta = 27.2$	$\eta = 2.7$	x: 0.983 m $\eta = 0.3$	x: 0.983 m $\eta = 2.5$	x: 0 m $\eta = 27.4$	x: 0.983 m $\eta = 0.1$	x: 0 m $\eta = 7.6$	x: 0 m $\eta = 40.0$	x: 0 m $\eta = 11.2$	x: 0 m $\eta = 38.3$	CUMPLE $\eta = 40.0$
N559/N563	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.028 m $\eta = 3.9$	x: 0 m $\eta = 10.0$	x: 0.343 m $\eta = 0.5$	x: 0 m $\eta = 4.1$	x: 0 m $\eta = 2.7$	x: 0.685 m $\eta = 0.1$	x: 0 m $\eta = 0.4$	x: 0 m $\eta = 3.2$	x: 0 m $\eta = 2.9$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 0.1$	N.P.[1]	x: 0 m $\eta = 13.4$	x: 0 m $\eta = 13.9$	CUMPLE $\eta = 13.9$
N563/N560	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.371 m $\eta = 6.2$	x: 0.371 m $\eta = 5.9$	x: 0.557 m $\eta = 4.8$	x: 1.114 m $\eta = 8.6$	x: 1.114 m $\eta = 27.8$	x: 0.371 m $\eta = 2.1$	x: 0 m $\eta = 0.6$	x: 1.114 m $\eta = 7.5$	x: 1.114 m $\eta = 29.9$	x: 1.114 m $\eta = 0.7$	x: 1.114 m $\eta = 9.0$	x: 1.114 m $\eta = 46.8$	x: 1.114 m $\eta = 41.3$	x: 1.114 m $\eta = 40.6$	CUMPLE $\eta = 46.8$
N566/N561	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.819 m $\eta = 4.8$	x: 0 m $\eta = 20.8$	x: 0.819 m $\eta = 1.0$	x: 0 m $\eta = 17.6$	x: 0 m $\eta = 17.5$	x: 0.819 m $\eta = 1.5$	x: 0.819 m $\eta = 1.6$	x: 0 m $\eta = 17.7$	x: 0 m $\eta = 17.8$	x: 0 m $\eta = 3.2$	x: 0 m $\eta = 3.2$	x: 0 m $\eta = 24.8$	x: 0 m $\eta = 45.1$	x: 0 m $\eta = 42.8$	CUMPLE $\eta = 45.1$
N571/N567	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.41 m $\eta = 20.6$	x: 1.41 m $\eta = 32.3$	$\eta = 2.0$	x: 0 m $\eta = 1.7$	x: 1.41 m $\eta = 16.2$	$\eta = 1.5$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 2.6$	x: 1.41 m $\eta = 17.1$	x: 0 m $\eta = 0.1$	x: 1.41 m $\eta = 3.0$	x: 1.41 m $\eta = 43.9$	x: 1.41 m $\eta = 51.9$	x: 1.41 m $\eta = 52.2$	CUMPLE $\eta = 52.2$
N567/N568	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.7 m $\eta = 12.3$	x: 0.7 m $\eta = 14.6$	$\eta = 0.5$	x: 1.4 m $\eta = 1.1$	x: 0 m $\eta = 37.4$	$\eta = 4.6$	x: 1.4 m $\eta = 0.2$	x: 0 m $\eta = 0.9$	x: 0 m $\eta = 37.7$	x: 1.4 m $\eta < 0.1$	x: 0 m $\eta = 14.4$	x: 0 m $\eta = 60.4$	x: 0 m $\eta = 52.2$	x: 0 m $\eta = 61.0$	CUMPLE $\eta = 61.0$
N568/N569	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.225 m $\eta = 5.9$	x: 0.225 m $\eta = 3.1$	$\eta = 1.1$	x: 1.35 m $\eta = 10.8$	x: 1.35 m $\eta = 52.8$	x: 1.35 m $\eta = 6.2$	x: 0 m $\eta = 1.0$	x: 1.35 m $\eta = 11.0$	x: 1.35 m $\eta = 53.3$	x: 1.35 m $\eta = 1.2$	x: 1.35 m $\eta = 28.8$	x: 1.35 m $\eta = 76.5$	x: 1.35 m $\eta = 58.0$	x: 1.35 m $\eta = 69.4$	CUMPLE $\eta = 76.5$
N569/N570	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.79 m $\eta = 10.8$	x: 0.79 m $\eta = 5.3$	x: 0.592 m $\eta = 6.2$	x: 0 m $\eta = 1.2$	x: 0 m $\eta = 45.4$	$\eta = 8.8$	x: 0 m $\eta = 0.2$	x: 0.79 m $\eta = 3.5$	x: 0 m $\eta = 48.1$	x: 0.79 m $\eta = 0.1$	x: 0 m $\eta = 23.9$	x: 0 m $\eta = 70.7$	x: 0 m $\eta = 52.1$	x: 0 m $\eta = 63.4$	CUMPLE $\eta = 70.7$
N571/N575	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.755 m $\eta = 20.0$	x: 0.566 m $\eta = 41.8$	x: 0.378 m $\eta = 4.7$	x: 0.755 m $\eta = 10.2$	x: 0 m $\eta = 21.0$	x: 0.378 m $\eta = 2.0$	x: 0.755 m $\eta = 1.0$	x: 0.755 m $\eta = 12.2$	x: 0 m $\eta = 23.0$	x: 0.755 m $\eta = 1.5$	x: 0 m $\eta = 5.3$	x: 0 m $\eta = 15.5$	x: 0.755 m $\eta = 49.4$	x: 0.755 m $\eta = 48.1$	CUMPLE $\eta = 49.4$
N575/N567	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.424 m $\eta = 21.1$	x: 0.424 m $\eta = 16.6$	$\eta = 1.1$	x: 0 m $\eta = 8.6$	x: 0 m $\eta = 56.3$	$\eta = 6.5$	x: 0 m $\eta = 0.8$	x: 0 m $\eta = 8.6$	x: 0 m $\eta = 56.8$	x: 0 m $\eta = 0.8$	x: 0 m $\eta = 32.7$	x: 0 m $\eta = 87.8$	x: 0 m $\eta = 62.2$	x: 0 m $\eta = 82.8$	CUMPLE $\eta = 87.8$
N567/N574	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.869 m $\eta = 8.3$	x: 0 m $\eta = 18.2$	x: 0.652 m $\eta = 1.8$	x: 0.869 m $\eta = 3.2$	x: 0 m $\eta = 7.7$	$\eta = 0.6$	x: 0 m $\eta = 0.3$	x: 0.869 m $\eta = 3.2$	x: 0 m $\eta = 8.5$	x: 0.869 m $\eta = 0.1$	x: 0 m $\eta = 0.7$	N.P.[1]	x: 0.869 m $\eta = 21.7$	x: 0.869 m $\eta = 22.1$	CUMPLE $\eta = 22.1$
N574/N568	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.983 m $\eta = 11.5$	x: 0 m $\eta = 9.6$	$\eta = 0.5$	x: 0 m $\eta = 3.0$	x: 0 m $\eta = 27.9$	$\eta = 2.8$	x: 0.983 m $\eta = 0.3$	x: 0 m $\eta = 3.0$	x: 0 m $\eta = 28.1$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 8.0$	x: 0 m $\eta = 40.7$	x: 0 m $\eta = 12.7$	x: 0 m $\eta = 38.3$	CUMPLE $\eta = 40.7$
N568/N573	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.856 m $\eta = 5.2$	x: 0.856 m $\eta = 11.8$	x: 0.343 m $\eta = 0.5$	x: 0 m $\eta = 2.7$	x: 0 m $\eta = 3.0$	x: 0.343 m $\eta = 0.2$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 2.6$	x: 0 m $\eta = 3.2$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 0.1$	N.P.[1]	x: 0 m $\eta = 14.7$	x: 0 m $\eta = 14.9$	CUMPLE $\eta = 14.9$
N573/N569	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.114 m $\eta = 7.1$	x: 0 m $\eta = 6.2$	x: 0.557 m $\eta = 4.7$	x: 1.114 m $\eta = 7.8$	x: 1.114 m $\eta = 27.6$	x: 0.557 m $\eta = 2.1$	x: 0 m $\eta = 0.6$	x: 1.114 m $\eta = 7.2$	x: 1.114 m $\eta = 29.6$	x: 1.114 m $\eta = 0.6$	x: 1.114 m $\eta = 8.8$	x: 1.114 m $\eta = 46.2$	x: 1.114 m $\eta = 38.9$	x: 1.114 m $\eta = 40.1$	CUMPLE $\eta = 46.2$
N569/N576	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.8 m $\eta = 1.4$	x: 0 m $\eta = 3.3$	$\eta = 0.8$	x: 0.8 m $\eta = 30.3$	x: 0.8 m $\eta = 10.2$	x: 0 m $\eta = 2.0$	x: 0 m $\eta = 4.9$	x: 0.8 m $\eta = 30.7$	x: 0.8 m $\eta = 10.4$	x: 0.8 m $\eta = 9.8$	x: 0.8 m $\eta = 1.1$	x: 0.8 m $\eta = 36.5$	x: 0.8 m $\eta = 35.8$	x: 0.8 m $\eta = 40.8$	CUMPLE $\eta = 40.8$
N576/N572	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.273 m $\eta = 3.8$	x: 0 m $\eta = 7.6$	x: 0 m $\eta = 7.6$	x: 0.273 m $\eta = 55.6$	x: 0.273 m $\eta = 10.7$	x: 0 m $\eta = 1.5$	x: 0.273 m $\eta = 32.9$	x: 0.273 m $\eta = 55.6$	x: 0.273 m $\eta = 14.0$	x: 0.273 m $\eta = 41.8$	x: 0.273 m $\eta = 2.0$	x: 0.273 m $\eta = 30.7$	x: 0.273 m $\eta = 61.2$	x: 0.273 m $\eta = 75.0$	CUMPLE $\eta = 75.0$
N576/N570	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.686 m $\eta = 9.2$	x: 0.686 m $\eta = 30.6$	x: 0.915 m $\eta = 2.4$	x: 0 m $\eta = 17.5$	x: 0 m $\eta = 13.6$	x: 0.915 m $\eta = 1.0$	x: 0.915 m $\eta = 1.4$	x: 0 m $\eta = 15.1$	x: 0 m $\eta = 14.7$	x: 0 m $\eta = 3.1$	x: 0 m $\eta = 2.2$	x: 0 m $\eta = 21.5$	x: 0 m $\eta = 50.0$	x: 0 m $\eta = 50.0$	CUMPLE $\eta = 50.0$
N562/N577	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.617 m $\eta = 2.3$	x: 0 m $\eta = 11.7$	$\eta = 6.6$	x: 0 m $\eta = 66.4$	x: 0 m $\eta = 5.7$	x: 0.309 m $\eta = 1.0$	x: 0 m $\eta = 14.7$	x: 0 m $\eta = 67.7$	x: 0 m $\eta = 8.6$	x: 0 m $\eta = 48.0$	x: 0 m $\eta = 0.7$	x: 0 m $\eta = 8.3$	x: 0 m $\eta = 83.6$	x: 0 m $\eta = 94.7$	CUMPLE $\eta = 94.7$
N577/N578	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.081 m $\eta = 3.9$	x: 0 m $\eta = 9.7$	x: 0.721 m $\eta = 2.8$	x: 0 m $\eta = 20.7$	x: 0 m $\eta = 4.7$	x: 1.081 m $\eta = 0.8$	x: 1.081 m $\eta = 2.4$	x: 0 m $\eta = 21.8$	x: 0 m $\eta = 5.9$	x: 0 m $\eta = 4.8$	x: 0 m $\eta = 0.4$	x: 0 m $\eta = 8.8$	x: 0 m $\eta = 34.6$	x: 0 m $\eta = 34.8$	CUMPLE $\eta = 34.8$
N578/N579	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.907 m $\eta = 5.0$	x: 0.907 m $\eta = 7.3$	$\eta = 2.3$	x: 0 m $\eta = 5.0$	x: 1.088 m $\eta = 3.4$	$\eta = 0.5$	x: 0 m $\eta = 0.7$	x: 0 m $\eta = 5.8$	x: 1.088 m $\eta = 4.2$	x: 0 m $\eta = 0.3$	x: 1.088 m $\eta = 0.2$	x: 0 m $\eta = 10.8$	x: 0 m $\eta = 12.5$	x: 0 m $\eta = 12.3$	CUMPLE $\eta = 12.5$
N579/N580	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.18 m $\eta = 5.5$	x: 0.18 m $\eta = 5.3$	$\eta = 1.4$	x: 0.18 m $\eta = 1.1$	x: 1.08 m $\eta = 3.1$	$\eta = 0.4$	x: 1.08 m $\eta = 0.1$	x: 0.18 m $\eta = 1.7$	x: 1.08 m $\eta = 3.7$	x: 0.18 m $\eta < 0.1$	x: 1.08 m $\eta = 0.1$	x: 0 m $\eta = 9.1$	x: 1.08 m $\eta = 6.7$	x: 0 m $\eta = 7.3$	CUMPLE $\eta = 9.1$
N580/N581	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.085 m $\eta = 5.9$	x: 1.085 m $\eta = 3.6$	$\eta = 1.1$	x: 1.085 m $\eta = 1.3$	x: 1.085 m $\eta = 4.0$	$\eta = 0.6$	x: 0 m $\eta = 0.2$	x: 1.085 m $\eta = 1.8$	x: 1.085 m $\eta = 4.1$	x: 1.085 m $\eta < 0.1$	x: 1.085 m $\eta = 0.2$	x: 1.085 m $\eta = 10.4$	x: 1.085 m $\eta = 4.9$	x: 1.085 m $\eta = 9.5$	CUMPLE $\eta = 10.4$
N581/N582	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.082 m $\eta = 6.2$	x: 1.082 m $\eta = 2.1$	$\eta = 0.8$	x: 0.902 m $\eta = 1.2$	x: 1.082 m $\eta = 2.2$	$\eta = 0.2$	x: 0 m $\eta = 0.1$	x: 0.902 m $\eta = 1.6$	x: 1.082 m $\eta = 2.6$	x: 0.902 m $\eta < 0.1$	x: 1.082 m $\eta = 0.1$	x: 1.082 m $\eta = 11.4$	x: 0 m $\eta = 2.8$	x: 1.082 m $\eta = 9.4$	CUMPLE $\eta = 11.4$
N582/N583	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.085 m $\eta = 7.3$	x: 0.181 m $\eta = 1.6$	$\eta = 1.3$	x: 0.723 m $\eta = 1.2$	x: 1.085 m $\eta = 1.8$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 0.1$	x: 0.723 m $\eta = 1.4$	x: 1.085 m $\eta = 2.2$	x: 0.723 m $\eta < 0.1$	x: 1.085 m $\eta < 0.1$	x: 1.085 m $\eta = 11.6$	x: 1.085 m $\eta = 3.0$	x: 1.085 m $\eta = 10.0$	CUMPLE $\eta = 11.6$
N583/N584	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.081 m $\eta = 8.3$	x: 0 m $\eta = 1.9$	x: 1.081 m $\eta = 1.1$	x: 0.901 m $\eta = 1.4$	x: 0 m $\eta = 1.4$	x: 1.081 m $\eta = 0.2$	x: 0 m $\eta = 0.1$	x: 0.901 m $\eta = 1.5$	x: 0 m $\eta = 1.5$	x: 0.901 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	x: 1.081 m $\eta = 11.8$	x: 1.081 m $\eta = 3.6$	x: 1.081 m $\eta = 10.5$	CUMPLE $\eta = 11.8$
N585/N584	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.08 m $\eta = 8.6$	x: 0.36 m $\eta = 1.8$	$\eta = 0.3$	x: 0.54 m $\eta = 1.4$	x: 1.08 m $\eta = 2.5$	x: 0.18 m $\eta = 0.3$	x: 0 m $\eta = 0.1$	x: 0.54 m $\eta = 1.4$	x: 1.08 m $\eta = 2.5$	x: 0.54 m $\eta < 0.1$	x: 1.08 m $\eta = 0.1$	x: 0.9 m $\eta = 11.7$	x: 1.08 m $\eta = 4.2$	x: 0.9 m $\eta = 10.7$	CUMPLE $\eta = 11.7$
N586/N585	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.084 m $\eta = 8.0$	x: 1.084 m $\eta = 0.8$	x: 0.903 m $\eta = 0.7$	x: 0.722 m $\eta = 1.3$	x: 0 m $\eta = 2.5$	x: 0.903 m $\eta = 0.3$	x: 0 m $\eta = 0.1$	x: 0.722 m $\eta = 1.5$	x: 0 m $\eta = 2.8$	x: 0.722 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	x: 1.084 m $\eta = 12.1$	x: 0 m $\eta = 3.7$	x: 1.084 m $\eta = 10.6$	CUMPLE $\eta = 12.1$
N587/N586	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.08 m $\eta = 6.8$	x: 0 m $\eta = 0.5$	$\eta = 0.8$	x: 0.9 m $\eta = 1.3$	x: 1.08 m $\eta = 3.1$	$\eta = 0.2$	x: 0 m $\eta = 0.1$	x: 0.9 m $\eta = 1.6$	x: 1.08 m $\eta = 3.3$	x: 0.9 m $\eta < 0.1$	x: 1.08 m $\eta = 0.1$	x: 1.08 m $\eta = 11.9$	x: 1.08 m $\eta = 2.5$	x: 1.08 m $\eta = 9.9$	CUMPLE $\eta = 11.9$
N588/N587	$w/t \leq (w/t)_{Máx}$ Cumple	x: 1.083 m $\eta = 4.7$	x: 1.083 m $\eta = 1.6$	$\eta = 1.1$	x: 1.083 m $\eta = 1.3$	x: 1.083 m $\eta = 4.3$	$\eta = 0.6$	x: 0 m $\eta = 0.1$	x: 1.083 m $\eta = 1.8$	x: 1.083 m $\eta = 4.3$	x: 1.083 m $\eta < 0.1$	x: 1.083 m $\eta = 0.2$	x: 1.083 m $\eta = 10.8$	x: 1.083 m $\eta = 4.6$	x: 1.083 m $\eta = 9.7$	CUMPLE $\eta = 10.8$
N589/N588	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.906 m $\eta = 4.7$	x: 0.906 m $\eta = 4.1$	$\eta = 1.5$	x: 0.724 m $\eta = 0.9$	x: 0 m $\eta = 3.1$	x: 0.362 m $\eta = 0.4$	x: 0 m $\eta = 0.1$	x: 0.724 m $\eta = 1.6$	x: 0 m $\eta = 3.8$	x: 0.724 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 9.3$	x: 0 m $\eta = 5.5$	x: 0 m $\eta = 7.2$	CUMPLE $\eta = 9.3$
N590/N589	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.181 m $\eta = 4.8$	x: 0.181 m $\eta = 7.1$	x: 0.904 m $\eta = 2.6$	x: 0 m $\eta = 3.6$	x: 1.085 m $\eta = 3.4$	$\eta = 0.5$	x: 0 m $\eta = 0.5$	x: 0 m $\eta = 4.4$	x: 1.085 m $\eta = 4.3$	x: 0 m $\eta = 0.2$	x: 1.085 m $\eta = 0.2$	x: 1.085 m $\eta = 8.3$	x: 0 m $\eta = 11.2$	x: 0 m $\eta = 11.4$	CUMPLE $\eta = 11.4$



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (ABN 2100-18 (2018))															Estado
	w / t	T	P	Tr	M_x	M_y	V_z	V_y	M_xTr	M_yTr	M_xV_y	M_yV_z	MT	MP	TPTrMV	
N591/N590	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 1.077 m η = 4.9	x: 0 m η = 10.7	x: 1.077 m η = 3.0	x: 0 m η = 13.5	x: 1.077 m η = 5.1	x: 0 m η = 0.8	x: 1.077 m η = 1.6	x: 0 m η = 14.5	x: 1.077 m η = 6.4	x: 0 m η = 2.1	x: 1.077 m η = 0.4	x: 0 m η = 10.2	x: 0 m η = 26.8	x: 0 m η = 25.5	CUMPLE η = 26.8
N572/N591	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.801 m η = 4.6	x: 0 m η = 13.2	x: 0.401 m η = 5.9	x: 0 m η = 51.1	x: 0 m η = 7.2	x: 0.601 m η = 1.2	x: 0 m η = 8.4	x: 0 m η = 52.3	x: 0 m η = 9.7	x: 0 m η = 28.1	x: 0 m η = 1.0	x: 0 m η = 20.2	x: 0 m η = 70.0	x: 0 m η = 76.9	CUMPLE η = 76.9
N593/N592	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 1.128 m η = 1.2	x: 0 m η = 14.1	η = 1.4	x: 1.128 m η = 1.8	x: 0 m η = 13.5	η = 2.0	x: 0 m η = 0.3	x: 1.128 m η = 2.3	x: 0 m η = 13.8	x: 1.128 m η = 0.1	x: 0 m η = 1.9	x: 0 m η = 4.4	x: 0 m η = 20.4	x: 0 m η = 22.8	CUMPLE η = 22.8
N594/N593	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.751 m η = 3.1	x: 0 m η = 9.5	η = 1.6	x: 1.126 m η = 1.5	x: 1.126 m η = 11.6	x: 0.939 m η = 1.7	x: 0 m η = 0.3	x: 1.126 m η = 2.1	x: 1.126 m η = 11.7	x: 1.126 m η < 0.1	x: 1.126 m η = 1.4	x: 1.126 m η = 14.7	x: 1.126 m η = 18.6	x: 1.126 m η = 19.6	CUMPLE η = 19.6
N595/N594	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 1.126 m η = 6.1	x: 0 m η = 8.4	x: 0.188 m η = 2.0	x: 0 m η = 1.8	x: 0 m η = 2.9	x: 0.188 m η = 0.1	x: 0 m η = 0.3	x: 0 m η = 2.6	x: 0 m η = 3.8	x: 0 m η = 0.1	x: 0 m η = 0.1	x: 0 m η = 9.3	x: 1.126 m η = 10.1	x: 1.126 m η = 9.4	CUMPLE η = 10.1
N596/N595	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 1.12 m η = 10.5	x: 0 m η = 7.9	η = 1.8	x: 0 m η = 4.2	x: 1.12 m η = 4.0	x: 0 m η = 0.4	x: 0 m η = 0.6	x: 0 m η = 5.0	x: 1.12 m η = 4.6	x: 0 m η = 0.3	x: 1.12 m η = 0.2	x: 0 m η = 16.2	x: 0 m η = 9.3	x: 0 m η = 14.7	CUMPLE η = 16.2
N570/N596	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.396 m η = 11.9	x: 0.396 m η = 6.2	η = 2.4	x: 1.187 m η = 3.7	x: 0 m η = 12.8	x: 0.791 m η = 1.7	x: 1.187 m η = 0.5	x: 1.187 m η = 4.0	x: 0 m η = 13.6	x: 1.187 m η = 0.2	x: 0 m η = 1.9	x: 0 m η = 28.5	x: 0 m η = 18.4	x: 0 m η = 25.3	CUMPLE η = 28.5
N587/N592	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.934 m η = 5.9	x: 0.701 m η = 1.3	η < 0.1	x: 0 m η = 0.8	x: 0.934 m η = 8.1	x: 0.467 m η = 0.7	x: 0 m η = 0.1	x: 0 m η = 0.8	x: 0.934 m η = 8.1	x: 0 m η < 0.1	x: 0.934 m η = 0.7	x: 0.934 m η = 14.0	x: 0.934 m η = 2.6	x: 0.934 m η = 13.5	CUMPLE η = 14.0
N588/N592	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.168 m η = 1.0	x: 0 m η = 11.8	η = 1.3	x: 0 m η = 1.2	x: 1.006 m η = 5.8	η = 0.5	x: 1.006 m η = 0.1	x: 0 m η = 1.3	x: 1.006 m η = 6.4	x: 0 m η < 0.1	x: 1.006 m η = 0.4	N.P.(1)	x: 1.006 m η = 14.5	x: 1.006 m η = 14.4	CUMPLE η = 14.5
N588/N593	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.94 m η = 8.0	x: 0.705 m η = 0.5	x: 0.47 m η = 0.9	x: 0 m η = 0.9	x: 0 m η = 6.8	x: 0.235 m η = 0.7	x: 0 m η = 0.1	x: 0 m η = 1.2	x: 0 m η = 7.2	x: 0 m η < 0.1	x: 0 m η = 0.5	x: 0 m η = 14.5	x: 0 m η = 7.8	x: 0 m η = 12.6	CUMPLE η = 14.5
N589/N593	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.845 m η = 1.3	x: 0 m η = 15.2	x: 0.507 m η = 0.7	x: 0 m η = 1.9	x: 0 m η = 5.6	x: 0.676 m η = 0.5	x: 1.014 m η = 0.2	x: 0 m η = 2.0	x: 0 m η = 5.9	x: 0 m η < 0.1	x: 0 m η = 0.4	x: 0 m η = 9.0	x: 1.014 m η = 18.9	x: 1.014 m η = 18.2	CUMPLE η = 18.9
N589/N594	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.935 m η = 9.1	x: 0.234 m η = 1.6	x: 0.468 m η = 1.6	x: 0 m η = 1.8	x: 0.935 m η = 5.1	x: 0.234 m η = 0.5	x: 0 m η = 0.2	x: 0 m η = 2.1	x: 0.935 m η = 5.8	x: 0 m η < 0.1	x: 0.935 m η = 0.3	N.P.(1)	x: 0.935 m η = 8.3	x: 0.935 m η = 13.4	CUMPLE η = 13.4
N590/N594	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.677 m η = 1.3	x: 0 m η = 17.8	x: 0.677 m η = 0.2	x: 0 m η = 1.1	x: 1.015 m η = 10.0	x: 0.169 m η = 0.7	x: 0 m η = 0.1	x: 0 m η = 1.2	x: 1.015 m η = 10.0	x: 0 m η < 0.1	x: 1.015 m η = 1.0	x: 1.015 m η = 12.3	x: 1.015 m η = 22.7	x: 1.015 m η = 24.8	CUMPLE η = 24.8
N590/N595	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.932 m η = 12.0	x: 0.466 m η = 0.5	x: 0.466 m η = 0.9	x: 0 m η = 0.6	x: 0.932 m η = 9.5	x: 0.466 m η = 0.9	x: 0.932 m η = 0.1	x: 0.932 m η = 0.8	x: 0.932 m η = 9.9	x: 0.932 m η < 0.1	x: 0.932 m η = 1.0	x: 0.932 m η = 20.9	x: 0.932 m η = 11.1	x: 0.932 m η = 19.7	CUMPLE η = 20.9
N591/N595	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.678 m η = 0.6	x: 0 m η = 23.5	x: 0.678 m η = 1.1	x: 0 m η = 11.1	x: 1.017 m η = 10.6	x: 0.169 m η = 0.7	x: 1.017 m η = 0.9	x: 0 m η = 8.8	x: 1.017 m η = 11.1	x: 0 m η = 1.2	x: 1.017 m η = 1.2	x: 1.017 m η = 13.4	x: 0 m η = 36.1	x: 0 m η = 37.4	CUMPLE η = 37.4
N591/N596	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.932 m η = 5.6	N.P.(2)	x: 0.233 m η = 0.7	x: 0 m η = 12.8	x: 0.932 m η = 7.3	x: 0.233 m η = 0.6	x: 0 m η = 1.0	x: 0 m η = 12.9	x: 0.932 m η = 7.7	x: 0 m η = 1.7	x: 0.932 m η = 0.6	x: 0 m η = 24.3	N.P.(3)	x: 0 m η = 21.8	CUMPLE η = 24.3
N576/N596	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 1.02 m η = 0.7	x: 0 m η = 17.5	η = 3.4	x: 0 m η = 19.1	x: 1.02 m η = 2.7	η = 0.1	x: 0 m η = 1.4	x: 0 m η = 19.2	x: 1.02 m η = 4.2	x: 0 m η = 3.7	x: 1.02 m η = 0.2	N.P.(1)	x: 0 m η = 38.9	x: 0 m η = 41.4	CUMPLE η = 41.4
N599/N602	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.458 m η = 2.3	x: 0.458 m η = 3.7	x: 0.153 m η = 2.1	x: 0.61 m η = 29.6	x: 0.61 m η = 8.4	x: 0.458 m η = 2.4	x: 0 m η = 6.2	x: 0.61 m η = 29.9	x: 0.61 m η = 9.1	x: 0.61 m η = 9.3	x: 0.61 m η = 0.9	x: 0.61 m η = 23.6	x: 0.61 m η = 33.1	x: 0.61 m η = 38.5	CUMPLE η = 38.5
N602/N603	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.463 m η = 3.2	x: 0 m η = 6.2	η = 6.0	x: 0.463 m η = 53.3	x: 0.463 m η = 10.9	η = 1.7	x: 0.463 m η = 18.5	x: 0.463 m η = 53.4	x: 0.463 m η = 13.5	x: 0.463 m η = 31.9	x: 0.463 m η = 1.9	x: 0.463 m η = 38.2	x: 0.463 m η = 58.4	x: 0.463 m η = 70.8	CUMPLE η = 70.8
N597/N604	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0 m η = 6.6	x: 0 m η = 16.3	η = 1.7	x: 0.869 m η = 3.0	x: 0 m η = 8.6	η = 0.7	x: 0 m η = 0.4	x: 0.869 m η = 3.7	x: 0 m η = 9.3	x: 0.869 m η = 0.1	x: 0 m η = 0.9	x: 0 m η = 16.1	x: 0 m η = 22.4	x: 0 m η = 20.8	CUMPLE η = 22.4
N604/N598	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.983 m η = 10.3	x: 0 m η = 7.5	η = 0.4	x: 0.983 m η = 2.6	x: 0 m η = 27.5	x: 0.492 m η = 2.8	x: 0.983 m η = 0.3	x: 0.983 m η = 2.6	x: 0 m η = 27.7	x: 0.983 m η = 0.1	x: 0 m η = 7.8	x: 0 m η = 42.1	x: 0 m η = 31.9	x: 0 m η = 41.1	CUMPLE η = 42.1
N598/N605	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.685 m η = 4.3	x: 0.685 m η = 10.5	x: 0.343 m η = 0.5	x: 0 m η = 3.6	x: 0 m η = 3.0	η = 0.2	x: 0 m η = 0.3	x: 0 m η = 3.1	x: 0 m η = 3.2	x: 0 m η = 0.1	x: 0 m η = 0.1	N.P.(1)	x: 0 m η = 14.5	x: 0 m η = 14.2	CUMPLE η = 14.5
N605/N599	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.743 m η = 6.5	x: 0.743 m η = 6.9	x: 0.743 m η = 4.5	x: 1.114 m η = 7.7	x: 1.114 m η = 25.6	x: 0.743 m η = 2.0	x: 0 m η = 0.5	x: 1.114 m η = 5.8	x: 1.114 m η = 27.5	x: 1.114 m η = 0.6	x: 1.114 m η = 7.6	x: 1.114 m η = 47.1	x: 1.114 m η = 37.3	x: 1.114 m η = 38.3	CUMPLE η = 47.1
N602/N600	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.819 m η = 4.7	x: 0 m η = 22.6	x: 0.819 m η = 0.9	x: 0 m η = 16.1	x: 0 m η = 17.9	x: 0.819 m η = 1.5	x: 0.819 m η = 1.5	x: 0 m η = 16.2	x: 0 m η = 18.3	x: 0 m η = 2.6	x: 0 m η = 3.4	N.P.(1)	x: 0 m η = 40.8	x: 0 m η = 42.6	CUMPLE η = 42.8
N610/N606	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 1.234 m η = 25.2	x: 1.234 m η = 37.5	x: 1.234 m η = 2.0	x: 0 m η = 1.8	x: 1.41 m η = 16.2	x: 1.234 m η = 1.5	x: 0 m η = 0.1	x: 0 m η = 2.7	x: 1.41 m η = 17.1	x: 0 m η = 0.1	x: 1.41 m η = 2.9	x: 1.41 m η = 46.9	x: 1.41 m η = 56.4	x: 1.41 m η = 56.6	CUMPLE η = 56.6
N606/N607	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.467 m η = 14.0	x: 0.467 m η = 16.0	x: 0.467 m η = 0.5	x: 0 m η = 1.0	x: 0 m η = 37.6	x: 0.467 m η = 4.7	x: 1.4 m η = 0.1	x: 1.4 m η = 1.0	x: 0 m η = 37.9	x: 0 m η < 0.1	x: 0 m η = 14.6	x: 0 m η = 61.6	x: 0 m η = 55.8	x: 0 m η = 62.8	CUMPLE η = 62.8
N607/N608	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.225 m η = 7.3	x: 0.225 m η = 4.0	η = 1.0	x: 1.35 m η = 9.6	x: 1.35 m η = 49.7	x: 0.9 m η = 5.9	x: 0 m η = 0.8	x: 1.35 m η = 9.8	x: 1.35 m η = 50.1	x: 1.35 m η = 1.0	x: 1.35 m η = 25.4	x: 1.35 m η = 75.1	x: 1.35 m η = 50.7	x: 1.35 m η = 66.7	CUMPLE η = 75.1
N608/N609	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.79 m η = 12.6	x: 0.79 m η = 6.7	x: 0.395 m η = 6.4	x: 0.79 m η = 0.6	x: 0 m η = 50.1	x: 0.592 m η = 9.7	x: 0 m η = 0.1	x: 0.79 m η = 3.4	x: 0 m η = 52.9	x: 0.79 m η = 0.1	x: 0 m η = 29.0	x: 0 m η = 78.3	x: 0 m η = 58.6	x: 0 m η = 71.3	CUMPLE η = 78.3
N614/N606	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.847 m η = 21.4	x: 0.424 m η = 16.9	η = 1.1	x: 0 m η = 8.6	x: 0 m η = 56.3	η = 6.5	x: 0 m η = 0.8	x: 0 m η = 8.7	x: 0 m η = 56.8	x: 0 m η = 0.8	x: 0 m η = 32.6	x: 0 m η = 81.5	x: 0 m η = 24.2	x: 0 m η = 75.8	CUMPLE η = 81.5
N606/N613	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0 m η = 8.6	x: 0 m η = 18.7	η = 1.8	x: 0.869 m η = 3.1	x: 0 m η = 7.7	x: 0.652 m η = 0.6	x: 0 m η = 0.4	x: 0.869 m η = 3.9	x: 0 m η = 8.4	x: 0.869 m η = 0.1	x: 0 m η = 0.7	x: 0 m η = 14.4	x: 0.869 m η = 22.2	x: 0.869 m η = 22.5	CUMPLE η = 22.5
N613/N607	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.983 m η = 11.8	x: 0 m η = 10.0	η = 0.4	x: 0 m η = 3.0	x: 0 m η = 28.1	η = 2.8	x: 0.983 m η = 0.3	x: 0 m η = 3.0	x: 0 m η = 28.2	x: 0 m η = 0.1	x: 0 m η = 8.1	x: 0 m η = 42.7	x: 0 m η = 33.1	x: 0 m η = 42.0	CUMPLE η = 42.7
N607/N612	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 1.028 m η = 5.7	x: 1.028 m η = 12.1	x: 0.343 m η = 0.5	x: 0 m η = 2.4	x: 0 m η = 3.3	x: 0.343 m η = 0.2	x: 0 m η = 0.2	x: 0 m η = 2.4	x: 0 m η = 3.5	x: 0 m η = 0.1	x: 0 m η = 0.1	N.P.(1)	x: 0 m η = 15.1	x: 0 m η = 15.1	CUMPLE η = 15.1
N612/N608	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.371 m η = 7.4	x: 0.371 m η = 7.5	x: 0.743 m η = 4.5	x: 1.114 m η = 6.9	x: 1.114 m η = 25.4	x: 0.743 m η = 2.0	x: 0 m η = 0.5	x: 1.114 m η = 5.8	x: 1.114 m η = 27.3	x: 1.114 m η = 0.5	x: 1.114 m η = 7.5	x: 1.114 m η = 47.0	x: 1.114 m η = 36.8	x: 1.114 m η = 38.3	CUMPLE η = 47.0
N608/N615	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0 m η = 2.3	x: 0 m η = 3.7	x: 0 m η = 1.1	x: 0.8 m η = 26.0	x: 0.8 m η = 9.5	x: 0 m η = 1.9	x: 0 m η = 4.2	x: 0.8 m η = 26.3	x: 0.8 m η = 9.8	x: 0.8 m η = 7.1	x: 0.8 m η = 1.0	x: 0.8 m η = 22.6	x: 0.8 m η = 29.9	x: 0.8 m η = 34.1	CUMPLE η = 34.1
N615/N611	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.273 m η = 2.8	x: 0 m η = 6.1	η = 7.1	x: 0.273 m η = 47.9	x: 0.273 m η = 10.7	η = 1.6	x: 0.273 m η = 28.3	x: 0.273 m η = 47.9	x: 0.273 m η = 13.8	x: 0.273 m η = 30.9	x: 0.273 m η = 1.9	x: 0.273 m η = 37.2	x: 0.273 m η = 52.7	x: 0.273 m η = 64.6	CUMPLE η = 64.6
N615/N609	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.915 m η = 4.3	x: 0 m η = 29.0	x: 0.915 m η = 2.4	x: 0 m η = 15.4	x: 0 m η = 13.9	x: 0.915 m η = 1.0	x: 0.915 m η = 1.3	x: 0 m η = 13.3	x: 0 m η = 14.9	x: 0 m η = 2.4	x: 0 m η = 2.2	N.P.(1)	x: 0 m η = 46.6	x: 0 m η = 48.3	CUMPLE η = 48.3
N603/N616	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.617 m η = 3.8	x: 0 m η = 9.8	x: 0.617 m η = 6.7	x: 0 m η = 58.2	x: 0 m η = 5.8	x: 0.463 m η = 1.0	x: 0 m η = 12.8	x: 0 m η = 59.5	x: 0 m η = 8.8	x: 0 m η = 37.1	x: 0 m η = 0.8	x: 0 m η = 28.4	x: 0 m η = 72.1	x: 0 m η = 81.2	CUMPLE η = 81.2
N616/N617	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.721 m η = 5.2	x: 0.721 m η = 9.6	x: 0.721 m η = 2.8	x: 0 m η = 18.5	x: 0 m η = 4.8	x: 1.081 m η = 0.8	x: 1.081 m η = 2.2	x: 0 m η = 19.5	x: 0 m η = 6.0	x: 0 m η = 3.8	x: 0 m η = 0.4	x: 0 m η = 10.8	x: 0 m η = 29.0	x: 0 m η = 28.7	CUMPLE η = 29.0

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N617/N618	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.088 m η = 6.2	x: 0 m η = 6.9	η = 2.3	x: 0 m η = 4.4	x: 1.088 m η = 3.4	η = 0.5	x: 0 m η = 0.6	x: 0 m η = 5.3	x: 1.088 m η = 4.2	x: 0 m η = 0.3	x: 1.088 m η = 0.2	x: 0 m η = 11.1	x: 0 m η = 12.0	x: 0 m η = 11.8	CUMPLE η = 12.0
N618/N619	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 6.9	x: 0 m η = 4.8	η = 1.4	x: 0 m η = 1.0	x: 1.08 m η = 3.1	η = 0.5	x: 1.08 m η = 0.1	x: 0 m η = 1.6	x: 1.08 m η = 3.7	x: 0 m η < 0.1	x: 1.08 m η = 0.1	x: 1.08 m η = 10.7	x: 1.08 m η = 6.3	x: 1.08 m η = 8.7	CUMPLE η = 10.7
N619/N620	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.085 m η = 8.2	x: 1.085 m η = 3.2	η = 1.1	x: 1.085 m η = 1.0	x: 1.085 m η = 4.1	η = 0.6	x: 0 m η = 0.1	x: 1.085 m η = 1.5	x: 1.085 m η = 4.3	x: 1.085 m η < 0.1	x: 1.085 m η = 0.2	x: 1.085 m η = 14.1	x: 0 m η = 4.1	x: 1.085 m η = 11.8	CUMPLE η = 14.1
N620/N621	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.082 m η = 10.8	x: 0 m η = 1.9	η = 0.8	x: 0.721 m η = 1.1	x: 1.082 m η = 2.2	η = 0.2	x: 0 m η = 0.1	x: 0.721 m η = 1.4	x: 1.082 m η = 2.6	x: 0.721 m η < 0.1	x: 1.082 m η = 0.1	x: 1.082 m η = 15.7	x: 0 m η = 2.7	x: 1.082 m η = 13.8	CUMPLE η = 15.7
N621/N622	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.085 m η = 12.3	x: 0.362 m η = 0.8	x: 0 m η = 1.3	x: 0.723 m η = 1.1	x: 1.085 m η = 1.8	x: 0 m η = 0.2	x: 0 m η = 0.1	x: 0.723 m η = 1.4	x: 1.085 m η = 2.2	x: 0.723 m η < 0.1	x: 1.085 m η < 0.1	x: 1.085 m η = 16.4	x: 1.085 m η = 2.3	x: 1.085 m η = 14.9	CUMPLE η = 16.4
N622/N623	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.081 m η = 13.3	x: 0 m η = 0.1	η = 1.1	x: 0.72 m η = 1.3	x: 0 m η = 1.4	x: 1.081 m η = 0.2	x: 0 m η = 0.1	x: 0.72 m η = 1.4	x: 1.081 m η = 1.5	x: 0.72 m η < 0.1	x: 0 m η < 0.1	x: 1.081 m η = 16.6	x: 1.081 m η = 2.1	x: 1.081 m η = 15.4	CUMPLE η = 16.6
N624/N623	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.08 m η = 13.5	N.P.(2)	η = 0.2	x: 0.72 m η = 1.3	x: 1.08 m η = 2.4	η = 0.3	x: 0 m η = 0.1	x: 0.72 m η = 1.3	x: 1.08 m η = 2.4	x: 0.54 m η < 0.1	x: 1.08 m η = 0.1	x: 1.08 m η = 16.5	N.P.(3)	x: 1.08 m η = 15.6	CUMPLE η = 16.5
N625/N624	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.084 m η = 12.7	x: 1.084 m η = 0.6	x: 0.722 m η = 0.6	x: 0.722 m η = 1.2	x: 0 m η = 2.6	x: 0 m η = 0.3	x: 0 m η = 0.1	x: 0.722 m η = 1.4	x: 0 m η = 2.8	x: 0.722 m η < 0.1	x: 0 m η = 0.1	x: 1.084 m η = 16.7	x: 0 m η = 3.4	x: 1.084 m η = 15.3	CUMPLE η = 16.7
N626/N625	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.08 m η = 11.2	x: 0.54 m η = 0.8	η = 0.8	x: 0.72 m η = 1.2	x: 1.08 m η = 3.1	η = 0.2	x: 0 m η = 0.1	x: 0.72 m η = 1.5	x: 1.08 m η = 3.3	x: 0.72 m η < 0.1	x: 1.08 m η = 0.1	x: 1.08 m η = 16.1	x: 1.08 m η = 2.8	x: 1.08 m η = 14.2	CUMPLE η = 16.1
N627/N626	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.083 m η = 8.6	x: 0 m η = 0.4	η = 1.1	x: 1.083 m η = 1.1	x: 1.083 m η = 4.4	η = 0.6	x: 0 m η = 0.1	x: 1.083 m η = 1.6	x: 1.083 m η = 4.5	x: 1.083 m η < 0.1	x: 1.083 m η = 0.2	x: 1.083 m η = 14.5	x: 1.083 m η = 3.8	x: 1.083 m η = 12.1	CUMPLE η = 14.5
N628/N627	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.087 m η = 5.1	x: 0 m η = 1.9	η = 1.5	x: 0.543 m η = 0.8	x: 0 m η = 3.0	x: 1.087 m η = 0.4	x: 0 m η = 0.1	x: 0.543 m η = 1.4	x: 1.087 m η = 3.7	x: 0.543 m η < 0.1	x: 1.087 m η = 0.1	x: 1.087 m η = 11.2	x: 1.087 m η = 2.7	x: 1.087 m η = 8.9	CUMPLE η = 11.2
N629/N628	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.085 m η = 4.3	x: 0 m η = 4.6	x: 1.085 m η = 2.6	x: 0 m η = 3.3	x: 1.085 m η = 3.4	η = 0.5	x: 0 m η = 0.4	x: 0 m η = 3.9	x: 1.085 m η = 4.3	x: 0 m η = 0.2	x: 1.085 m η = 0.2	x: 0 m η = 9.4	x: 0 m η = 8.5	x: 0 m η = 8.7	CUMPLE η = 9.4
N630/N629	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.718 m η = 4.2	x: 0 m η = 8.3	x: 0.539 m η = 3.1	x: 0 m η = 11.8	x: 1.077 m η = 5.2	x: 0 m η = 0.9	x: 1.077 m η = 1.4	x: 0 m η = 12.8	x: 1.077 m η = 6.6	x: 0 m η = 1.7	x: 1.077 m η = 0.4	x: 0 m η = 9.3	x: 0 m η = 21.7	x: 0 m η = 20.9	CUMPLE η = 21.7
N611/N630	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.801 m η = 4.1	x: 0 m η = 11.0	η = 6.3	x: 0 m η = 43.9	x: 0 m η = 7.2	x: 0.601 m η = 1.2	x: 0 m η = 7.2	x: 0 m η = 45.1	x: 0 m η = 9.9	x: 0 m η = 20.9	x: 0 m η = 1.0	x: 0 m η = 24.5	x: 0 m η = 59.5	x: 0 m η = 64.5	CUMPLE η = 64.5
N632/N631	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.128 m η = 2.8	x: 0 m η = 9.1	η = 1.2	x: 1.128 m η = 1.0	x: 0 m η = 13.5	η = 2.0	x: 0 m η = 0.1	x: 1.128 m η = 1.5	x: 0 m η = 13.8	x: 1.128 m η < 0.1	x: 0 m η = 2.0	x: 0 m η = 7.5	x: 0 m η = 18.0	x: 0 m η = 20.6	CUMPLE η = 20.6
N633/N632	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.126 m η = 5.7	x: 0 m η = 9.4	x: 0.563 m η = 2.5	x: 0 m η = 0.6	x: 1.126 m η = 11.5	x: 0.563 m η = 1.6	x: 0 m η = 0.1	x: 0.751 m η = 1.3	x: 1.126 m η = 12.2	x: 0.751 m η < 0.1	x: 1.126 m η = 1.5	x: 1.126 m η = 6.7	x: 1.126 m η = 15.0	x: 1.126 m η = 16.3	CUMPLE η = 16.3
N634/N633	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.126 m η = 9.0	x: 0 m η = 9.7	x: 1.126 m η = 2.1	x: 0 m η = 1.2	x: 0 m η = 2.7	η = 0.1	x: 0 m η = 0.2	x: 0 m η = 1.6	x: 0 m η = 3.6	x: 0 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 8.7	x: 0 m η = 11.0	x: 0 m η = 10.7	CUMPLE η = 11.0
N635/N634	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.12 m η = 13.7	x: 0 m η = 10.6	η = 1.9	x: 0 m η = 2.8	x: 1.12 m η = 3.7	x: 0 m η = 0.4	x: 0 m η = 0.3	x: 0 m η = 3.6	x: 1.12 m η = 4.1	x: 0 m η = 0.1	x: 1.12 m η = 0.2	x: 0 m η = 18.4	x: 0 m η = 12.3	x: 0 m η = 17.2	CUMPLE η = 18.4
N609/N635	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.187 m η = 16.2	x: 0.396 m η = 11.4	x: 0.791 m η = 4.3	x: 1.187 m η = 3.6	x: 0 m η = 12.5	x: 0.791 m η = 1.6	x: 1.187 m η = 0.5	x: 1.187 m η = 4.5	x: 0 m η = 14.4	x: 1.187 m η = 0.2	x: 0 m η = 2.1	x: 0 m η = 25.4	x: 1.187 m η = 13.8	x: 1.187 m η = 21.0	CUMPLE η = 25.4
N626/N631	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.934 m η = 5.6	x: 0.701 m η = 1.2	x: 0.234 m η = 1.0	x: 0 m η = 0.9	x: 0 m η = 1.7	x: 0.467 m η = 0.2	x: 0 m η = 0.1	x: 0.934 m η = 1.1	x: 0 m η = 2.1	x: 0.934 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0.934 m η = 3.4	x: 0 m η = 7.4	CUMPLE η = 7.4
N627/N631	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 1.4	x: 0 m η = 7.9	η = 0.2	x: 0 m η = 0.9	x: 1.006 m η = 2.0	η = 0.1	x: 1.006 m η = 0.1	x: 0 m η = 1.0	x: 1.006 m η = 2.1	x: 0 m η < 0.1	x: 1.006 m η < 0.1	N.P.(1)	x: 1.006 m η = 10.5	x: 1.006 m η = 10.5	CUMPLE η = 10.5
N627/N632	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.94 m η = 6.9	x: 0 m η = 0.6	η = 0.3	x: 0 m η = 1.0	x: 0.94 m η = 8.0	x: 0.235 m η = 0.8	x: 0 m η = 0.1	x: 0 m η = 1.0	x: 0.94 m η = 8.2	x: 0 m η < 0.1	x: 0.94 m η = 0.7	x: 0.94 m η = 15.6	x: 0 m η = 7.7	x: 0.94 m η = 14.6	CUMPLE η = 15.6
N628/N632	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.014 m η = 1.4	x: 0 m η = 10.1	η = 0.1	x: 0 m η = 1.4	x: 0 m η = 6.2	x: 0.676 m η = 0.6	x: 1.014 m η = 0.1	x: 0 m η = 1.5	x: 0 m η = 6.3	x: 0 m η < 0.1	x: 0 m η = 0.4	N.P.(1)	x: 1.014 m η = 13.6	x: 1.014 m η = 13.3	CUMPLE η = 13.6
N628/N633	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.935 m η = 7.4	x: 0 m η = 0.4	η = 0.6	x: 0 m η = 1.8	x: 0 m η = 2.5	η = 0.1	x: 0 m η = 0.2	x: 0 m η = 1.8	x: 0 m η = 2.7	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.(1)	x: 0 m η = 1.4	x: 0 m η = 10.5	CUMPLE η = 10.5
N629/N633	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.015 m η = 1.1	x: 0 m η = 11.8	x: 0.677 m η = 0.9	x: 0 m η = 1.2	x: 1.015 m η = 4.4	x: 1.015 m η = 0.3	x: 0 m η = 0.1	x: 0 m η = 1.2	x: 1.015 m η = 4.8	x: 0 m η < 0.1	x: 1.015 m η = 0.2	N.P.(1)	x: 1.015 m η = 14.6	x: 1.015 m η = 15.1	CUMPLE η = 15.1
N629/N634	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.932 m η = 9.3	x: 0.466 m η = 0.5	η = 0.2	x: 0.233 m η = 0.5	x: 0 m η = 5.3	x: 0.932 m η = 0.4	x: 0.932 m η = 0.1	x: 0.233 m η = 0.6	x: 0 m η = 5.3	x: 0.233 m η < 0.1	x: 0 m η = 0.3	N.P.(1)	x: 0 m η = 1.3	x: 0 m η = 11.9	CUMPLE η = 11.9
N630/N634	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.678 m η = 1.4	x: 0 m η = 15.7	η = 0.1	x: 0 m η = 9.4	x: 1.017 m η = 4.6	x: 0.169 m η = 0.3	x: 1.017 m η = 0.7	x: 0 m η = 7.8	x: 1.017 m η = 4.7	x: 0 m η = 0.9	x: 1.017 m η = 0.2	N.P.(1)	x: 0 m η = 26.1	x: 0 m η = 27.4	CUMPLE η = 27.4
N630/N635	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.932 m η = 3.0	x: 0 m η = 1.2	η = 0.3	x: 0 m η = 11.1	x: 0.932 m η = 1.9	η = 0.2	x: 0 m η = 0.9	x: 0 m η = 11.2	x: 0 m η = 2.0	x: 0 m η = 1.3	x: 0 m η < 0.1	x: 0 m η = 19.4	x: 0 m η = 3.7	x: 0 m η = 17.0	CUMPLE η = 19.4
N615/N635	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.68 m η = 1.4	x: 0 m η = 8.7	x: 0.68 m η = 2.6	x: 0 m η = 16.8	x: 1.02 m η = 3.0	x: 0.51 m η = 0.3	x: 0 m η = 1.2	x: 0 m η = 16.9	x: 1.02 m η = 4.1	x: 0 m η = 2.9	x: 1.02 m η = 0.2	N.P.(1)	x: 0 m η = 26.1	x: 0 m η = 29.8	CUMPLE η = 29.8
N610/N614	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.755 m η = 20.1	x: 0 m η = 41.8	η = 4.7	x: 0.755 m η = 10.2	x: 0 m η = 20.9	x: 0.189 m η = 2.0	x: 0.755 m η = 1.1	x: 0.755 m η = 12.2	x: 0 m η = 23.0	x: 0.755 m η = 1.5	x: 0 m η = 5.3	x: 0 m η = 13.6	x: 0.755 m η = 48.3	x: 0.755 m η = 47.5	CUMPLE η = 48.3
N636/N597	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.424 m η = 18.7	x: 0.424 m η = 12.8	x: 0.424 m η = 0.8	x: 0 m η = 7.9	x: 0 m η = 56.6	η = 6.5	x: 0 m η = 0.7	x: 0 m η = 7.9	x: 0 m η = 57.0	x: 0 m η = 0.6	x: 0 m η = 32.9	x: 0 m η = 81.3	x: 0 m η = 18.4	x: 0 m η = 76.6	CUMPLE η = 81.3
N601/N636	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.755 m η = 15.4	x: 0 m η = 36.8	x: 0.566 m η = 5.0	x: 0.755 m η = 10.5	x: 0 m η = 20.9	x: 0.566 m η = 2.0	x: 0.755 m η = 1.1	x: 0.755 m η = 12.6	x: 0 m η = 23.0	x: 0.755 m η = 1.6	x: 0 m η = 5.4	N.P.(1)	x: 0 m η = 45.3	x: 0.755 m η = 40.7	CUMPLE η = 45.3
N636/N565	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.4	η = 0.4	η = 3.9	x: 0 m η = 22.4	x: 0 m η = 5.3	x: 0.3 m η = 1.6	x: 0 m η = 50.1	x: 0 m η = 24.0	x: 0 m η = 6.9	x: 0 m η = 78.8	x: 0 m η = 0.5	x: 0 m η = 63.1	x: 0 m η = 31.2	x: 0 m η = 35.5	CUMPLE η = 35.5
N597/N558	$w/t \leq (w/t)_{Máx.}$ Cumple	η < 0.1	η < 0.1	η = 0.4	x: 0 m η = 24.6	x: 0 m η = 30.1	η = 12.4	x: 0 m η = 51.2	x: 0 m η = 24.7	x: 0 m η = 30.3	x: 0 m η = 81.7	x: 0 m η = 10.7	x: 0 m η = 93.7	x: 0 m η = 53.9	x: 0 m η = 56.2	CUMPLE η = 56.2
N604/N564	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.1	η = 0.2	η = 0.1	x: 0.3 m η = 59.3	x: 0.3 m η = 3.8	η = 1.6	x: 0 m η = 67.8	x: 0.3 m η = 59.3	x: 0.3 m η = 3.9	x: 0.3 m η = 99.8	x: 0.3 m η = 0.2	x: 0.3 m η = 24.0	x: 0.3 m η = 61.7	x: 0.3 m η = 96.9	CUMPLE η = 96.9
N598/N559	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.1	η = 0.1	η = 0.7	x: 0.3 m η = 51.3	x: 0 m η = 30.2	x: 0.15 m η = 12.8	x: 0 m η = 64.2	x: 0.3 m η = 51.6	x: 0 m η = 30.5	x: 0.3 m η = 71.0	x: 0 m η = 10.9	x: 0.3 m η = 26.2	x: 0.3 m η = 81.6	x: 0.3 m η = 71.6	CUMPLE η = 71.6
N605/N563	$w/t \leq (w/t)_{Máx.}$ Cumple	η < 0.1	η < 0.1	η = 1.2	x: 0.3 m η = 39.5	x: 0.3 m η = 14.4	η = 4.7	x: 0 m η = 46.7	x: 0.3 m η = 40.0	x: 0.3 m η = 14.9	x: 0.3 m η = 17.8	x: 0.3 m η = 2.5	x: 0.3 m η = 89.9	x: 0.3 m η = 52.8	x: 0.3 m η = 34.6	CUMPLE η = 34.6
N599/N560	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 10.5	η = 11.1	x: 0.15 m η = 1.4	x: 0.3 m η = 5.9	x: 0 m η = 25.0	x: 0 m η = 8.1	x: 0 m η = 1.8	x: 0.3 m η = 6.4	x: 0 m η = 25.5	x: 0.3 m η = 0.4	x: 0 m η = 7.2	x: 0.3 m η = 48.0	x: 0.3 m η = 35.0	x: 0 m η = 41.7	CUMPLE η = 48.0

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N603/N562	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta = 0.1$	$\eta = 0.1$	$\eta = 0.3$	x: 0 m $\eta = 37.2$	x: 0 m $\eta = 18.4$	$\eta = 6.2$	x: 0 m $\eta = 12.4$	x: 0 m $\eta = 37.3$	x: 0 m $\eta = 18.5$	x: 0 m $\eta = 15.4$	x: 0 m $\eta = 3.8$	x: 0 m $\eta = 49.3$	x: 0 m $\eta = 47.4$	x: 0 m $\eta = 46.7$	CUMPLE $\eta = 49.3$
N600/N561	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.3 m $\eta = 6.5$	x: 0.3 m $\eta = 7.1$	$\eta = 1.1$	x: 0.3 m $\eta = 70.4$	x: 0.3 m $\eta = 30.4$	x: 0.3 m $\eta = 10.2$	x: 0.15 m $\eta = 23.6$	x: 0.3 m $\eta = 70.7$	x: 0.3 m $\eta = 30.8$	x: 0.3 m $\eta = 55.5$	x: 0.3 m $\eta = 10.5$	x: 0 m $\eta = 32.8$	x: 0.3 m $\eta = 18.6$	x: 0.3 m $\eta = 16.0$	CUMPLE $\eta = 32.8$
N602/N566	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta = 0.3$	$\eta = 0.3$	x: 0.3 m $\eta = 0.4$	x: 0.3 m $\eta = 9.5$	x: 0 m $\eta = 24.0$	x: 0.15 m $\eta = 8.0$	x: 0 m $\eta = 3.2$	x: 0.3 m $\eta = 9.6$	x: 0 m $\eta = 24.2$	x: 0.3 m $\eta = 1.0$	x: 0 m $\eta = 6.5$	x: 0.3 m $\eta = 33.1$	x: 0 m $\eta = 22.5$	x: 0 m $\eta = 30.2$	CUMPLE $\eta = 33.1$
N616/N577	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 2.3$	x: 0 m $\eta = 26.9$	x: 0.3 m $\eta = 18.9$	$\eta = 6.3$	x: 0 m $\eta = 9.0$	x: 0 m $\eta = 27.9$	x: 0.3 m $\eta = 19.9$	x: 0 m $\eta = 8.6$	x: 0.3 m $\eta = 4.4$	x: 0 m $\eta = 43.3$	x: 0 m $\eta = 46.8$	x: 0 m $\eta = 40.4$	CUMPLE $\eta = 46.8$
N617/N578	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 0.7$	x: 0 m $\eta = 16.6$	x: 0 m $\eta = 23.0$	x: 0.15 m $\eta = 7.7$	x: 0 m $\eta = 5.6$	x: 0 m $\eta = 16.9$	x: 0 m $\eta = 23.3$	x: 0 m $\eta = 3.2$	x: 0 m $\eta = 6.0$	x: 0 m $\eta = 50.2$	x: 0 m $\eta = 40.2$	x: 0 m $\eta = 35.4$	CUMPLE $\eta = 50.2$
N618/N579	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.15 m $\eta = 0.2$	x: 0.15 m $\eta = 0.2$	$\eta = 0.8$	x: 0 m $\eta = 10.3$	x: 0 m $\eta = 22.4$	x: 0 m $\eta = 7.5$	x: 0 m $\eta = 3.4$	x: 0 m $\eta = 10.6$	x: 0 m $\eta = 22.7$	x: 0 m $\eta = 1.2$	x: 0 m $\eta = 5.7$	x: 0 m $\eta = 39.1$	x: 0.3 m $\eta = 14.8$	x: 0.3 m $\eta = 29.5$	CUMPLE $\eta = 39.1$
N619/N580	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.15 m $\eta < 0.1$	x: 0.15 m $\eta < 0.1$	$\eta = 0.6$	x: 0 m $\eta = 7.9$	x: 0 m $\eta = 25.9$	x: 0.15 m $\eta = 8.7$	x: 0 m $\eta = 2.6$	x: 0 m $\eta = 8.2$	x: 0 m $\eta = 26.1$	x: 0 m $\eta = 0.7$	x: 0 m $\eta = 7.6$	x: 0 m $\eta = 31.8$	x: 0.3 m $\eta = 33.6$	x: 0.3 m $\eta = 33.6$	CUMPLE $\eta = 33.6$
N620/N581	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta = 0.1$	$\eta = 0.1$	$\eta = 0.4$	x: 0.3 m $\eta = 11.0$	x: 0 m $\eta = 17.5$	$\eta = 5.8$	x: 0 m $\eta = 3.5$	x: 0.3 m $\eta = 11.1$	x: 0 m $\eta = 17.6$	x: 0.3 m $\eta = 1.4$	x: 0 m $\eta = 3.4$	x: 0 m $\eta = 24.5$	x: 0.3 m $\eta = 28.6$	x: 0.3 m $\eta = 25.6$	CUMPLE $\eta = 28.6$
N621/N582	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta = 0.3$	$\eta = 0.3$	$\eta = 0.4$	x: 0.3 m $\eta = 10.1$	x: 0 m $\eta = 8.9$	$\eta = 3.0$	x: 0 m $\eta = 3.1$	x: 0.3 m $\eta = 10.2$	x: 0 m $\eta = 9.0$	x: 0.3 m $\eta = 1.1$	x: 0 m $\eta = 0.9$	x: 0.3 m $\eta = 22.1$	x: 0.3 m $\eta = 10.9$	x: 0.3 m $\eta = 15.6$	CUMPLE $\eta = 22.1$
N622/N583	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta = 0.1$	$\eta = 0.1$	$\eta = 0.4$	x: 0.3 m $\eta = 5.3$	x: 0.3 m $\eta = 6.9$	x: 0 m $\eta = 2.3$	x: 0 m $\eta = 1.5$	x: 0.3 m $\eta = 5.4$	x: 0.3 m $\eta = 6.9$	x: 0.3 m $\eta = 0.3$	x: 0.3 m $\eta = 0.5$	x: 0 m $\eta = 9.8$	x: 0.3 m $\eta = 8.9$	x: 0 m $\eta = 8.7$	CUMPLE $\eta = 9.8$
N623/N584	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 0.2$	x: 0 m $\eta = 3.6$	x: 0.3 m $\eta = 7.6$	x: 0 m $\eta = 2.6$	x: 0 m $\eta = 1.2$	x: 0 m $\eta = 3.7$	x: 0.3 m $\eta = 7.7$	x: 0 m $\eta = 0.1$	x: 0.3 m $\eta = 0.7$	x: 0 m $\eta = 11.7$	x: 0.3 m $\eta = 9.1$	x: 0.3 m $\eta = 9.7$	CUMPLE $\eta = 11.7$
N624/N585	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta = 0.1$	$\eta = 0.1$	$\eta = 0.1$	x: 0 m $\eta = 4.0$	x: 0.3 m $\eta = 12.8$	$\eta = 4.3$	x: 0 m $\eta = 1.3$	x: 0.3 m $\eta = 2.6$	x: 0.3 m $\eta = 12.8$	x: 0 m $\eta = 0.2$	x: 0.3 m $\eta = 1.8$	x: 0 m $\eta = 17.3$	x: 0.3 m $\eta = 13.1$	x: 0.3 m $\eta = 16.1$	CUMPLE $\eta = 17.3$
N625/N586	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta = 0.1$	$\eta = 0.1$	$\eta = 0.2$	x: 0.3 m $\eta = 8.3$	x: 0.3 m $\eta = 8.3$	$\eta = 2.8$	x: 0 m $\eta = 2.5$	x: 0.3 m $\eta = 8.4$	x: 0.3 m $\eta = 8.4$	x: 0.3 m $\eta = 0.8$	x: 0.3 m $\eta = 0.8$	x: 0 m $\eta = 16.6$	x: 0.3 m $\eta = 9.0$	x: 0 m $\eta = 12.0$	CUMPLE $\eta = 16.6$
N626/N587	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta = 0.1$	$\eta = 0.1$	$\eta = 0.4$	x: 0.3 m $\eta = 10.9$	x: 0 m $\eta = 17.6$	$\eta = 5.8$	x: 0 m $\eta = 3.3$	x: 0.3 m $\eta = 10.9$	x: 0 m $\eta = 17.7$	x: 0.3 m $\eta = 1.3$	x: 0 m $\eta = 3.5$	x: 0.3 m $\eta = 23.7$	x: 0.3 m $\eta = 28.3$	x: 0.3 m $\eta = 25.5$	CUMPLE $\eta = 28.3$
N631/N592	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta = 0.9$	$\eta = 1.0$	$\eta = 0.2$	x: 0.3 m $\eta = 7.7$	x: 0.3 m $\eta = 32.8$	$\eta = 10.5$	x: 0 m $\eta = 1.3$	x: 0.3 m $\eta = 7.7$	x: 0.3 m $\eta = 32.9$	x: 0.3 m $\eta = 0.6$	x: 0.3 m $\eta = 11.9$	x: 0.3 m $\eta = 51.4$	x: 0.3 m $\eta = 39.8$	x: 0.3 m $\eta = 42.8$	CUMPLE $\eta = 51.4$
N627/N588	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta = 0.1$	$\eta = 0.1$	$\eta = 0.6$	x: 0.3 m $\eta = 8.0$	x: 0 m $\eta = 25.7$	x: 0.15 m $\eta = 8.6$	x: 0 m $\eta = 2.6$	x: 0.3 m $\eta = 8.2$	x: 0 m $\eta = 25.9$	x: 0.3 m $\eta = 0.7$	x: 0 m $\eta = 7.4$	x: 0 m $\eta = 30.8$	x: 0.3 m $\eta = 33.9$	x: 0.3 m $\eta = 33.4$	CUMPLE $\eta = 33.9$
N632/N593	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.15 m $\eta = 2.3$	x: 0.15 m $\eta = 2.5$	$\eta = 0.5$	x: 0.3 m $\eta = 9.7$	x: 0.3 m $\eta = 10.7$	x: 0.15 m $\eta = 3.4$	x: 0 m $\eta = 2.3$	x: 0.3 m $\eta = 9.8$	x: 0.3 m $\eta = 10.9$	x: 0.3 m $\eta = 1.0$	x: 0.3 m $\eta = 1.3$	x: 0.3 m $\eta = 26.1$	x: 0.3 m $\eta = 23.1$	x: 0.3 m $\eta = 20.5$	CUMPLE $\eta = 26.1$
N628/N589	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta = 0.1$	$\eta = 0.1$	$\eta = 0.9$	x: 0 m $\eta = 10.0$	x: 0.3 m $\eta = 20.0$	$\eta = 6.7$	x: 0 m $\eta = 3.3$	x: 0 m $\eta = 10.4$	x: 0.3 m $\eta = 20.4$	x: 0 m $\eta = 1.2$	x: 0.3 m $\eta = 4.6$	x: 0 m $\eta = 38.4$	x: 0.3 m $\eta = 30.0$	x: 0 m $\eta = 27.9$	CUMPLE $\eta = 38.4$
N633/N594	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.15 m $\eta = 0.9$	x: 0.15 m $\eta = 1.0$	x: 0.15 m $\eta = 0.9$	x: 0.3 m $\eta = 17.7$	x: 0 m $\eta = 16.4$	x: 0 m $\eta = 4.8$	x: 0 m $\eta = 3.9$	x: 0.3 m $\eta = 17.9$	x: 0 m $\eta = 16.8$	x: 0.3 m $\eta = 3.4$	x: 0 m $\eta = 3.0$	x: 0.3 m $\eta = 38.6$	x: 0.3 m $\eta = 29.9$	x: 0.3 m $\eta = 27.6$	CUMPLE $\eta = 38.6$
N629/N590	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta = 0.1$	$\eta = 0.1$	$\eta = 0.9$	x: 0.3 m $\eta = 20.0$	x: 0 m $\eta = 24.1$	x: 0.3 m $\eta = 7.9$	x: 0 m $\eta = 6.4$	x: 0.3 m $\eta = 20.4$	x: 0 m $\eta = 24.4$	x: 0.3 m $\eta = 4.6$	x: 0 m $\eta = 6.6$	x: 0 m $\eta = 44.5$	x: 0.3 m $\eta = 44.3$	x: 0.3 m $\eta = 38.5$	CUMPLE $\eta = 44.5$
N634/N595	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta = 0.4$	$\eta = 0.5$	x: 0.3 m $\eta = 1.0$	x: 0.3 m $\eta = 10.1$	x: 0.3 m $\eta = 8.9$	x: 0 m $\eta = 2.2$	x: 0 m $\eta = 1.3$	x: 0.3 m $\eta = 10.3$	x: 0.3 m $\eta = 9.2$	x: 0.3 m $\eta = 1.1$	x: 0.3 m $\eta = 0.9$	x: 0.3 m $\eta = 24.7$	x: 0.3 m $\eta = 18.3$	x: 0.3 m $\eta = 17.2$	CUMPLE $\eta = 24.7$
N630/N591	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta = 0.1$	$\eta = 0.1$	$\eta = 2.3$	x: 0.3 m $\eta = 29.6$	x: 0 m $\eta = 25.8$	x: 0.3 m $\eta = 8.5$	x: 0 m $\eta = 9.7$	x: 0.3 m $\eta = 30.6$	x: 0 m $\eta = 26.8$	x: 0.3 m $\eta = 10.3$	x: 0 m $\eta = 7.9$	x: 0.3 m $\eta = 48.5$	x: 0.3 m $\eta = 57.0$	x: 0.3 m $\eta = 48.7$	CUMPLE $\eta = 57.0$
N635/N596	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0 m $\eta = 5.2$	x: 0 m $\eta = 5.7$	$\eta = 0.9$	x: 0.3 m $\eta = 10.5$	x: 0.3 m $\eta = 30.8$	x: 0 m $\eta = 9.5$	x: 0 m $\eta = 1.9$	x: 0.3 m $\eta = 10.7$	x: 0.3 m $\eta = 31.0$	x: 0.3 m $\eta = 1.2$	x: 0.3 m $\eta = 10.5$	x: 0.3 m $\eta = 56.4$	x: 0.3 m $\eta = 47.3$	x: 0.3 m $\eta = 46.2$	CUMPLE $\eta = 56.4$
N611/N572	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.15 m $\eta < 0.1$	x: 0.15 m $\eta < 0.1$	$\eta = 0.4$	x: 0 m $\eta = 39.7$	x: 0 m $\eta = 17.6$	$\eta = 5.9$	x: 0 m $\eta = 13.3$	x: 0 m $\eta = 39.9$	x: 0 m $\eta = 17.8$	x: 0 m $\eta = 17.7$	x: 0 m $\eta = 3.5$	x: 0 m $\eta = 55.5$	x: 0 m $\eta = 43.9$	x: 0 m $\eta = 49.8$	CUMPLE $\eta = 55.5$
N615/N576	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta = 0.2$	$\eta = 0.1$	$\eta = 1.1$	x: 0 m $\eta = 16.7$	x: 0 m $\eta = 16.5$	x: 0.3 m $\eta = 5.5$	x: 0 m $\eta = 5.5$	x: 0 m $\eta = 17.2$	x: 0 m $\eta = 16.7$	x: 0 m $\eta = 3.3$	x: 0 m $\eta = 3.1$	x: 0 m $\eta = 35.7$	x: 0 m $\eta = 27.5$	x: 0 m $\eta = 25.2$	CUMPLE $\eta = 35.7$
N609/N570	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.15 m $\eta = 6.2$	x: 0.15 m $\eta = 6.8$	$\eta = 1.0$	x: 0.3 m $\eta = 70.7$	x: 0.3 m $\eta = 32.1$	x: 0.15 m $\eta = 10.6$	x: 0 m $\eta = 23.5$	x: 0.3 m $\eta = 71.1$	x: 0.3 m $\eta = 32.4$	x: 0.3 m $\eta = 56.1$	x: 0.3 m $\eta = 11.6$	x: 0.3 m $\eta = 34.8$	x: 0.3 m $\eta = 10.2$	x: 0.3 m $\eta = 17.6$	CUMPLE $\eta = 34.8$
N608/N569	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta = 10.1$	$\eta = 10.7$	$\eta = 1.3$	x: 0.3 m $\eta = 5.5$	x: 0 m $\eta = 23.2$	$\eta = 7.5$	x: 0 m $\eta = 1.8$	x: 0.3 m $\eta = 5.7$	x: 0 m $\eta = 23.7$	x: 0.3 m $\eta = 0.4$	x: 0 m $\eta = 6.2$	x: 0 m $\eta = 42.5$	x: 0 m $\eta = 34.7$	x: 0 m $\eta = 39.1$	CUMPLE $\eta = 42.5$
N612/N573	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 1.3$	x: 0.3 m $\eta = 42.8$	x: 0.3 m $\eta = 13.4$	$\eta = 4.4$	x: 0 m $\eta = 47.8$	x: 0.3 m $\eta = 43.4$	x: 0.3 m $\eta = 14.0$	x: 0.3 m $\eta = 28.5$	x: 0.3 m $\eta = 2.1$	x: 0.3 m $\eta = 92.3$	x: 0.3 m $\eta = 55.1$	x: 0.3 m $\eta = 19.2$	CUMPLE $\eta = 19.2$
N607/N568	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta = 0.1$	$\eta = 0.1$	$\eta = 0.7$	x: 0.3 m $\eta = 51.2$	x: 0 m $\eta = 30.1$	$\eta = 12.8$	x: 0 m $\eta = 64.2$	x: 0.3 m $\eta = 51.5$	x: 0 m $\eta = 30.4$	x: 0.3 m $\eta = 70.8$	x: 0 m $\eta = 10.9$	x: 0.3 m $\eta = 25.6$	x: 0.3 m $\eta = 81.4$	x: 0.3 m $\eta = 71.1$	CUMPLE $\eta = 71.1$
N613/N574	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 0.2$	x: 0 m $\eta = 58.9$	x: 0.3 m $\eta = 4.0$	$\eta = 1.7$	x: 0 m $\eta = 67.6$	x: 0 m $\eta = 59.0$	x: 0.3 m $\eta = 4.1$	x: 0 m $\eta = 98.5$	x: 0.3 m $\eta = 0.2$	x: 0 m $\eta = 23.6$	x: 0.3 m $\eta = 60.9$	x: 0 m $\eta = 94.5$	CUMPLE $\eta = 94.5$
N606/N567	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 0.3$	x: 0 m $\eta = 21.7$	x: 0 m $\eta = 30.1$	$\eta = 12.4$	x: 0 m $\eta = 50.0$	x: 0 m $\eta = 21.8$	x: 0 m $\eta = 30.3$	x: 0 m $\eta = 73.5$	x: 0 m $\eta = 10.7$	x: 0 m $\eta = 90.1$	x: 0 m $\eta = 50.7$	x: 0 m $\eta = 45.2$	CUMPLE $\eta = 45.2$
N614/N575	$w / t \leq (w / t)_{Máx.}$ Cumple	$\eta < 0.1$	$\eta < 0.1$	$\eta = 3.9$	x: 0 m $\eta = 17.7$	x: 0 m $\eta = 4.8$	$\eta = 2.0$	x: 0 m $\eta = 48.4$	x: 0 m $\eta = 19.3$	x: 0 m $\eta = 6.5$	x: 0 m $\eta = 65.8$	x: 0 m $\eta = 0.5$	x: 0 m $\eta = 57.0$	x: 0 m $\eta = 25.6$	x: 0 m $\eta = 16.6$	CUMPLE $\eta = 16.6$
N631/N637	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 1.118 m $\eta = 0.3$	x: 0 m $\eta = 12.1$	$\eta = 0.8$	x: 0.932 m $\eta = 1.1$	x: 1.118 m $\eta = 4.6$	$\eta = 0.3$	x: 0 m $\eta = 0.1$	x: 0.932 m $\eta = 1.4$	x: 1.118 m $\eta = 4.6$	x: 0.932 m $\eta < 0.1$	x: 1.118 m $\eta = 0.2$	N.P.[1]	x: 1.118 m $\eta = 14.7$	x: 1.118 m $\eta = 13.8$	CUMPLE $\eta = 14.7$
N592/N638	$w / t \leq (w / t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m $\eta = 18.8$	$\eta = 0.8$	x: 1.118 m $\eta = 1.7$	x: 1.118 m $\eta = 4.7$	$\eta = 0.3$	x: 0 m $\eta = 0.2$	x: 1.118 m $\eta = 2.1$	x: 1.118 m $\eta = 4.8$	x: 1.118 m $\eta < 0.1$	x: 1.118 m $\eta = 0.2$	N.P.[1]	x: 1.118 m $\eta = 22.1$	x: 1.118 m $\eta = 21.1$	CUMPLE $\eta = 22.1$
N626/N637	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.168 m $\eta = 1.9$	x: 0.168 m $\eta = 5.8$	$\eta = 0.7$	x: 0 m $\eta = 0.9$	x: 0 m $\eta = 3.7$	x: 0.503 m $\eta = 0.4$	x: 1.006 m $\eta = 0.1$	x: 0 m $\eta = 1.0$	x: 0 m $\eta = 4.0$	x: 0 m $\eta < 0.1$	x: 0 m $\eta = 0.2$	N.P.[4]	x: 0 m $\eta = 8.5$	x: 0 m $\eta = 8.4$	CUMPLE $\eta = 8.5$
N625/N637	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.953 m $\eta = 4.0$	x: 0.715 m $\eta = 1.7$	x: 0.238 m $\eta = 0.7$	x: 0 m $\eta = 0.6$	x: 0 m $\eta = 4.2$	x: 0.476 m $\eta = 0.4$	x: 0 m $\eta = 0.1$	x: 0.953 m $\eta = 0.8$	x: 0 m $\eta = 4.5$	x: 0.953 m $\eta < 0.1$	x: 0 m $\eta = 0.2$	N.P.[1]	x: 0 m $\eta = 4.9$	x: 0 m $\eta = 8.2$	CUMPLE $\eta = 8.2$
N587/N638	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.335 m $\eta = 1.7$	x: 0 m $\eta = 7.6$	$\eta = 0.5$	x: 0 m $\eta = 1.3$	x: 1.006 m $\eta = 9.5$	$\eta = 0.8$	x: 1.006 m $\eta = 0.1$	x: 0 m $\eta = 1.3$	x: 1.006 m $\eta = 9.7$	x: 0 m $\eta < 0.1$	x: 1.006 m $\eta = 0.9$	x: 1.006 m $\eta = 11.7$	x: 1.006 m $\eta = 15.1$	x: 1.006 m $\eta = 16.7$	CUMPLE $\eta = 16.7$
N586/N638	$w / t \leq (w / t)_{Máx.}$ Cumple	x: 0.715 m $\eta = 4.0$	x: 0 m $\eta = 2.0$	x: 0.476 m $\eta = 0.4$	x: 0 m $\eta = 0.5$	x: 0.953 m $\eta = 9.9$	$\eta = 0.9$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 0.5$	x: 0.953 m $\eta = 10.1$	x: 0 m $\eta < 0.1$	x: 0.953 m $\eta = 1.0$	x: 0.953 m $\eta = 16.0$	x: 0.953 m $\eta = 10.7$	x: 0.953 m $\eta = 15.2$	CUMPLE $\eta = 16.0$

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N637/N639	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 14.5	η = 0.6	x: 0.746 m η = 1.1	x: 0 m η = 3.1	x: 0 m η = 0.1	x: 0 m η = 0.1	x: 0.746 m η = 1.4	x: 0 m η = 3.4	x: 0.746 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 1.119 m η = 17.0	x: 1.119 m η = 16.3	CUMPLE η = 17.0
N639/N640	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 15.9	x: 1.122 m η = 1.0	x: 0.748 m η = 1.2	x: 1.122 m η = 10.0	x: 1.122 m η = 1.6	x: 0 m η = 0.1	x: 0.748 m η = 1.3	x: 1.122 m η = 10.4	x: 0.748 m η < 0.1	x: 1.122 m η = 1.1	N.P.[1]	x: 1.122 m η = 18.4	x: 1.122 m η = 19.4	CUMPLE η = 19.4
N638/N641	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 21.7	η = 0.5	x: 1.119 m η = 1.4	x: 0 m η = 3.3	x: 0 m η = 0.1	x: 0 m η = 0.1	x: 1.119 m η = 1.6	x: 0 m η = 3.3	x: 1.119 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 1.119 m η = 24.7	x: 1.119 m η = 23.9	CUMPLE η = 24.7
N641/N642	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 23.3	η = 0.7	x: 1.122 m η = 1.5	x: 1.122 m η = 10.0	η = 1.6	x: 0 m η = 0.1	x: 1.122 m η = 1.6	x: 1.122 m η = 10.3	x: 1.122 m η < 0.1	x: 1.122 m η = 1.1	N.P.[1]	x: 0.748 m η = 25.7	x: 0.935 m η = 25.3	CUMPLE η = 25.7
N637/N638	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 0.4	x: 0 m η = 0.5	η = 0.2	x: 0.3 m η = 9.9	x: 0.3 m η = 6.9	x: 0 m η = 2.0	x: 0 m η = 1.3	x: 0.3 m η = 9.9	x: 0.3 m η = 7.0	x: 0.3 m η = 1.0	x: 0.3 m η = 0.5	x: 0.3 m η = 20.8	x: 0.3 m η = 15.4	x: 0.3 m η = 15.1	CUMPLE η = 20.8
N639/N641	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.15 m η = 0.9	x: 0.15 m η = 1.1	η = 0.1	x: 0.3 m η = 11.9	x: 0 m η = 21.8	x: 0.15 m η = 7.1	x: 0 m η = 2.2	x: 0.3 m η = 11.9	x: 0 m η = 21.8	x: 0.3 m η = 1.5	x: 0 m η = 5.3	x: 0.3 m η = 41.8	x: 0.3 m η = 31.7	x: 0.3 m η = 30.8	CUMPLE η = 41.8
N640/N642	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 1.4	η = 1.5	η = 0.1	x: 0.3 m η = 8.7	x: 0.3 m η = 14.8	x: 0 m η = 5.0	x: 0 m η = 2.4	x: 0.3 m η = 8.8	x: 0.3 m η = 14.9	x: 0.3 m η = 0.8	x: 0.3 m η = 2.5	x: 0.3 m η = 28.6	x: 0.3 m η = 25.0	x: 0.3 m η = 22.9	CUMPLE η = 28.6
N625/N639	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.017 m η = 2.1	x: 0 m η = 4.3	x: 1.017 m η = 1.0	x: 0 m η = 0.7	x: 1.017 m η = 3.5	x: 1.017 m η = 0.3	x: 1.017 m η = 0.1	x: 0 m η = 0.8	x: 1.017 m η = 3.9	x: 0 m η < 0.1	x: 1.017 m η = 0.2	N.P.[1]	x: 1.017 m η = 5.2	x: 1.017 m η = 5.1	CUMPLE η = 5.2
N624/N639	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.974 m η = 3.2	x: 0 m η = 2.0	η = 0.2	x: 0.974 m η = 0.5	x: 0 m η = 3.1	x: 0.974 m η = 0.2	x: 0 m η = 0.1	x: 0.974 m η = 0.5	x: 0 m η = 3.2	x: 0.974 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 3.9	x: 0 m η = 5.2	CUMPLE η = 5.2
N624/N640	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.021 m η = 2.3	x: 0 m η = 3.3	x: 0.51 m η = 0.2	x: 0.17 m η = 0.5	x: 0 m η = 4.8	x: 0.34 m η = 0.5	x: 1.021 m η = 0.1	x: 0.17 m η = 0.6	x: 0 m η = 4.9	x: 0.17 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 0 m η = 5.6	x: 0 m η = 6.6	CUMPLE η = 6.6
N623/N640	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.246 m η = 2.8	x: 0.246 m η = 2.8	x: 0.492 m η = 0.5	x: 0.985 m η = 0.4	x: 0.985 m η = 5.9	x: 0.739 m η = 0.6	x: 0.985 m η = 0.1	x: 0.985 m η = 0.5	x: 0.985 m η = 6.1	x: 0.985 m η < 0.1	x: 0.985 m η = 0.4	x: 0.985 m η = 8.0	x: 0.985 m η = 6.6	x: 0.985 m η = 7.5	CUMPLE η = 8.0
N586/N641	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.339 m η = 2.0	x: 0.339 m η = 5.3	η = 0.2	x: 0 m η = 1.1	x: 1.017 m η = 8.2	x: 1.017 m η = 0.6	x: 1.017 m η = 0.1	x: 0 m η = 1.2	x: 1.017 m η = 8.2	x: 0 m η < 0.1	x: 1.017 m η = 0.7	x: 1.017 m η = 10.4	x: 1.017 m η = 12.4	x: 1.017 m η = 14.1	CUMPLE η = 14.1
N585/N641	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.974 m η = 3.4	x: 0 m η = 2.6	x: 0 m η = 1.0	x: 0 m η = 0.5	x: 0.974 m η = 6.5	x: 0.487 m η = 0.6	x: 0.974 m η = 0.1	x: 0.974 m η = 0.7	x: 0.974 m η = 6.9	x: 0.974 m η < 0.1	x: 0.974 m η = 0.5	x: 0.974 m η = 11.9	x: 0.974 m η = 8.4	x: 0.974 m η = 10.5	CUMPLE η = 11.9
N585/N642	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.34 m η = 2.2	x: 0.34 m η = 3.9	x: 0.681 m η = 0.2	x: 0 m η = 0.8	x: 0 m η = 4.8	η = 0.4	x: 1.021 m η = 0.1	x: 0 m η = 0.9	x: 0 m η = 4.8	x: 0 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 0 m η = 7.2	x: 0 m η = 7.7	CUMPLE η = 7.7
N584/N642	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.985 m η = 2.3	x: 0 m η = 3.0	η = 0.8	x: 0 m η = 0.8	x: 0 m η = 5.0	η = 0.5	x: 0.985 m η = 0.1	x: 0 m η = 0.9	x: 0 m η = 5.3	x: 0 m η < 0.1	x: 0 m η = 0.3	N.P.[1]	x: 0 m η = 6.5	x: 0 m η = 6.7	CUMPLE η = 6.7
N623/N643	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.026 m η = 2.8	x: 0.342 m η = 2.2	x: 0 m η = 0.6	x: 0.513 m η = 0.4	x: 1.026 m η = 5.0	x: 0.684 m η = 0.4	x: 1.026 m η = 0.1	x: 0.342 m η = 0.4	x: 1.026 m η = 5.3	x: 0.342 m η < 0.1	x: 1.026 m η = 0.3	N.P.[1]	x: 0 m η = 4.3	x: 1.026 m η = 7.1	CUMPLE η = 7.1
N622/N643	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.007 m η = 2.0	x: 0 m η = 3.3	η = 0.7	x: 0 m η = 0.6	x: 0 m η = 3.0	x: 0.671 m η = 0.3	x: 1.007 m η = 0.1	x: 0 m η = 0.7	x: 0 m η = 3.2	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 6.0	x: 0 m η = 5.8	CUMPLE η = 6.0
N640/N643	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 16.2	x: 1.12 m η = 0.8	x: 0.56 m η = 1.2	x: 0 m η = 6.0	η = 0.8	x: 1.12 m η = 0.1	x: 0.56 m η = 1.3	x: 0 m η = 6.4	x: 0.56 m η < 0.1	x: 0 m η = 0.4	N.P.[1]	x: 0.933 m η = 18.3	x: 0.747 m η = 17.9	CUMPLE η = 18.3
N644/N643	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 15.3	x: 0.561 m η = 1.5	x: 0.935 m η = 1.1	x: 0 m η = 6.6	η = 1.1	x: 0 m η = 0.1	x: 0.935 m η = 1.3	x: 0 m η = 7.3	x: 0.748 m η < 0.1	x: 0 m η = 0.5	N.P.[1]	x: 0 m η = 17.8	x: 0 m η = 17.2	CUMPLE η = 17.8
N645/N644	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 13.9	η = 0.9	x: 0.566 m η = 1.0	x: 0 m η = 3.7	η = 0.3	x: 1.131 m η = 0.1	x: 0.566 m η = 1.3	x: 0 m η = 4.1	x: 0.377 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 1.131 m η = 16.6	x: 1.131 m η = 15.8	CUMPLE η = 16.6
N646/N645	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.752 m η = 0.5	x: 0 m η = 11.5	η = 0.9	x: 1.128 m η = 1.1	x: 1.128 m η = 4.7	x: 1.128 m η = 0.4	x: 0 m η = 0.1	x: 1.128 m η = 1.5	x: 1.128 m η = 4.8	x: 1.128 m η < 0.1	x: 1.128 m η = 0.2	N.P.[1]	x: 0.564 m η = 13.9	x: 0.94 m η = 12.9	CUMPLE η = 13.9
N647/N646	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.138 m η = 2.1	x: 0 m η = 8.1	η = 1.2	x: 1.138 m η = 0.8	x: 0 m η = 13.0	η = 1.9	x: 0 m η = 0.1	x: 1.138 m η = 1.3	x: 0 m η = 13.4	x: 1.138 m η < 0.1	x: 0 m η = 1.8	N.P.[1]	x: 0 m η = 17.3	x: 0 m η = 20.0	CUMPLE η = 20.0
N648/N647	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.148 m η = 3.8	x: 0 m η = 7.3	η = 1.9	x: 0.383 m η = 0.6	x: 1.148 m η = 9.6	η = 1.2	x: 0 m η = 0.1	x: 0.766 m η = 1.2	x: 1.148 m η = 10.0	x: 0.766 m η < 0.1	x: 1.148 m η = 1.0	x: 1.148 m η = 6.5	x: 1.148 m η = 13.3	x: 1.148 m η = 13.8	CUMPLE η = 13.8
N649/N648	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.941 m η = 5.5	x: 0 m η = 5.9	x: 1.129 m η = 2.0	x: 0 m η = 1.3	x: 0 m η = 4.3	x: 1.129 m η = 0.4	x: 0 m η = 0.2	x: 0 m η = 2.2	x: 0 m η = 5.1	x: 0 m η < 0.1	x: 0 m η = 0.3	x: 0 m η = 9.8	x: 1.129 m η = 7.2	x: 0 m η = 7.2	CUMPLE η = 9.8
N650/N649	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.187 m η = 8.6	x: 0.187 m η = 4.5	η = 1.8	x: 0 m η = 3.0	x: 1.12 m η = 6.2	x: 0.56 m η = 0.8	x: 0 m η = 0.3	x: 0 m η = 3.8	x: 1.12 m η = 6.7	x: 0 m η = 0.1	x: 1.12 m η = 0.5	x: 0 m η = 13.6	x: 1.12 m η = 7.4	x: 1.12 m η = 12.8	CUMPLE η = 13.6
N600/N650	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.902 m η = 7.4	x: 0 m η = 1.9	x: 0.677 m η = 4.9	x: 0.902 m η = 3.5	x: 0 m η = 13.0	x: 0.677 m η = 2.0	x: 0.902 m η = 0.7	x: 0.902 m η = 4.2	x: 0 m η = 15.2	x: 0.902 m η = 0.2	x: 0 m η = 2.3	x: 0 m η = 25.9	x: 0.902 m η = 3.7	x: 0 m η = 19.9	CUMPLE η = 25.9
N622/N644	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.034 m η = 3.2	x: 0 m η = 0.9	x: 0.689 m η = 0.2	x: 1.034 m η = 0.4	x: 0 m η = 4.3	x: 0.862 m η = 0.3	x: 0 m η = 0.1	x: 0 m η = 0.4	x: 0 m η = 4.4	x: 0 m η < 0.1	x: 0 m η = 0.2	N.P.[1]	x: 0 m η = 2.6	x: 0 m η = 6.3	CUMPLE η = 6.3
N621/N644	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.024 m η = 1.6	x: 0 m η = 3.5	η = 0.9	x: 0 m η = 0.7	x: 1.024 m η = 5.2	η = 0.5	x: 1.024 m η = 0.1	x: 0 m η = 0.8	x: 1.024 m η = 5.6	x: 0 m η < 0.1	x: 1.024 m η = 0.3	N.P.[1]	x: 1.024 m η = 7.2	x: 1.024 m η = 7.1	CUMPLE η = 7.2
N621/N645	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.013 m η = 3.8	x: 1.013 m η = 0.5	η = 0.5	x: 1.013 m η = 0.5	x: 0 m η = 6.4	η = 0.6	x: 0 m η = 0.1	x: 0.844 m η = 0.5	x: 0 m η = 6.6	x: 0.844 m η < 0.1	x: 0 m η = 0.4	x: 0 m η = 11.1	x: 1.013 m η = 1.1	x: 0 m η = 10.3	CUMPLE η = 11.1
N620/N645	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.167 m η = 0.8	x: 0 m η = 4.8	x: 0.502 m η = 0.5	x: 0 m η = 0.9	x: 1.003 m η = 5.7	η = 0.6	x: 1.003 m η = 0.1	x: 0 m η = 1.0	x: 1.003 m η = 5.9	x: 0 m η < 0.1	x: 1.003 m η = 0.4	x: 0 m η = 7.3	x: 0 m η = 9.7	x: 1.003 m η = 10.3	CUMPLE η = 10.3
N620/N646	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.011 m η = 5.8	x: 0.337 m η = 0.7	x: 0.674 m η = 1.0	x: 1.011 m η = 0.7	x: 1.011 m η = 3.0	x: 0.337 m η = 0.3	x: 0 m η = 0.1	x: 0 m η = 0.9	x: 1.011 m η = 3.5	x: 0 m η < 0.1	x: 1.011 m η = 0.1	N.P.[1]	x: 1.011 m η = 4.5	x: 1.011 m η = 8.1	CUMPLE η = 8.1
N619/N646	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.675 m η = 0.6	x: 0 m η = 6.9	x: 0.675 m η = 0.4	x: 0 m η = 0.9	x: 0 m η = 2.4	x: 0.844 m η = 0.2	x: 1.012 m η = 0.1	x: 0 m η = 1.0	x: 0 m η = 2.5	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 1.012 m η = 10.0	x: 1.012 m η = 9.8	CUMPLE η = 10.0
N619/N647	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.999 m η = 6.7	x: 0.25 m η = 0.2	x: 0.25 m η = 0.2	x: 0 m η = 0.6	x: 0 m η = 6.6	x: 0.749 m η = 0.7	x: 0 m η = 0.1	x: 0 m η = 0.6	x: 0 m η = 6.7	x: 0 m η < 0.1	x: 0 m η = 0.5	x: 0.999 m η = 13.1	x: 0 m η = 6.9	x: 0.999 m η = 12.4	CUMPLE η = 13.1
N618/N647	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.248 m η = 0.2	x: 0 m η = 9.0	x: 0.745 m η = 0.3	x: 0 m η = 1.6	x: 0 m η = 6.6	x: 0.745 m η = 0.5	x: 0.993 m η = 0.2	x: 0 m η = 1.7	x: 0 m η = 6.7	x: 0 m η < 0.1	x: 0 m η = 0.5	N.P.[1]	x: 0 m η = 12.5	x: 0 m η = 12.9	CUMPLE η = 12.9
N618/N648	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.968 m η = 7.3	N.P.[2]	x: 0.242 m η = 0.8	x: 0 m η = 1.9	x: 0.968 m η = 2.3	η = 0.1	x: 0 m η = 0.2	x: 0 m η = 1.4	x: 0.968 m η = 2.7	x: 0 m η < 0.1	x: 0.968 m η = 0.1	N.P.[1]	N.P.[3]	x: 0 m η = 10.1	CUMPLE η = 10.1
N617/N648	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 10.4	x: 0.235 m η = 0.7	x: 0 m η = 1.7	x: 0.941 m η = 4.5	x: 0.706 m η = 0.3	x: 0 m η = 0.1	x: 0 m η = 1.8	x: 0.941 m η = 4.8	x: 0 m η < 0.1	x: 0.941 m η = 0.2	N.P.[1]	x: 0.941 m η = 13.0	x: 0.941 m η = 13.6	CUMPLE η = 13.6
N617/N649	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.971 m η = 10.4	N.P.[2]	η = 0.1	x: 0 m η = 2.0	x: 0 m η = 5.4	x: 0.243 m η = 0.5	x: 0.971 m η = 0.2	x: 0 m η = 1.6	x: 0 m η = 5.4	x: 0 m η < 0.1	x: 0 m η = 0.3	x: 0 m η = 13.9	N.P.[3]	x: 0 m η = 13.9	CUMPLE η = 13.9
N616/N649	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 15.0	x: 0.474 m η = 0.5	x: 0 m η = 14.9	x: 0.947 m η = 5.9	x: 0.474 m η = 0.5	x: 0.947 m η = 1.2	x: 0 m η = 10.7	x: 0.947 m η = 6.1	x: 0 m η = 2.2	x: 0.947 m η = 0.4	N.P.[1]	x: 0 m η = 31.6	x: 0 m η = 33.7	CUMPLE η = 33.7

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N616/N650	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.981 m η = 3.9	x: 0 m η = 6.8	η = 0.3	x: 0 m η = 15.2	x: 0 m η = 2.4	η = 0.1	x: 0 m η = 1.2	x: 0 m η = 15.3	x: 0 m η = 2.6	x: 0 m η = 2.4	x: 0 m η = 0.1	x: 0 m η = 13.4	x: 0 m η = 20.0	x: 0 m η = 21.8	CUMPLE η = 21.8
N602/N650	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.974 m η = 2.3	x: 0 m η = 4.4	x: 0 m η = 3.3	x: 0 m η = 15.2	x: 0.974 m η = 6.2	η = 0.6	x: 0 m η = 1.2	x: 0 m η = 11.8	x: 0.974 m η = 7.6	x: 0 m η = 2.3	x: 0.974 m η = 0.6	x: 0 m η = 17.0	x: 0 m η = 18.3	x: 0 m η = 20.4	CUMPLE η = 20.4
N584/N651	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.026 m η = 2.5	x: 0 m η = 2.2	x: 0.513 m η = 1.3	x: 0.171 m η = 0.6	x: 0 m η = 2.0	x: 0.342 m η = 0.2	x: 1.026 m η = 0.1	x: 1.026 m η = 1.0	x: 0 m η = 2.0	x: 1.026 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 3.8	x: 0 m η = 3.9	CUMPLE η = 3.9
N583/N651	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.336 m η = 1.8	x: 0.336 m η = 4.1	η = 0.2	x: 0 m η = 1.0	x: 1.007 m η = 3.4	x: 1.007 m η = 0.2	x: 1.007 m η = 0.1	x: 0 m η = 1.1	x: 1.007 m η = 3.5	x: 0 m η < 0.1	x: 1.007 m η = 0.1	N.P.(1)	x: 1.007 m η = 7.4	x: 1.007 m η = 7.9	CUMPLE η = 7.9
N583/N652	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.172 m η = 3.5	x: 0.172 m η = 2.1	x: 0.172 m η = 1.1	x: 0 m η = 0.4	x: 1.034 m η = 6.8	x: 0.517 m η = 0.6	x: 1.034 m η = 0.1	x: 1.034 m η = 0.9	x: 1.034 m η = 7.3	x: 1.034 m η < 0.1	x: 1.034 m η = 0.5	x: 1.034 m η = 13.4	x: 1.034 m η = 9.6	x: 1.034 m η = 11.9	CUMPLE η = 13.4
N642/N651	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 23.7	x: 0.933 m η = 0.6	x: 0.373 m η = 1.2	x: 0 m η = 6.0	x: 0 m η = 0.8	x: 1.12 m η = 0.1	x: 0.373 m η = 1.3	x: 0 m η = 6.3	x: 0.373 m η < 0.1	x: 0 m η = 0.4	N.P.(1)	x: 0.933 m η = 25.8	x: 0.747 m η = 25.4	CUMPLE η = 25.8
N652/N651	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 22.7	x: 0.187 m η = 1.2	x: 1.122 m η = 1.5	x: 0 m η = 7.1	η = 1.2	x: 0 m η = 0.1	x: 1.122 m η = 1.7	x: 0 m η = 7.6	x: 1.122 m η < 0.1	x: 0 m η = 0.6	N.P.(1)	x: 0.561 m η = 25.3	x: 1.122 m η = 24.6	CUMPLE η = 25.3
N582/N652	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.171 m η = 1.7	x: 0.171 m η = 4.6	η = 0.2	x: 0 m η = 1.1	x: 1.024 m η = 10.5	x: 0.853 m η = 0.8	x: 1.024 m η = 0.1	x: 0 m η = 1.2	x: 1.024 m η = 10.5	x: 0 m η < 0.1	x: 1.024 m η = 1.1	x: 1.024 m η = 13.6	x: 1.024 m η = 15.2	x: 1.024 m η = 17.3	CUMPLE η = 17.3
N653/N652	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 21.0	x: 0.377 m η = 1.2	x: 1.131 m η = 1.2	x: 0 m η = 3.6	x: 0.377 m η = 0.2	x: 0 m η = 0.1	x: 1.131 m η = 1.4	x: 0 m η = 4.2	x: 0.943 m η < 0.1	x: 0 m η = 0.2	N.P.(1)	x: 1.131 m η = 24.0	x: 1.131 m η = 23.2	CUMPLE η = 24.0
N582/N653	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.013 m η = 3.7	x: 0.844 m η = 1.1	x: 0 m η = 0.3	x: 0 m η = 0.5	x: 1.013 m η = 9.7	x: 0.169 m η = 0.9	x: 0 m η = 0.1	x: 0 m η = 0.5	x: 1.013 m η = 9.8	x: 0 m η < 0.1	x: 1.013 m η = 1.0	x: 1.013 m η = 15.8	x: 1.013 m η = 10.9	x: 1.013 m η = 15.1	CUMPLE η = 15.8
N581/N653	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.167 m η = 0.6	x: 0 m η = 8.1	x: 1.003 m η = 0.3	x: 0 m η = 1.3	x: 1.003 m η = 10.3	x: 1.003 m η = 0.9	x: 1.003 m η = 0.1	x: 0 m η = 1.4	x: 1.003 m η = 10.5	x: 0 m η < 0.1	x: 1.003 m η = 1.1	x: 1.003 m η = 12.5	x: 1.003 m η = 16.0	x: 1.003 m η = 17.9	CUMPLE η = 17.9
N581/N654	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.011 m η = 6.5	N.P.(2)	η = 0.4	x: 0 m η = 0.6	x: 1.011 m η = 6.3	η = 0.5	x: 0 m η = 0.1	x: 0 m η = 0.6	x: 1.011 m η = 6.4	x: 0 m η < 0.1	x: 1.011 m η = 0.4	x: 1.011 m η = 12.3	N.P.(3)	x: 1.011 m η = 11.5	CUMPLE η = 12.3
N654/N653	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 18.1	η = 1.0	x: 1.128 m η = 1.7	x: 1.128 m η = 4.6	η = 0.4	x: 0 m η = 0.2	x: 1.128 m η = 2.2	x: 1.128 m η = 5.0	x: 1.128 m η < 0.1	x: 1.128 m η = 0.2	N.P.(1)	x: 1.128 m η = 21.2	x: 1.128 m η = 20.3	CUMPLE η = 21.2
N580/N654	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.012 m η = 0.1	x: 0 m η = 10.5	η = 0.9	x: 0 m η = 1.4	x: 1.012 m η = 4.7	η = 0.4	x: 1.012 m η = 0.1	x: 0 m η = 1.5	x: 1.012 m η = 5.1	x: 0 m η < 0.1	x: 1.012 m η = 0.3	N.P.(1)	x: 1.012 m η = 13.7	x: 1.012 m η = 13.3	CUMPLE η = 13.7
N655/N654	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.138 m η = 1.8	x: 0 m η = 13.9	η = 1.2	x: 1.138 m η = 1.4	x: 0 m η = 13.2	x: 0.569 m η = 2.0	x: 0 m η = 0.2	x: 1.138 m η = 2.0	x: 0 m η = 13.4	x: 1.138 m η < 0.1	x: 0 m η = 1.8	x: 0 m η = 4.7	x: 0 m η = 20.2	x: 0 m η = 22.8	CUMPLE η = 22.8
N580/N655	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.999 m η = 7.8	N.P.(2)	x: 0.5 m η = 0.4	x: 0 m η = 0.6	x: 0 m η = 6.8	x: 0.5 m η = 0.7	x: 0 m η = 0.1	x: 0 m η = 0.7	x: 0 m η = 6.9	x: 0 m η < 0.1	x: 0 m η = 0.5	x: 0 m η = 13.3	N.P.(3)	x: 0.999 m η = 12.3	CUMPLE η = 13.3
N579/N655	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.745 m η = 0.8	x: 0 m η = 13.2	η = 0.4	x: 0 m η = 2.1	x: 0 m η = 6.5	η = 0.6	x: 0.993 m η = 0.2	x: 0 m η = 2.2	x: 0 m η = 6.7	x: 0 m η < 0.1	x: 0 m η = 0.5	x: 0 m η = 9.2	x: 0 m η = 16.7	x: 0 m η = 16.8	CUMPLE η = 16.8
N579/N656	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.968 m η = 8.9	x: 0.242 m η = 1.7	x: 0 m η = 0.7	x: 0 m η = 1.8	x: 0.968 m η = 2.9	x: 0 m η = 0.2	x: 0 m η = 0.2	x: 0 m η = 1.7	x: 0.968 m η = 3.2	x: 0 m η < 0.1	x: 0.968 m η = 0.1	N.P.(1)	x: 0.968 m η = 5.3	x: 0 m η = 11.6	CUMPLE η = 11.6
N656/N655	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.148 m η = 3.0	x: 0 m η = 9.7	x: 0.574 m η = 2.2	x: 1.148 m η = 1.5	x: 1.148 m η = 9.6	x: 0.191 m η = 1.2	x: 0 m η = 0.2	x: 1.148 m η = 2.1	x: 1.148 m η = 10.2	x: 1.148 m η < 0.1	x: 1.148 m η = 1.1	N.P.(1)	x: 1.148 m η = 16.3	x: 1.148 m η = 15.7	CUMPLE η = 16.3
N578/N656	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.471 m η = 0.3	x: 0 m η = 16.3	x: 0.941 m η = 0.8	x: 0 m η = 1.7	x: 0.941 m η = 3.9	x: 0.471 m η = 0.2	x: 0 m η = 0.1	x: 0 m η = 1.7	x: 0.941 m η = 4.2	x: 0 m η < 0.1	x: 0.941 m η = 0.2	N.P.(1)	x: 0.941 m η = 19.1	x: 0.941 m η = 19.4	CUMPLE η = 19.4
N657/N656	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.941 m η = 5.2	x: 0 m η = 7.6	η = 1.9	x: 0 m η = 2.4	x: 0 m η = 4.1	x: 1.129 m η = 0.4	x: 0 m η = 0.4	x: 0 m η = 3.3	x: 0 m η = 4.8	x: 0 m η = 0.1	x: 0 m η = 0.2	x: 0 m η = 8.6	x: 1.129 m η = 9.5	x: 1.129 m η = 8.9	CUMPLE η = 9.5
N578/N657	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.971 m η = 13.6	N.P.(2)	η = 0.2	x: 0 m η = 2.3	x: 0 m η = 5.6	x: 0 m η = 0.5	x: 0.971 m η = 0.2	x: 0 m η = 1.7	x: 0 m η = 5.7	x: 0 m η = 0.1	x: 0 m η = 0.3	x: 0 m η = 17.0	N.P.(3)	x: 0 m η = 17.3	CUMPLE η = 17.3
N577/N657	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.(4)	x: 0 m η = 22.8	η = 0.6	x: 0 m η = 17.2	x: 0.947 m η = 6.5	x: 0.71 m η = 0.5	x: 0.947 m η = 1.4	x: 0 m η = 11.4	x: 0.947 m η = 6.8	x: 0 m η = 3.0	x: 0.947 m η = 0.5	N.P.(1)	x: 0 m η = 42.3	x: 0 m η = 44.3	CUMPLE η = 44.3
N658/N657	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.12 m η = 8.9	x: 0 m η = 5.8	η = 1.8	x: 0 m η = 4.3	x: 1.12 m η = 6.1	x: 0.373 m η = 0.8	x: 0 m η = 0.6	x: 0 m η = 5.1	x: 1.12 m η = 6.3	x: 0 m η = 0.3	x: 1.12 m η = 0.4	x: 1.12 m η = 14.5	x: 1.12 m η = 8.7	x: 1.12 m η = 13.3	CUMPLE η = 14.5
N577/N658	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.736 m η = 4.4	x: 0.736 m η = 5.9	η = 0.2	x: 0 m η = 17.4	x: 0 m η = 2.6	η = 0.1	x: 0 m η = 1.3	x: 0 m η = 17.5	x: 0 m η = 2.7	x: 0 m η = 3.1	x: 0 m η = 0.1	x: 0 m η = 24.9	x: 0 m η = 17.8	x: 0 m η = 22.3	CUMPLE η = 24.9
N566/N658	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.974 m η = 0.9	x: 0 m η = 8.5	x: 0.487 m η = 3.1	x: 0 m η = 16.7	x: 0.974 m η = 6.6	x: 0.487 m η = 0.6	x: 0 m η = 1.3	x: 0 m η = 12.3	x: 0.974 m η = 7.9	x: 0 m η = 2.8	x: 0.974 m η = 0.6	x: 0 m η = 16.7	x: 0 m η = 25.3	x: 0 m η = 29.4	CUMPLE η = 29.4
N561/N658	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.226 m η = 7.7	x: 0.226 m η = 3.6	x: 0.677 m η = 5.3	x: 0.902 m η = 2.7	x: 0 m η = 14.3	x: 0.677 m η = 2.1	x: 0.902 m η = 0.6	x: 0.902 m η = 3.7	x: 0 m η = 16.3	x: 0.902 m η = 0.1	x: 0 m η = 2.7	x: 0 m η = 31.6	x: 0 m η = 21.9	x: 0 m η = 25.0	CUMPLE η = 31.6
N643/N651	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 6.8	x: 0 m η = 7.4	η = 0.3	x: 0.3 m η = 14.8	x: 0 m η = 19.0	x: 0.3 m η = 6.3	x: 0 m η = 3.3	x: 0.3 m η = 14.9	x: 0 m η = 19.1	x: 0.3 m η = 2.3	x: 0 m η = 4.0	x: 0.3 m η = 47.2	x: 0.3 m η = 40.3	x: 0.3 m η = 36.2	CUMPLE η = 47.2
N644/N652	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.6	η = 0.7	η = 0.4	x: 0.3 m η = 10.9	x: 0 m η = 19.1	x: 0 m η = 6.2	x: 0 m η = 1.7	x: 0.3 m η = 11.0	x: 0 m η = 19.3	x: 0.3 m η = 1.2	x: 0 m η = 4.1	x: 0.3 m η = 37.3	x: 0.3 m η = 28.0	x: 0.3 m η = 27.0	CUMPLE η = 37.3
N645/N653	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 0.6	x: 0 m η = 0.7	η = 0.3	x: 0 m η = 7.6	x: 0.3 m η = 4.5	x: 0.3 m η = 1.2	x: 0 m η = 1.2	x: 0 m η = 7.7	x: 0.3 m η = 4.6	x: 0 m η = 0.6	x: 0.3 m η = 0.2	x: 0 m η = 11.6	x: 0 m η = 11.3	x: 0 m η = 10.8	CUMPLE η = 11.6
N646/N654	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 0.9	η = 1.0	η = 0.4	x: 0 m η = 9.7	x: 0.3 m η = 31.1	x: 0.3 m η = 10.2	x: 0 m η = 2.1	x: 0 m η = 9.8	x: 0.3 m η = 31.2	x: 0 m η = 1.0	x: 0.3 m η = 10.8	x: 0 m η = 48.0	x: 0 m η = 40.6	x: 0.3 m η = 40.0	CUMPLE η = 48.0
N647/N655	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.15 m η = 2.0	x: 0.15 m η = 2.2	η = 0.3	x: 0.3 m η = 4.5	x: 0.3 m η = 15.9	x: 0.15 m η = 5.3	x: 0 m η = 1.4	x: 0.3 m η = 4.6	x: 0.3 m η = 16.0	x: 0.3 m η = 0.2	x: 0.3 m η = 2.8	x: 0.3 m η = 24.7	x: 0.3 m η = 21.5	x: 0.3 m η = 21.9	CUMPLE η = 24.7
N648/N656	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.3 m η = 0.5	x: 0.3 m η = 0.5	x: 0.3 m η = 0.8	x: 0 m η = 4.6	x: 0.3 m η = 13.8	x: 0.3 m η = 4.6	x: 0 m η = 1.4	x: 0 m η = 4.8	x: 0.3 m η = 14.0	x: 0 m η = 0.2	x: 0.3 m η = 2.2	x: 0 m η = 23.4	x: 0 m η = 16.7	x: 0 m η = 18.3	CUMPLE η = 23.4
N649/N657	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.15 m η = 1.9	x: 0.15 m η = 2.2	η = 0.8	x: 0 m η = 5.6	x: 0.3 m η = 6.8	x: 0.3 m η = 2.2	x: 0 m η = 1.7	x: 0 m η = 5.9	x: 0.3 m η = 6.9	x: 0 m η = 0.4	x: 0.3 m η = 0.5	x: 0 m η = 16.7	x: 0 m η = 13.1	x: 0 m η = 11.8	CUMPLE η = 16.7
N650/N658	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.15 m η = 0.4	x: 0.15 m η = 0.5	η = 0.6	x: 0.3 m η = 2.4	x: 0 m η = 28.7	x: 0.15 m η = 9.6	x: 0 m η = 0.5	x: 0.3 m η = 2.4	x: 0 m η = 28.8	x: 0.3 m η = 0.1	x: 0 m η = 9.2	x: 0 m η = 39.0	x: 0 m η = 30.5	x: 0 m η = 36.3	CUMPLE η = 39.0
N570/N666	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.473 m η = 16.5	x: 0.473 m η = 19.8	x: 0.63 m η = 1.1	x: 0 m η = 5.7	x: 0 m η = 2.7	x: 0.473 m η = 0.2	x: 0.63 m η = 0.6	x: 0 m η = 6.1	x: 0 m η = 3.1	x: 0 m η = 0.4	x: 0 m η = 0.1	x: 0 m η = 27.9	x: 0 m η = 27.0	x: 0 m η = 26.6	CUMPLE η = 27.9
N666/N665	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 12.5	η = 15.2	η = 0.2	x: 0 m η = 1.9	x: 0 m η = 1.2	η = 0.1	x: 0 m η = 0.2	x: 0 m η = 1.9	x: 0 m η = 1.3	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 18.2	x: 0 m η = 17.7	CUMPLE η = 18.2
N665/N664	$w/t \leq (w/t)_{Máx.}$ Cumple	η = 8.6	η = 10.9	η = 0.4	x: 0 m η = 1.4	x: 0.63 m η = 1.2	η = 0.1	x: 0 m η = 0.2	x: 0 m η = 1.6	x: 0.63 m η = 1.3	x: 0 m η < 0.1	x: 0.63 m η < 0.1	N.P.(1)	x: 0 m η = 12.9	x: 0 m η = 12.6	CUMPLE η = 12.9

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N664/N663	$w/t \leq (w/t)_{Máx}$ Cumple	$\eta = 4.8$	$\eta = 6.4$	$\eta = 0.5$	x: 0 m $\eta = 1.4$	x: 0.63 m $\eta = 1.0$	$\eta = 0.1$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 1.6$	x: 0.63 m $\eta = 1.2$	x: 0 m $\eta < 0.1$	x: 0.63 m $\eta < 0.1$	N.P.(1)	x: 0 m $\eta = 8.6$	x: 0 m $\eta = 8.2$	CUMPLE $\eta = 8.6$
N663/N662	$w/t \leq (w/t)_{Máx}$ Cumple	$\eta = 1.1$	$\eta = 1.8$	x: 0 m $\eta = 0.5$	x: 0 m $\eta = 1.4$	x: 0.63 m $\eta = 1.1$	$\eta < 0.1$	x: 0.63 m $\eta = 0.2$	x: 0 m $\eta = 1.6$	x: 0.63 m $\eta = 1.4$	x: 0 m $\eta < 0.1$	x: 0.63 m $\eta < 0.1$	N.P.(1)	x: 0 m $\eta = 4.6$	x: 0 m $\eta = 3.9$	CUMPLE $\eta = 4.6$
N662/N661	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.473 m $\eta = 2.4$	x: 0.473 m $\eta = 3.1$	$\eta = 0.5$	x: 0 m $\eta = 1.2$	x: 0 m $\eta = 1.3$	$\eta < 0.1$	x: 0.63 m $\eta = 0.2$	x: 0 m $\eta = 1.4$	x: 0 m $\eta = 1.6$	x: 0 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.(1)	x: 0.63 m $\eta = 4.8$	x: 0 m $\eta = 4.6$	CUMPLE $\eta = 4.8$
N661/N660	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.315 m $\eta = 6.4$	x: 0.315 m $\eta = 7.3$	$\eta = 0.5$	x: 0.63 m $\eta = 2.2$	x: 0 m $\eta = 1.4$	x: 0.473 m $\eta = 0.1$	x: 0.63 m $\eta = 0.3$	x: 0.63 m $\eta = 2.4$	x: 0 m $\eta = 1.7$	x: 0.63 m $\eta = 0.1$	x: 0 m $\eta < 0.1$	N.P.(1)	x: 0.63 m $\eta = 10.9$	x: 0.63 m $\eta = 10.1$	CUMPLE $\eta = 10.9$
N660/N659	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0 m $\eta = 10.6$	x: 0 m $\eta = 11.8$	x: 0.63 m $\eta = 0.3$	x: 0.63 m $\eta = 1.8$	x: 0 m $\eta = 1.5$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 0.2$	x: 0.63 m $\eta = 1.9$	x: 0 m $\eta = 1.6$	x: 0.63 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.(1)	x: 0.63 m $\eta = 14.4$	x: 0.63 m $\eta = 13.9$	CUMPLE $\eta = 14.4$
N659/N508	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0 m $\eta = 13.6$	x: 0 m $\eta = 14.0$	$\eta = 1.6$	x: 0.49 m $\eta = 10.1$	x: 0.49 m $\eta = 5.1$	$\eta = 0.5$	x: 0.49 m $\eta = 1.1$	x: 0.49 m $\eta = 10.8$	x: 0.49 m $\eta = 5.7$	x: 0.49 m $\eta = 1.2$	x: 0.49 m $\eta = 0.3$	x: 0.49 m $\eta = 34.2$	x: 0.49 m $\eta = 24.4$	x: 0.49 m $\eta = 27.6$	CUMPLE $\eta = 34.2$
N569/N667	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.49 m $\eta = 20.0$	x: 0.49 m $\eta = 22.1$	$\eta = 1.4$	x: 0 m $\eta = 37.0$	x: 0 m $\eta = 14.1$	x: 0.49 m $\eta = 1.3$	x: 0.49 m $\eta = 5.2$	x: 0 m $\eta = 37.6$	x: 0 m $\eta = 14.7$	x: 0 m $\eta = 14.4$	x: 0 m $\eta = 2.2$	x: 0 m $\eta = 85.4$	x: 0 m $\eta = 72.1$	x: 0 m $\eta = 69.5$	CUMPLE $\eta = 85.4$
N667/N668	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.158 m $\eta = 17.2$	x: 0.158 m $\eta = 19.3$	$\eta = 0.1$	x: 0 m $\eta = 4.0$	x: 0 m $\eta = 2.8$	$\eta = 0.2$	x: 0 m $\eta = 0.5$	x: 0 m $\eta = 4.0$	x: 0 m $\eta = 2.8$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 0.1$	N.P.(1)	x: 0 m $\eta = 23.9$	x: 0 m $\eta = 23.5$	CUMPLE $\eta = 23.9$
N668/N669	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.63 m $\eta = 13.5$	x: 0.63 m $\eta = 14.6$	x: 0.63 m $\eta = 0.4$	x: 0 m $\eta = 2.3$	x: 0 m $\eta = 1.7$	x: 0.473 m $\eta = 0.2$	x: 0 m $\eta = 0.3$	x: 0 m $\eta = 2.5$	x: 0 m $\eta = 1.8$	x: 0 m $\eta = 0.1$	x: 0 m $\eta < 0.1$	N.P.(1)	x: 0 m $\eta = 18.8$	x: 0 m $\eta = 18.0$	CUMPLE $\eta = 18.8$
N669/N670	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.315 m $\eta = 9.7$	x: 0.315 m $\eta = 10.1$	x: 0.473 m $\eta = 0.5$	x: 0 m $\eta = 1.3$	x: 0 m $\eta = 1.4$	$\eta = 0.1$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 1.5$	x: 0 m $\eta = 1.6$	x: 0 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.(1)	x: 0 m $\eta = 13.1$	x: 0 m $\eta = 12.4$	CUMPLE $\eta = 13.1$
N670/N671	$w/t \leq (w/t)_{Máx}$ Cumple	$\eta = 5.9$	$\eta = 5.6$	$\eta = 0.5$	x: 0 m $\eta = 1.3$	x: 0.63 m $\eta = 1.6$	$\eta = 0.1$	x: 0.63 m $\eta = 0.2$	x: 0 m $\eta = 1.5$	x: 0.63 m $\eta = 1.8$	x: 0 m $\eta < 0.1$	x: 0.63 m $\eta < 0.1$	N.P.(1)	x: 0 m $\eta = 8.4$	x: 0.63 m $\eta = 8.1$	CUMPLE $\eta = 8.4$
N671/N672	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.315 m $\eta = 2.1$	x: 0.315 m $\eta = 1.2$	x: 0 m $\eta = 0.5$	x: 0 m $\eta = 1.2$	x: 0.63 m $\eta = 1.7$	$\eta = 0.1$	x: 0.63 m $\eta = 0.2$	x: 0 m $\eta = 1.4$	x: 0.63 m $\eta = 2.0$	x: 0 m $\eta < 0.1$	x: 0.63 m $\eta < 0.1$	N.P.(1)	x: 0 m $\eta = 3.5$	x: 0.63 m $\eta = 4.5$	CUMPLE $\eta = 4.5$
N672/N673	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.315 m $\eta = 2.8$	x: 0.315 m $\eta = 2.3$	x: 0.315 m $\eta = 0.5$	x: 0.63 m $\eta = 1.6$	x: 0.63 m $\eta = 1.8$	$\eta = 0.2$	x: 0.63 m $\eta = 0.3$	x: 0.63 m $\eta = 1.8$	x: 0.63 m $\eta = 2.0$	x: 0.63 m $\eta < 0.1$	x: 0.63 m $\eta < 0.1$	N.P.(1)	x: 0.63 m $\eta = 6.1$	x: 0.63 m $\eta = 5.4$	CUMPLE $\eta = 6.1$
N673/N674	$w/t \leq (w/t)_{Máx}$ Cumple	$\eta = 6.3$	$\eta = 7.0$	$\eta = 0.3$	x: 0.63 m $\eta = 3.0$	x: 0.63 m $\eta = 2.3$	$\eta = 0.1$	x: 0.63 m $\eta = 0.3$	x: 0.63 m $\eta = 3.1$	x: 0.63 m $\eta = 2.4$	x: 0.63 m $\eta = 0.1$	x: 0.63 m $\eta = 0.1$	N.P.(1)	x: 0.63 m $\eta = 11.1$	x: 0.63 m $\eta = 11.0$	CUMPLE $\eta = 11.1$
N674/N507	$w/t \leq (w/t)_{Máx}$ Cumple	$\eta = 10.0$	$\eta = 12.0$	x: 0 m $\eta = 1.5$	x: 0.63 m $\eta = 30.8$	x: 0.63 m $\eta = 11.1$	$\eta = 0.8$	x: 0.63 m $\eta = 3.4$	x: 0.63 m $\eta = 31.5$	x: 0.63 m $\eta = 11.4$	x: 0.63 m $\eta = 10.0$	x: 0.63 m $\eta = 1.3$	x: 0.63 m $\eta = 61.8$	x: 0.63 m $\eta = 52.4$	x: 0.63 m $\eta = 51.8$	CUMPLE $\eta = 61.8$
N507/N659	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.929 m $\eta = 3.7$	x: 0 m $\eta = 5.9$	x: 0.697 m $\eta = 1.8$	x: 0 m $\eta = 18.8$	x: 0 m $\eta = 10.7$	x: 0.697 m $\eta = 0.7$	x: 0.929 m $\eta = 1.5$	x: 0 m $\eta = 19.5$	x: 0 m $\eta = 11.0$	x: 0 m $\eta = 3.8$	x: 0 m $\eta = 1.2$	x: 0 m $\eta = 40.8$	x: 0 m $\eta = 35.5$	x: 0 m $\eta = 32.5$	CUMPLE $\eta = 40.8$
N674/N659	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.802 m $\eta = 4.4$	x: 0 m $\eta = 4.6$	$\eta = 0.4$	x: 0.802 m $\eta = 4.4$	x: 0 m $\eta = 4.9$	x: 0.602 m $\eta = 0.6$	x: 0 m $\eta = 0.6$	x: 0.802 m $\eta = 4.5$	x: 0 m $\eta = 4.9$	x: 0.802 m $\eta = 0.2$	x: 0 m $\eta = 0.2$	N.P.(1)	x: 0 m $\eta = 13.3$	x: 0 m $\eta = 12.4$	CUMPLE $\eta = 13.3$
N674/N660	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.929 m $\eta = 5.5$	x: 0 m $\eta = 8.4$	x: 0.929 m $\eta = 0.4$	x: 0 m $\eta = 3.1$	x: 0 m $\eta = 0.4$	$\eta < 0.1$	x: 0.929 m $\eta = 0.3$	x: 0 m $\eta = 3.3$	x: 0 m $\eta = 0.4$	x: 0 m $\eta = 0.1$	x: 0 m $\eta < 0.1$	N.P.(1)	x: 0 m $\eta = 11.8$	x: 0 m $\eta = 12.3$	CUMPLE $\eta = 12.3$
N673/N660	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.802 m $\eta = 5.2$	x: 0 m $\eta = 5.8$	x: 0.602 m $\eta = 0.6$	x: 0.802 m $\eta = 0.5$	x: 0 m $\eta = 0.8$	$\eta = 0.1$	x: 0 m $\eta = 0.1$	x: 0.802 m $\eta = 0.7$	x: 0 m $\eta = 1.1$	x: 0.802 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.(1)	x: 0 m $\eta = 7.2$	x: 0 m $\eta = 6.7$	CUMPLE $\eta = 7.2$
N673/N661	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.929 m $\eta = 5.2$	x: 0 m $\eta = 7.8$	$\eta = 0.2$	x: 0.929 m $\eta = 0.9$	x: 0 m $\eta = 0.3$	x: 0.929 m $\eta < 0.1$	x: 0.929 m $\eta = 0.1$	x: 0.929 m $\eta = 1.0$	x: 0 m $\eta = 0.3$	x: 0.929 m $\eta < 0.1$	$\eta < 0.1$	N.P.(1)	x: 0.929 m $\eta = 8.9$	x: 0.929 m $\eta = 8.8$	CUMPLE $\eta = 8.9$
N672/N661	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.802 m $\eta = 5.0$	x: 0 m $\eta = 5.8$	x: 0.401 m $\eta = 0.6$	x: 0.802 m $\eta = 1.3$	x: 0 m $\eta = 1.2$	$\eta = 0.1$	x: 0 m $\eta = 0.2$	x: 0.802 m $\eta = 1.6$	x: 0 m $\eta = 1.5$	x: 0.802 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.(1)	x: 0 m $\eta = 8.2$	x: 0.802 m $\eta = 7.6$	CUMPLE $\eta = 8.2$
N672/N662	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.929 m $\eta = 5.4$	x: 0 m $\eta = 7.7$	$\eta = 0.3$	x: 0.929 m $\eta = 0.7$	x: 0 m $\eta = 0.6$	$\eta < 0.1$	x: 0.929 m $\eta = 0.1$	x: 0.929 m $\eta = 0.8$	x: 0 m $\eta = 0.7$	x: 0.929 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.(1)	x: 0 m $\eta = 8.8$	x: 0.929 m $\eta = 8.6$	CUMPLE $\eta = 8.8$
N671/N662	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.802 m $\eta = 4.9$	x: 0 m $\eta = 5.9$	x: 0.401 m $\eta = 0.6$	x: 0.802 m $\eta = 1.2$	x: 0 m $\eta = 1.0$	$\eta = 0.1$	x: 0 m $\eta = 0.1$	x: 0.802 m $\eta = 1.5$	x: 0 m $\eta = 1.3$	x: 0.802 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.(1)	x: 0 m $\eta = 8.0$	x: 0.802 m $\eta = 7.5$	CUMPLE $\eta = 8.0$
N671/N663	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.929 m $\eta = 5.4$	x: 0 m $\eta = 7.6$	x: 0.465 m $\eta = 0.4$	x: 0.929 m $\eta = 0.7$	x: 0 m $\eta = 0.7$	$\eta < 0.1$	x: 0.929 m $\eta = 0.1$	x: 0.929 m $\eta = 0.8$	x: 0 m $\eta = 0.8$	x: 0.929 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.(1)	x: 0 m $\eta = 8.7$	x: 0 m $\eta = 8.5$	CUMPLE $\eta = 8.7$
N670/N663	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.802 m $\eta = 4.8$	x: 0 m $\eta = 6.0$	$\eta = 0.5$	x: 0.802 m $\eta = 1.3$	x: 0 m $\eta = 1.0$	$\eta = 0.1$	x: 0 m $\eta = 0.1$	x: 0.802 m $\eta = 1.5$	x: 0 m $\eta = 1.2$	x: 0.802 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.(1)	x: 0.802 m $\eta = 8.0$	x: 0.802 m $\eta = 7.7$	CUMPLE $\eta = 8.0$
N670/N664	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.929 m $\eta = 5.5$	x: 0 m $\eta = 7.4$	$\eta = 0.5$	x: 0 m $\eta = 0.7$	x: 0 m $\eta = 0.7$	$\eta < 0.1$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 0.9$	x: 0 m $\eta = 0.9$	x: 0 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.(1)	x: 0 m $\eta = 8.7$	x: 0 m $\eta = 8.5$	CUMPLE $\eta = 8.7$
N669/N664	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.802 m $\eta = 4.7$	x: 0 m $\eta = 6.1$	$\eta = 0.4$	x: 0.802 m $\eta = 1.3$	x: 0 m $\eta = 1.0$	$\eta = 0.1$	x: 0 m $\eta = 0.1$	x: 0.802 m $\eta = 1.4$	x: 0 m $\eta = 1.2$	x: 0.802 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.(1)	x: 0.802 m $\eta = 8.2$	x: 0.802 m $\eta = 7.9$	CUMPLE $\eta = 8.2$
N669/N665	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.929 m $\eta = 5.6$	x: 0 m $\eta = 7.3$	$\eta = 0.5$	x: 0 m $\eta = 0.9$	x: 0 m $\eta = 0.8$	$\eta < 0.1$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 1.1$	x: 0 m $\eta = 1.0$	x: 0 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.(1)	x: 0 m $\eta = 9.1$	x: 0 m $\eta = 8.7$	CUMPLE $\eta = 9.1$
N668/N665	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.802 m $\eta = 4.6$	x: 0 m $\eta = 6.2$	$\eta = 0.2$	x: 0.802 m $\eta = 1.2$	x: 0 m $\eta = 0.6$	$\eta = 0.1$	x: 0 m $\eta = 0.1$	x: 0.802 m $\eta = 1.2$	x: 0 m $\eta = 0.6$	x: 0.802 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.(1)	x: 0.802 m $\eta = 8.0$	x: 0.802 m $\eta = 7.7$	CUMPLE $\eta = 8.0$
N668/N666	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.929 m $\eta = 5.9$	x: 0 m $\eta = 7.5$	x: 0.929 m $\eta = 0.6$	x: 0 m $\eta = 0.4$	x: 0 m $\eta = 0.8$	$\eta = 0.1$	x: 0 m $\eta < 0.1$	x: 0 m $\eta = 0.5$	x: 0 m $\eta = 1.0$	x: 0 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.(1)	x: 0 m $\eta = 8.9$	x: 0 m $\eta = 8.5$	CUMPLE $\eta = 8.9$
N667/N666	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.802 m $\eta = 4.7$	x: 0 m $\eta = 6.4$	$\eta = 0.5$	x: 0 m $\eta = 4.8$	x: 0 m $\eta = 3.1$	$\eta = 0.3$	x: 0 m $\eta = 0.5$	x: 0 m $\eta = 5.0$	x: 0 m $\eta = 3.3$	x: 0 m $\eta = 0.3$	x: 0 m $\eta = 0.1$	N.P.(1)	x: 0 m $\eta = 13.8$	x: 0 m $\eta = 12.9$	CUMPLE $\eta = 13.8$
N667/N570	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.929 m $\eta = 4.1$	x: 0 m $\eta = 4.7$	$\eta = 0.6$	x: 0 m $\eta = 3.3$	x: 0.929 m $\eta = 3.4$	$\eta = 0.3$	x: 0.929 m $\eta = 0.1$	x: 0 m $\eta = 3.5$	x: 0.929 m $\eta = 3.6$	x: 0 m $\eta = 0.1$	x: 0.929 m $\eta = 0.1$	N.P.(1)	x: 0 m $\eta = 10.1$	x: 0 m $\eta = 9.5$	CUMPLE $\eta = 10.1$
N561/N675	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.315 m $\eta = 17.5$	x: 0.315 m $\eta = 21.1$	$\eta = 2.0$	x: 0 m $\eta = 7.1$	x: 0 m $\eta = 26.5$	x: 0.315 m $\eta = 2.4$	x: 0.63 m $\eta = 0.8$	x: 0 m $\eta = 7.4$	x: 0 m $\eta = 27.3$	x: 0 m $\eta = 0.6$	x: 0 m $\eta = 7.5$	x: 0 m $\eta = 43.0$	x: 0 m $\eta = 32.3$	x: 0 m $\eta = 35.6$	CUMPLE $\eta = 43.0$
N675/N676	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0 m $\eta = 13.3$	x: 0 m $\eta = 16.4$	$\eta = 0.7$	x: 0 m $\eta = 1.8$	x: 0 m $\eta = 2.5$	x: 0.315 m $\eta = 0.1$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 1.9$	x: 0 m $\eta = 2.7$	x: 0 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	N.P.(1)	x: 0 m $\eta = 19.7$	x: 0 m $\eta = 19.1$	CUMPLE $\eta = 19.7$
N676/N677	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.63 m $\eta = 9.4$	x: 0.63 m $\eta = 11.9$	x: 0.315 m $\eta = 1.6$	x: 0 m $\eta = 1.5$	x: 0.63 m $\eta = 4.5$	$\eta = 0.1$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 1.7$	x: 0.63 m $\eta = 5.2$	x: 0 m $\eta < 0.1$	x: 0.63 m $\eta = 0.3$	N.P.(1)	x: 0 m $\eta = 14.3$	x: 0 m $\eta = 13.8$	CUMPLE $\eta = 14.3$
N677/N678	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.473 m $\eta = 5.5$	x: 0.473 m $\eta = 7.3$	x: 0 m $\eta = 1.8$	x: 0 m $\eta = 1.5$	x: 0.63 m $\eta = 7.4$	$\eta = 0.1$	x: 0.63 m $\eta = 0.2$	x: 0 m $\eta = 1.8$	x: 0.63 m $\eta = 8.1$	x: 0 m $\eta < 0.1$	x: 0.63 m $\eta = 0.7$	x: 0.63 m $\eta = 12.7$	x: 0 m $\eta = 10.1$	x: 0.63 m $\eta = 9.7$	CUMPLE $\eta = 12.7$
N678/N679	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.473 m $\eta = 1.7$	x: 0.473 m $\eta = 2.5$	x: 0 m $\eta = 0.9$	x: 0 m $\eta = 1.5$	x: 0 m $\eta = 7.8$	$\eta < 0.1$	x: 0.63 m $\eta = 0.2$	x: 0 m $\eta = 1.7$	x: 0 m $\eta = 8.2$	x: 0 m $\eta < 0.1$	x: 0 m $\eta = 0.7$	x: 0.158 m $\eta = 12.3$	x: 0 m $\eta = 9.0$	x: 0 m $\eta = 10.0$	CUMPLE $\eta = 12.3$
N679/N680	$w/t \leq (w/t)_{Máx}$ Cumple	x: 0.158 m $\eta = 2.0$	x: 0.158 m $\eta = 2.6$	x: 0.473 m $\eta = 0.6$	x: 0 m $\eta = 1.3$	x: 0 m $\eta = 6.6$	$\eta = 0.2$	x: 0.63 m $\eta = 0.2$	x: 0 m $\eta = 1.5$	x: 0 m $\eta = 6.8$	x: 0 m $\eta < 0.1$	x: 0 m $\eta = 0.5$	x: 0 m $\eta = 10.4$	x: 0 m $\eta = 7.3$	x: 0 m $\eta = 8.7$	CUMPLE $\eta = 10.4$

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_z	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N680/N681	$w/t \leq (w/t)_{Max}$ Cumple	x: 0 m η = 6.1	x: 0 m η = 7.0	x: 0.473 m η = 1.1	x: 0.63 m η = 2.2	x: 0 m η = 2.4	η = 0.3	x: 0.63 m η = 0.3	x: 0.63 m η = 2.5	x: 0 m η = 2.8	x: 0.63 m η = 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0.63 m η = 10.6	x: 0.63 m η = 9.7	CUMPLE η = 10.6
N681/N682	$w/t \leq (w/t)_{Max}$ Cumple	η = 10.4	η = 11.5	x: 0.315 m η = 1.3	x: 0.63 m η = 1.7	x: 0.63 m η = 7.4	η = 0.4	x: 0 m η = 0.2	x: 0.63 m η = 1.8	x: 0.63 m η = 8.0	x: 0.63 m η < 0.1	x: 0.63 m η = 0.6	x: 0.63 m η = 11.3	x: 0.158 m η = 14.0	x: 0.158 m η = 13.7	CUMPLE η = 14.0
N682/N500	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.245 m η = 13.5	x: 0.245 m η = 13.8	x: 0.245 m η = 2.1	x: 0.49 m η = 10.5	x: 0.49 m η = 10.2	x: 0.245 m η = 0.5	x: 0.49 m η = 1.2	x: 0.49 m η = 11.4	x: 0.49 m η = 10.9	x: 0.49 m η = 1.3	x: 0.49 m η = 1.2	x: 0.49 m η = 36.8	x: 0.49 m η = 25.9	x: 0.49 m η = 28.8	CUMPLE η = 36.8
N560/N690	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.49 m η = 20.9	x: 0.49 m η = 23.0	x: 0.245 m η = 1.4	x: 0 m η = 36.5	x: 0 m η = 15.6	x: 0.245 m η = 1.4	x: 0.49 m η = 5.1	x: 0 m η = 37.1	x: 0 m η = 17.1	x: 0 m η = 14.0	x: 0 m η = 2.9	x: 0 m η = 86.5	x: 0 m η = 73.5	x: 0 m η = 70.1	CUMPLE η = 86.5
N690/N689	$w/t \leq (w/t)_{Max}$ Cumple	η = 18.0	η = 20.3	x: 0.473 m η = 0.6	x: 0 m η = 4.1	x: 0 m η = 8.6	x: 0 m η = 0.8	x: 0 m η = 0.5	x: 0 m η = 4.2	x: 0 m η = 8.8	x: 0 m η = 0.2	x: 0 m η = 0.8	x: 0 m η = 16.7	x: 0 m η = 26.3	x: 0 m η = 25.3	CUMPLE η = 26.3
N689/N688	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.315 m η = 14.2	x: 0.315 m η = 15.5	x: 0 m η = 1.4	x: 0 m η = 2.3	x: 0.63 m η = 5.1	x: 0 m η = 0.5	x: 0 m η = 0.3	x: 0 m η = 2.6	x: 0.63 m η = 5.7	x: 0 m η = 0.1	x: 0.63 m η = 0.3	N.P.[1]	x: 0 m η = 20.3	x: 0 m η = 19.2	CUMPLE η = 20.3
N688/N687	$w/t \leq (w/t)_{Max}$ Cumple	x: 0 m η = 10.3	x: 0 m η = 10.8	x: 0.158 m η = 1.8	x: 0 m η = 1.3	x: 0.63 m η = 8.0	x: 0.158 m η = 0.4	x: 0 m η = 0.2	x: 0.63 m η = 2.0	x: 0.63 m η = 8.8	x: 0.63 m η < 0.1	x: 0.63 m η = 0.8	x: 0.63 m η = 14.4	x: 0 m η = 14.2	x: 0 m η = 13.6	CUMPLE η = 14.4
N687/N686	$w/t \leq (w/t)_{Max}$ Cumple	η = 6.4	η = 6.2	x: 0 m η = 1.6	x: 0.63 m η = 1.7	x: 0 m η = 11.7	x: 0 m η = 0.4	x: 0.63 m η = 0.2	x: 0.63 m η = 2.3	x: 0.63 m η = 12.4	x: 0.63 m η = 0.1	x: 0.63 m η = 1.5	x: 0.63 m η = 19.2	x: 0.63 m η = 14.2	x: 0.63 m η = 15.6	CUMPLE η = 19.2
N686/N685	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.63 m η = 2.4	x: 0.63 m η = 1.7	x: 0.473 m η = 0.6	x: 0 m η = 1.9	x: 0 m η = 12.9	x: 0.473 m η = 0.8	x: 0.63 m η = 0.2	x: 0 m η = 1.9	x: 0 m η = 13.0	x: 0 m η < 0.1	x: 0 m η = 1.7	x: 0 m η = 19.4	x: 0 m η = 5.4	x: 0 m η = 17.2	CUMPLE η = 19.4
N685/N684	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.315 m η = 2.5	x: 0.315 m η = 2.2	x: 0.63 m η = 1.1	x: 0.63 m η = 1.6	x: 0 m η = 6.4	x: 0.63 m η = 0.7	x: 0.63 m η = 0.3	x: 0.63 m η = 1.8	x: 0 m η = 6.9	x: 0.63 m η < 0.1	x: 0 m η = 0.5	x: 0 m η = 11.1	x: 0 m η = 7.1	x: 0 m η = 8.9	CUMPLE η = 11.1
N684/N683	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.473 m η = 6.1	x: 0.473 m η = 7.0	x: 0.473 m η = 1.5	x: 0.63 m η = 2.9	x: 0.63 m η = 7.3	x: 0.158 m η = 0.6	x: 0.63 m η = 0.3	x: 0.63 m η = 3.1	x: 0.63 m η = 8.0	x: 0.63 m η = 0.1	x: 0.63 m η = 0.6	x: 0.63 m η = 14.0	x: 0.63 m η = 11.1	x: 0.63 m η = 10.8	CUMPLE η = 14.0
N683/N499	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.158 m η = 10.0	x: 0.158 m η = 12.2	η = 2.0	x: 0.63 m η = 30.9	x: 0.63 m η = 14.3	x: 0.158 m η = 0.9	x: 0.63 m η = 3.4	x: 0.63 m η = 31.6	x: 0.63 m η = 15.1	x: 0.63 m η = 10.1	x: 0.63 m η = 2.3	x: 0.63 m η = 62.7	x: 0.63 m η = 53.3	x: 0.63 m η = 52.0	CUMPLE η = 62.7
N690/N561	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 4.2	x: 0 m η = 4.9	x: 0.697 m η = 4.5	x: 0 m η = 3.0	x: 0.929 m η = 4.6	x: 0.465 m η = 0.3	x: 0.929 m η = 0.1	x: 0.929 m η = 3.7	x: 0.929 m η = 6.5	x: 0.929 m η = 0.1	x: 0.929 m η = 0.4	N.P.[1]	x: 0 m η = 10.4	x: 0.929 m η = 9.5	CUMPLE η = 10.4
N690/N675	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 4.8	x: 0 m η = 6.5	x: 0.201 m η = 2.1	x: 0 m η = 4.8	x: 0 m η = 3.4	x: 0.401 m η = 0.3	x: 0 m η = 0.5	x: 0 m η = 5.1	x: 0 m η = 3.5	x: 0 m η = 0.3	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 14.1	x: 0 m η = 13.2	CUMPLE η = 14.1
N689/N675	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 6.0	x: 0 m η = 7.7	η = 0.7	x: 0 m η = 0.7	x: 0 m η = 1.6	x: 0.232 m η = 0.2	x: 0 m η = 0.1	x: 0 m η = 0.7	x: 0 m η = 1.7	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 9.5	x: 0 m η = 9.1	CUMPLE η = 9.5
N689/N676	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 4.8	x: 0 m η = 6.3	η = 1.2	x: 0.802 m η = 1.2	x: 0.802 m η = 1.2	η = 0.1	x: 0 m η = 0.1	x: 0.802 m η = 1.6	x: 0.802 m η = 1.7	x: 0.802 m η < 0.1	x: 0.802 m η < 0.1	N.P.[1]	x: 0.802 m η = 8.1	x: 0.802 m η = 7.9	CUMPLE η = 8.1
N688/N676	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 5.7	x: 0 m η = 7.5	x: 0.465 m η = 0.6	x: 0 m η = 0.9	x: 0 m η = 1.0	x: 0.929 m η < 0.1	x: 0 m η = 0.1	x: 0 m η = 1.2	x: 0 m η = 1.2	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 9.5	x: 0 m η = 9.0	CUMPLE η = 9.5
N688/N677	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 4.9	x: 0.201 m η = 6.2	x: 0 m η = 2.1	x: 0.802 m η = 1.4	x: 0.802 m η = 1.1	x: 0.201 m η = 0.1	x: 0 m η = 0.1	x: 0.802 m η = 1.9	x: 0.802 m η = 2.0	x: 0.802 m η < 0.1	x: 0.802 m η < 0.1	N.P.[1]	x: 0.802 m η = 8.4	x: 0.802 m η = 8.1	CUMPLE η = 8.4
N687/N677	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 5.7	x: 0 m η = 7.7	η = 1.5	x: 0 m η = 0.7	x: 0 m η = 0.8	η < 0.1	x: 0 m η = 0.1	x: 0 m η = 1.0	x: 0 m η = 1.1	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 9.1	x: 0 m η = 8.8	CUMPLE η = 9.1
N687/N678	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 5.0	x: 0.201 m η = 6.1	x: 0.802 m η = 2.7	x: 0.802 m η = 1.3	x: 0 m η = 1.1	x: 0.401 m η = 0.1	x: 0 m η = 0.1	x: 0 m η = 2.0	x: 0 m η = 2.2	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0.802 m η = 8.3	x: 0.802 m η = 7.9	CUMPLE η = 8.3
N686/N678	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.465 m η = 5.6	x: 0 m η = 7.8	x: 0.697 m η = 2.8	x: 0.929 m η = 0.7	x: 0 m η = 2.1	x: 0.697 m η = 0.1	x: 0.929 m η = 0.1	x: 0 m η = 1.7	x: 0 m η = 3.3	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 9.3	x: 0 m η = 9.0	CUMPLE η = 9.3
N686/N679	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 5.1	x: 0.201 m η = 6.1	x: 0.401 m η = 2.0	x: 0.802 m η = 1.3	x: 0 m η = 1.2	x: 0.401 m η = 0.1	x: 0 m η = 0.1	x: 0 m η = 1.8	x: 0 m η = 2.0	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 8.3	x: 0.802 m η = 7.8	CUMPLE η = 8.3
N685/N679	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 5.5	x: 0 m η = 8.0	x: 0.465 m η = 2.6	x: 0.929 m η = 0.8	x: 0 m η = 2.2	x: 0.929 m η < 0.1	x: 0.929 m η = 0.1	x: 0.232 m η = 1.7	x: 0 m η = 3.4	x: 0.232 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 9.2	x: 0 m η = 9.2	CUMPLE η = 9.2
N685/N680	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 5.1	x: 0.401 m η = 6.0	x: 0.401 m η = 0.6	x: 0.802 m η = 1.4	x: 0 m η = 1.3	x: 0.602 m η = 0.1	x: 0 m η = 0.2	x: 0.802 m η = 1.7	x: 0 m η = 1.5	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 8.4	x: 0.802 m η = 7.8	CUMPLE η = 8.4
N684/N680	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 5.4	x: 0 m η = 8.0	x: 0 m η = 0.9	x: 0.929 m η = 0.9	x: 0.929 m η = 1.2	η < 0.1	x: 0.929 m η = 0.1	x: 0.929 m η = 1.0	x: 0.929 m η = 1.6	x: 0.929 m η < 0.1	x: 0.929 m η < 0.1	N.P.[1]	x: 0.929 m η = 9.1	x: 0.929 m η = 9.1	CUMPLE η = 9.1
N684/N681	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 5.3	x: 0 m η = 6.0	x: 0 m η = 1.3	x: 0.802 m η = 0.8	x: 0 m η = 0.9	x: 0 m η = 0.1	x: 0 m η = 0.1	x: 0.802 m η = 1.4	x: 0.802 m η = 1.4	x: 0.802 m η < 0.1	x: 0.802 m η < 0.1	N.P.[1]	x: 0 m η = 7.6	x: 0 m η = 7.0	CUMPLE η = 7.6
N683/N681	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 5.6	x: 0 m η = 8.7	x: 0.465 m η = 1.0	x: 0 m η = 3.2	x: 0 m η = 0.4	η < 0.1	x: 0.929 m η = 0.3	x: 0 m η = 3.4	x: 0.929 m η = 0.8	x: 0 m η = 0.1	x: 0.929 m η < 0.1	N.P.[1]	x: 0 m η = 12.1	x: 0 m η = 12.6	CUMPLE η = 12.6
N683/N682	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.401 m η = 4.5	x: 0.401 m η = 4.8	x: 0.401 m η = 2.4	x: 0.802 m η = 4.3	x: 0 m η = 4.9	x: 0.602 m η = 0.6	x: 0 m η = 0.5	x: 0.802 m η = 4.4	x: 0 m η = 4.9	x: 0.802 m η = 0.2	x: 0 m η = 0.2	N.P.[1]	x: 0 m η = 13.4	x: 0 m η = 12.6	CUMPLE η = 13.4
N499/N682	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 3.8	x: 0 m η = 6.2	x: 0.697 m η = 3.7	x: 0 m η = 18.7	x: 0 m η = 11.1	η = 0.8	x: 0.929 m η = 1.5	x: 0 m η = 19.6	x: 0 m η = 11.5	x: 0 m η = 3.9	x: 0 m η = 1.3	x: 0 m η = 41.7	x: 0 m η = 36.4	x: 0 m η = 32.9	CUMPLE η = 41.7
N243/N698	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.315 m η = 11.4	x: 0.315 m η = 12.3	η = 1.1	x: 0 m η = 6.5	x: 0 m η = 7.6	η = 0.3	x: 0 m η = 0.7	x: 0 m η = 6.9	x: 0 m η = 7.8	x: 0 m η = 0.5	x: 0 m η = 0.6	x: 0 m η = 25.5	x: 0 m η = 20.0	x: 0 m η = 20.8	CUMPLE η = 25.5
N698/N697	$w/t \leq (w/t)_{Max}$ Cumple	η = 8.7	η = 9.6	x: 0 m η = 0.9	x: 0 m η = 1.2	x: 0 m η = 4.8	x: 0 m η = 0.2	x: 0 m η = 0.1	x: 0 m η = 1.3	x: 0 m η = 5.2	x: 0 m η < 0.1	x: 0 m η = 0.3	N.P.[1]	x: 0 m η = 11.0	x: 0 m η = 10.8	CUMPLE η = 11.0
N697/N696	$w/t \leq (w/t)_{Max}$ Cumple	η = 6.3	η = 7.0	x: 0 m η = 0.9	x: 0 m η = 0.7	x: 0 m η = 3.2	x: 0 m η = 0.2	x: 0 m η = 0.1	x: 0 m η = 0.9	x: 0 m η = 3.6	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 8.3	x: 0 m η = 7.9	CUMPLE η = 8.3
N696/N695	$w/t \leq (w/t)_{Max}$ Cumple	η = 4.0	η = 4.3	η = 0.8	x: 0 m η = 0.8	x: 0 m η = 2.5	η = 0.2	x: 0 m η = 0.1	x: 0 m η = 1.0	x: 0 m η = 2.9	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 6.2	x: 0 m η = 5.6	CUMPLE η = 6.2
N695/N694	$w/t \leq (w/t)_{Max}$ Cumple	x: 0 m η = 1.8	x: 0 m η = 1.7	x: 0.158 m η = 0.7	x: 0 m η = 0.8	x: 0.63 m η = 2.3	η = 0.2	x: 0.63 m η = 0.1	x: 0 m η = 1.0	x: 0.63 m η = 2.6	x: 0 m η < 0.1	x: 0.63 m η = 0.1	N.P.[1]	x: 0 m η = 4.0	x: 0.63 m η = 3.6	CUMPLE η = 4.0
N694/N693	$w/t \leq (w/t)_{Max}$ Cumple	η = 1.6	η = 0.9	x: 0.63 m η = 0.6	x: 0 m η = 0.7	x: 0.63 m η = 3.2	x: 0.63 m η = 0.2	x: 0.63 m η = 0.1	x: 0 m η = 0.9	x: 0.63 m η = 3.4	x: 0 m η < 0.1	x: 0.63 m η = 0.1	N.P.[1]	x: 0.63 m η = 3.6	x: 0.63 m η = 4.9	CUMPLE η = 4.9
N693/N692	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.473 m η = 3.6	x: 0.473 m η = 3.3	x: 0.315 m η = 0.5	x: 0.63 m η = 1.7	x: 0.63 m η = 4.0	x: 0.158 m η = 0.3	x: 0.63 m η = 0.2	x: 0.63 m η = 1.9	x: 0.63 m η = 4.2	x: 0.63 m η < 0.1	x: 0.63 m η = 0.2	N.P.[1]	x: 0.473 m η = 5.6	x: 0.63 m η = 5.9	CUMPLE η = 5.9
N692/N691	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.158 m η = 6.1	x: 0.158 m η = 5.8	η = 0.3	x: 0.63 m η = 1.8	x: 0.63 m η = 6.0	η = 0.3	x: 0 m η = 0.2	x: 0.63 m η = 1.8	x: 0.63 m η = 6.1	x: 0.63 m η < 0.1	x: 0.63 m η = 0.4	x: 0.63 m η = 9.6	x: 0.63 m η = 7.9	x: 0.63 m η = 8.9	CUMPLE η = 9.6
N691/N150	$w/t \leq (w/t)_{Max}$ Cumple	η = 7.5	η = 6.6	η = 1.5	x: 0.49 m η = 7.4	x: 0.49 m η = 7.4	x: 0.245 m η = 0.5	x: 0.49 m η = 0.9	x: 0.49 m η = 8.0	x: 0.49 m η = 7.4	x: 0.49 m η = 0.6	x: 0.49 m η = 0.6	x: 0.49 m η = 25.5	x: 0.49 m η = 15.0	x: 0.49 m η = 19.1	CUMPLE η = 25.5

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N242/N699	$w/t \leq (w/t)_{Máx.}$ Cumple	$\eta = 7.8$	$\eta = 9.0$	$\eta = 2.0$	x: 0 m $\eta = 39.2$	x: 0 m $\eta = 14.0$	$\eta = 1.3$	x: 0.49 m $\eta = 5.5$	x: 0 m $\eta = 39.6$	x: 0 m $\eta = 14.4$	x: 0 m $\eta = 16.0$	x: 0 m $\eta = 2.1$	x: 0 m $\eta = 75.1$	x: 0 m $\eta = 59.4$	x: 0 m $\eta = 59.6$	CUMPLE $\eta = 75.1$
N699/N700	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.473 m $\eta = 6.7$	x: 0.473 m $\eta = 7.6$	x: 0.473 m $\eta = 0.9$	x: 0 m $\eta = 5.6$	x: 0 m $\eta = 4.7$	x: 0.473 m $\eta = 0.1$	x: 0 m $\eta = 0.6$	x: 0 m $\eta = 5.6$	x: 0 m $\eta = 5.1$	x: 0 m $\eta = 0.3$	x: 0 m $\eta = 0.3$	x: 0 m $\eta = 16.9$	x: 0 m $\eta = 13.1$	x: 0 m $\eta = 14.4$	CUMPLE $\eta = 16.9$
N700/N701	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.315 m $\eta = 4.6$	x: 0.315 m $\eta = 4.7$	x: 0.315 m $\eta = 0.9$	x: 0 m $\eta = 1.7$	x: 0 m $\eta = 2.8$	x: 0.315 m $\eta = 0.2$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 1.9$	x: 0 m $\eta = 3.1$	x: 0 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	N.P.[1]	x: 0 m $\eta = 8.0$	x: 0 m $\eta = 7.3$	CUMPLE $\eta = 8.0$
N701/N702	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.158 m $\eta = 2.5$	x: 0.158 m $\eta = 2.0$	x: 0.158 m $\eta = 0.8$	x: 0 m $\eta = 0.6$	x: 0 m $\eta = 2.1$	x: 0.158 m $\eta = 0.1$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 0.8$	x: 0 m $\eta = 2.4$	x: 0 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	N.P.[1]	x: 0 m $\eta = 4.0$	x: 0.63 m $\eta = 3.9$	CUMPLE $\eta = 4.0$
N702/N703	$w/t \leq (w/t)_{Máx.}$ Cumple	$\eta = 1.3$	$\eta = 0.3$	$\eta = 0.7$	x: 0 m $\eta = 0.6$	x: 0.63 m $\eta = 1.4$	x: 0.158 m $\eta = 0.1$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 0.8$	x: 0.63 m $\eta = 1.6$	x: 0 m $\eta < 0.1$	x: 0.63 m $\eta < 0.1$	N.P.[1]	x: 0.63 m $\eta = 2.0$	x: 0 m $\eta = 2.6$	CUMPLE $\eta = 2.6$
N703/N704	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m $\eta = 3.1$	x: 0 m $\eta = 2.7$	x: 0.473 m $\eta = 0.6$	x: 0 m $\eta = 0.6$	x: 0 m $\eta = 1.8$	x: 0.315 m $\eta = 0.1$	x: 0.63 m $\eta = 0.1$	x: 0 m $\eta = 0.8$	x: 0 m $\eta = 2.1$	x: 0 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.[1]	x: 0.63 m $\eta = 4.8$	x: 0 m $\eta = 4.7$	CUMPLE $\eta = 4.8$
N704/N705	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.315 m $\eta = 5.2$	x: 0.315 m $\eta = 5.4$	$\eta = 0.5$	x: 0.63 m $\eta = 1.1$	x: 0 m $\eta = 2.8$	x: 0.315 m $\eta = 0.1$	x: 0.63 m $\eta = 0.2$	x: 0.63 m $\eta = 1.3$	x: 0 m $\eta = 3.0$	x: 0.63 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	N.P.[1]	x: 0.63 m $\eta = 8.1$	x: 0.63 m $\eta = 7.5$	CUMPLE $\eta = 8.1$
N705/N706	$w/t \leq (w/t)_{Máx.}$ Cumple	$\eta = 7.2$	$\eta = 8.2$	$\eta = 0.5$	x: 0.63 m $\eta = 3.4$	x: 0.63 m $\eta = 3.8$	$\eta = 0.1$	x: 0.63 m $\eta = 0.4$	x: 0.63 m $\eta = 3.5$	x: 0.63 m $\eta = 4.0$	x: 0.63 m $\eta = 0.1$	x: 0.63 m $\eta = 0.2$	N.P.[1]	x: 0.63 m $\eta = 12.3$	x: 0.63 m $\eta = 12.1$	CUMPLE $\eta = 12.3$
N706/N149	$w/t \leq (w/t)_{Máx.}$ Cumple	$\eta = 9.4$	$\eta = 11.2$	x: 0.158 m $\eta = 1.3$	x: 0.63 m $\eta = 29.5$	x: 0.63 m $\eta = 10.4$	$\eta = 0.7$	x: 0.63 m $\eta = 3.3$	x: 0.63 m $\eta = 30.0$	x: 0.63 m $\eta = 10.6$	x: 0.63 m $\eta = 9.1$	x: 0.63 m $\eta = 1.1$	x: 0.63 m $\eta = 58.5$	x: 0.63 m $\eta = 49.2$	x: 0.63 m $\eta = 49.1$	CUMPLE $\eta = 58.5$
N706/N691	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.602 m $\eta = 2.4$	x: 0 m $\eta = 2.2$	$\eta = 0.7$	x: 0 m $\eta = 3.6$	x: 0 m $\eta = 4.1$	x: 0.602 m $\eta = 0.5$	x: 0 m $\eta = 0.5$	x: 0 m $\eta = 3.6$	x: 0 m $\eta = 4.1$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 0.2$	N.P.[1]	x: 0 m $\eta = 9.4$	x: 0 m $\eta = 9.2$	CUMPLE $\eta = 9.4$
N706/N692	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m $\eta = 3.3$	x: 0 m $\eta = 5.3$	$\eta = 1.6$	x: 0 m $\eta = 3.0$	x: 0 m $\eta = 1.4$	$\eta < 0.1$	x: 0.929 m $\eta = 0.3$	x: 0 m $\eta = 3.1$	x: 0 m $\eta = 2.0$	x: 0 m $\eta = 0.1$	x: 0 m $\eta < 0.1$	N.P.[1]	x: 0 m $\eta = 8.7$	x: 0 m $\eta = 8.8$	CUMPLE $\eta = 8.8$
N705/N692	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m $\eta = 3.2$	x: 0 m $\eta = 3.5$	$\eta = 0.5$	x: 0 m $\eta = 0.3$	x: 0 m $\eta = 0.4$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	x: 0 m $\eta = 0.5$	x: 0 m $\eta = 0.6$	x: 0 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.[1]	x: 0 m $\eta = 4.3$	x: 0 m $\eta = 3.9$	CUMPLE $\eta = 4.3$
N705/N693	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m $\eta = 3.1$	x: 0 m $\eta = 4.7$	x: 0 m $\eta = 1.2$	x: 0.929 m $\eta = 0.7$	x: 0 m $\eta = 1.0$	$\eta < 0.1$	x: 0.929 m $\eta = 0.1$	x: 0.465 m $\eta = 0.9$	x: 0 m $\eta = 1.6$	x: 0.465 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.[1]	x: 0.929 m $\eta = 5.4$	x: 0.929 m $\eta = 5.5$	CUMPLE $\eta = 5.5$
N704/N693	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m $\eta = 3.0$	x: 0 m $\eta = 3.4$	x: 0.401 m $\eta = 0.5$	x: 0.802 m $\eta = 0.8$	x: 0 m $\eta = 0.8$	x: 0.401 m $\eta = 0.1$	x: 0 m $\eta = 0.1$	x: 0.802 m $\eta = 1.0$	x: 0 m $\eta = 1.0$	x: 0.802 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.[1]	x: 0 m $\eta = 4.8$	x: 0.802 m $\eta = 4.4$	CUMPLE $\eta = 4.8$
N704/N694	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m $\eta = 3.2$	x: 0 m $\eta = 4.6$	x: 0.697 m $\eta = 0.9$	x: 0.929 m $\eta = 0.6$	x: 0 m $\eta = 0.9$	x: 0.697 m $\eta < 0.1$	x: 0.929 m $\eta = 0.1$	x: 0.929 m $\eta = 0.8$	x: 0 m $\eta = 1.3$	x: 0.929 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.[1]	x: 0 m $\eta = 5.4$	x: 0.929 m $\eta = 5.4$	CUMPLE $\eta = 5.4$
N703/N694	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m $\eta = 2.9$	x: 0 m $\eta = 3.5$	x: 0.401 m $\eta = 0.6$	x: 0.802 m $\eta = 0.7$	x: 0 m $\eta = 0.6$	x: 0.401 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	x: 0.802 m $\eta = 0.9$	x: 0 m $\eta = 0.8$	x: 0.802 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.[1]	x: 0 m $\eta = 4.6$	x: 0 m $\eta = 4.3$	CUMPLE $\eta = 4.6$
N703/N695	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m $\eta = 3.3$	x: 0 m $\eta = 4.5$	x: 0 m $\eta = 0.6$	x: 0.929 m $\eta = 0.6$	x: 0 m $\eta = 0.7$	$\eta < 0.1$	x: 0 m $\eta = 0.1$	x: 0.929 m $\eta = 0.7$	x: 0 m $\eta = 1.0$	x: 0.929 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.[1]	x: 0 m $\eta = 5.3$	x: 0.929 m $\eta = 5.1$	CUMPLE $\eta = 5.3$
N702/N695	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m $\eta = 2.8$	x: 0 m $\eta = 3.6$	x: 0 m $\eta = 0.6$	x: 0.802 m $\eta = 0.7$	x: 0 m $\eta = 0.6$	$\eta < 0.1$	x: 0 m $\eta = 0.1$	x: 0.802 m $\eta = 0.9$	x: 0 m $\eta = 0.8$	x: 0.802 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.[1]	x: 0 m $\eta = 4.7$	x: 0.802 m $\eta = 4.5$	CUMPLE $\eta = 4.7$
N702/N696	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m $\eta = 3.3$	x: 0 m $\eta = 4.3$	$\eta = 0.4$	x: 0.929 m $\eta = 0.5$	x: 0 m $\eta = 0.6$	x: 0.465 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	x: 0.929 m $\eta = 0.7$	x: 0 m $\eta = 0.8$	x: 0.929 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.[1]	x: 0 m $\eta = 5.2$	x: 0 m $\eta = 5.0$	CUMPLE $\eta = 5.2$
N701/N696	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m $\eta = 2.8$	x: 0 m $\eta = 3.7$	x: 0.602 m $\eta = 1.0$	x: 0.802 m $\eta = 0.7$	x: 0 m $\eta = 0.7$	$\eta = 0.1$	x: 0 m $\eta = 0.1$	x: 0.802 m $\eta = 1.0$	x: 0 m $\eta = 1.0$	x: 0.802 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.[1]	x: 0 m $\eta = 4.9$	x: 0.802 m $\eta = 4.7$	CUMPLE $\eta = 4.9$
N701/N697	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m $\eta = 3.4$	x: 0 m $\eta = 4.2$	$\eta = 0.6$	x: 0 m $\eta = 0.6$	x: 0 m $\eta = 0.7$	$\eta < 0.1$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 0.8$	x: 0 m $\eta = 0.9$	x: 0 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.[1]	x: 0 m $\eta = 5.4$	x: 0 m $\eta = 5.1$	CUMPLE $\eta = 5.4$
N700/N697	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m $\eta = 2.6$	x: 0 m $\eta = 3.8$	$\eta = 1.2$	x: 0.802 m $\eta = 0.6$	x: 0 m $\eta = 0.5$	$\eta < 0.1$	x: 0.802 m $\eta < 0.1$	x: 0 m $\eta = 1.0$	x: 0 m $\eta = 1.0$	x: 0 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.[1]	x: 0.802 m $\eta = 4.6$	x: 0.802 m $\eta = 4.5$	CUMPLE $\eta = 4.6$
N700/N698	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m $\eta = 3.7$	x: 0 m $\eta = 4.4$	x: 0.465 m $\eta = 1.0$	x: 0 m $\eta = 0.3$	x: 0 m $\eta = 0.6$	x: 0.697 m $\eta = 0.1$	x: 0 m $\eta = 0.1$	x: 0.929 m $\eta = 0.6$	x: 0 m $\eta = 0.9$	x: 0 m $\eta < 0.1$	x: 0 m $\eta < 0.1$	N.P.[1]	x: 0 m $\eta = 5.7$	x: 0 m $\eta = 5.3$	CUMPLE $\eta = 5.7$
N699/N698	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m $\eta = 2.7$	x: 0 m $\eta = 4.0$	$\eta = 1.5$	x: 0 m $\eta = 4.7$	x: 0 m $\eta = 3.3$	x: 0.401 m $\eta = 0.3$	x: 0 m $\eta = 0.5$	x: 0 m $\eta = 5.0$	x: 0 m $\eta = 3.5$	x: 0 m $\eta = 0.3$	x: 0 m $\eta = 0.1$	N.P.[1]	x: 0 m $\eta = 11.2$	x: 0 m $\eta = 10.4$	CUMPLE $\eta = 11.2$
N149/N691	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m $\eta = 1.6$	x: 0 m $\eta = 3.0$	$\eta = 2.2$	x: 0 m $\eta = 18.8$	x: 0 m $\eta = 9.8$	x: 0.697 m $\eta = 0.7$	x: 0.929 m $\eta = 1.5$	x: 0 m $\eta = 19.5$	x: 0 m $\eta = 10.0$	x: 0 m $\eta = 3.8$	x: 0 m $\eta = 1.0$	x: 0 m $\eta = 37.7$	x: 0 m $\eta = 31.6$	x: 0 m $\eta = 28.9$	CUMPLE $\eta = 37.7$
N699/N243	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m $\eta = 1.8$	x: 0 m $\eta = 1.4$	x: 0.465 m $\eta = 2.0$	x: 0 m $\eta = 3.2$	x: 0.929 m $\eta = 3.9$	$\eta = 0.3$	x: 0.929 m $\eta = 0.1$	x: 0 m $\eta = 3.3$	x: 0.929 m $\eta = 4.3$	x: 0 m $\eta = 0.1$	x: 0.929 m $\eta = 0.2$	N.P.[1]	x: 0.929 m $\eta = 6.5$	x: 0.929 m $\eta = 7.5$	CUMPLE $\eta = 7.5$
N471/N714	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.473 m $\eta = 7.4$	x: 0.473 m $\eta = 7.2$	x: 0.473 m $\eta = 1.3$	x: 0 m $\eta = 6.5$	x: 0 m $\eta = 7.2$	$\eta = 0.2$	x: 0 m $\eta = 0.7$	x: 0 m $\eta = 6.9$	x: 0 m $\eta = 7.5$	x: 0 m $\eta = 0.5$	x: 0 m $\eta = 0.6$	x: 0 m $\eta = 21.6$	x: 0 m $\eta = 15.0$	x: 0 m $\eta = 16.8$	CUMPLE $\eta = 21.6$
N714/N713	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.63 m $\eta = 5.0$	x: 0.63 m $\eta = 4.8$	x: 0 m $\eta = 0.9$	x: 0 m $\eta = 1.1$	x: 0 m $\eta = 4.6$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 1.2$	x: 0 m $\eta = 5.0$	x: 0 m $\eta < 0.1$	x: 0 m $\eta = 0.3$	N.P.[1]	x: 0 m $\eta = 6.2$	x: 0 m $\eta = 6.8$	CUMPLE $\eta = 6.8$
N713/N712	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.473 m $\eta = 2.9$	x: 0.473 m $\eta = 2.8$	x: 0 m $\eta = 0.8$	x: 0 m $\eta = 0.7$	x: 0 m $\eta = 3.0$	$\eta = 0.2$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 0.9$	x: 0 m $\eta = 3.4$	x: 0 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	N.P.[1]	x: 0 m $\eta = 3.9$	x: 0.63 m $\eta = 4.4$	CUMPLE $\eta = 4.4$
N712/N711	$w/t \leq (w/t)_{Máx.}$ Cumple	$\eta = 1.5$	$\eta = 0.6$	$\eta = 0.7$	x: 0 m $\eta = 0.7$	x: 0 m $\eta = 2.4$	$\eta = 0.2$	x: 0 m $\eta = 0.1$	x: 0 m $\eta = 0.9$	x: 0 m $\eta = 2.7$	x: 0 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	N.P.[1]	x: 0 m $\eta = 2.5$	x: 0 m $\eta = 3.5$	CUMPLE $\eta = 3.5$
N711/N710	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m $\eta = 1.6$	x: 0 m $\eta = 1.5$	$\eta = 0.7$	x: 0 m $\eta = 0.7$	x: 0.63 m $\eta = 2.2$	$\eta = 0.2$	x: 0.63 m $\eta = 0.1$	x: 0 m $\eta = 1.0$	x: 0.63 m $\eta = 2.5$	x: 0 m $\eta < 0.1$	x: 0.63 m $\eta = 0.1$	N.P.[1]	x: 0.63 m $\eta = 3.2$	x: 0 m $\eta = 3.3$	CUMPLE $\eta = 3.3$
N710/N709	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.473 m $\eta = 3.6$	x: 0.473 m $\eta = 3.7$	x: 0.63 m $\eta = 0.6$	x: 0 m $\eta = 0.6$	x: 0.63 m $\eta = 3.1$	$\eta = 0.2$	x: 0.63 m $\eta = 0.1$	x: 0 m $\eta = 0.9$	x: 0.63 m $\eta = 3.4$	x: 0 m $\eta < 0.1$	x: 0.63 m $\eta = 0.1$	N.P.[1]	x: 0.63 m $\eta = 4.9$	x: 0 m $\eta = 5.4$	CUMPLE $\eta = 5.4$
N709/N708	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.315 m $\eta = 5.6$	x: 0.315 m $\eta = 5.9$	x: 0.315 m $\eta = 0.5$	x: 0.63 m $\eta = 1.6$	x: 0.63 m $\eta = 3.8$	$\eta = 0.2$	x: 0.63 m $\eta = 0.2$	x: 0.63 m $\eta = 1.8$	x: 0.63 m $\eta = 4.0$	x: 0.63 m $\eta < 0.1$	x: 0.63 m $\eta = 0.2$	N.P.[1]	x: 0.63 m $\eta = 8.3$	x: 0.63 m $\eta = 7.8$	CUMPLE $\eta = 8.3$
N708/N707	$w/t \leq (w/t)_{Máx.}$ Cumple	$\eta = 7.9$	$\eta = 8.3$	$\eta = 0.2$	x: 0.63 m $\eta = 2.1$	x: 0.63 m $\eta = 5.8$	$\eta = 0.3$	x: 0 m $\eta = 0.2$	x: 0.63 m $\eta = 2.1$	x: 0.63 m $\eta = 5.9$	x: 0.63 m $\eta < 0.1$	x: 0.63 m $\eta = 0.3$	x: 0.63 m $\eta = 10.3$	x: 0.63 m $\eta = 10.5$	x: 0.63 m $\eta = 11.0$	CUMPLE $\eta = 11.0$
N707/N378	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.245 m $\eta = 6.9$	x: 0.245 m $\eta = 6.7$	$\eta = 1.5$	x: 0.49 m $\eta = 8.3$	x: 0.49 m $\eta = 6.9$	x: 0.245 m $\eta = 0.5$	x: 0.49 m $\eta = 0.9$	x: 0.49 m $\eta = 9.0$	x: 0.49 m $\eta = 7.1$	x: 0.49 m $\eta = 0.8$	x: 0.49 m $\eta = 0.5$	x: 0.49 m $\eta = 27.9$	x: 0.49 m $\eta = 17.8$	x: 0.49 m $\eta = 21.4$	CUMPLE $\eta = 27.9$
N470/N715	$w/t \leq (w/t)_{Máx.}$ Cumple	$\eta = 9.2$	$\eta = 11.1$	$\eta = 2.0$	x: 0 m $\eta = 40.0$	x: 0 m $\eta = 14.4$	$\eta = 1.4$	x: 0.49 m $\eta = 5.7$	x: 0 m $\eta = 40.5$	x: 0 m $\eta = 14.9$	x: 0 m $\eta = 16.7$	x: 0 m $\eta = 2.2$	x: 0 m $\eta = 78.2$	x: 0 m $\eta = 62.9$	x: 0 m $\eta = 62.2$	CUMPLE $\eta = 78.2$
N715/N716	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.63 m $\eta = 8.4$	x: 0.63 m $\eta = 10.0$	$\eta = 0.9$	x: 0 m $\eta = 5.8$	x: 0 m $\eta = 4.5$	x: 0.315 m $\eta = 0.1$	x: 0 m $\eta = 0.7$	x: 0 m $\eta = 5.8$	x: 0 m $\eta = 4.9$	x: 0 m $\eta = 0.3$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 18.8$	x: 0 m $\eta = 15.6$	x: 0 m $\eta = 16.2$	CUMPLE $\eta = 18.8$
N716/N717	$w/t \leq (w/t)_{Máx.}$ Cumple	$\eta = 6.7$	$\eta = 7.5$	x: 0.315 m $\eta = 0.8$	x: 0 m $\eta = 1.7$	x: 0 m $\eta = 2.7$	x: 0.158 m $\eta = 0.2$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 1.9$	x: 0 m $\eta = 3.0$	x: 0 m $\eta < 0.1$	x: 0 m $\eta = 0.1$	N.P.[1]	x: 0 m $\eta = 10.5$	x: 0 m $\eta = 9.9$	CUMPLE $\eta = 10.5$



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_z	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N717/N718	$w/t \leq (w/t)_{max}$ Cumple	x: 0.63 m η = 4.9	x: 0.63 m η = 5.0	η = 0.8	x: 0 m η = 0.5	x: 0 m η = 2.0	x: 0.158 m η = 0.1	x: 0 m η = 0.1	x: 0 m η = 0.8	x: 0 m η = 2.3	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.(1)	x: 0 m η = 6.9	x: 0 m η = 6.5	CUMPLE η = 6.9
N718/N719	$w/t \leq (w/t)_{max}$ Cumple	η = 3.0	η = 2.6	η = 0.7	x: 0 m η = 0.6	x: 0.63 m η = 1.4	x: 0.158 m η = 0.1	x: 0 m η = 0.1	x: 0 m η = 0.8	x: 0.63 m η = 1.6	x: 0 m η < 0.1	x: 0.63 m η < 0.1	N.P.(1)	x: 0 m η = 4.7	x: 0.63 m η = 4.8	CUMPLE η = 4.8
N719/N720	$w/t \leq (w/t)_{max}$ Cumple	η = 1.3	η = 0.3	x: 0.473 m η = 0.6	x: 0 m η = 0.5	x: 0 m η = 1.8	x: 0.315 m η = 0.1	x: 0.63 m η = 0.1	x: 0 m η = 0.7	x: 0 m η = 2.0	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0.315 m η = 2.3	x: 0.63 m η = 3.0	CUMPLE η = 3.0
N720/N721	$w/t \leq (w/t)_{max}$ Cumple	x: 0.315 m η = 1.8	x: 0.315 m η = 1.3	x: 0.315 m η = 0.5	x: 0.63 m η = 1.0	x: 0 m η = 2.8	η = 0.1	x: 0.63 m η = 0.2	x: 0.63 m η = 1.2	x: 0 m η = 3.0	x: 0.63 m η < 0.1	x: 0 m η = 0.1	N.P.(1)	x: 0.63 m η = 4.1	x: 0.63 m η = 3.8	CUMPLE η = 4.1
N721/N722	$w/t \leq (w/t)_{max}$ Cumple	x: 0 m η = 3.6	x: 0 m η = 3.6	η = 0.5	x: 0.63 m η = 3.6	x: 0.63 m η = 3.7	η = 0.1	x: 0.63 m η = 0.4	x: 0.63 m η = 3.7	x: 0.63 m η = 3.9	x: 0.63 m η = 0.1	x: 0.63 m η = 0.2	N.P.(1)	x: 0.63 m η = 8.1	x: 0.63 m η = 8.7	CUMPLE η = 8.7
N722/N377	$w/t \leq (w/t)_{max}$ Cumple	x: 0.158 m η = 5.5	x: 0.158 m η = 6.3	x: 0.63 m η = 1.4	x: 0.63 m η = 30.0	x: 0.63 m η = 10.5	η = 0.8	x: 0.63 m η = 3.3	x: 0.63 m η = 30.6	x: 0.63 m η = 10.8	x: 0.63 m η = 9.5	x: 0.63 m η = 1.2	x: 0.63 m η = 55.6	x: 0.63 m η = 45.1	x: 0.63 m η = 44.9	CUMPLE η = 55.6
N722/N707	$w/t \leq (w/t)_{max}$ Cumple	x: 0.802 m η = 1.9	x: 0 m η = 1.8	η = 0.7	x: 0 m η = 3.8	x: 0 m η = 4.3	x: 0.602 m η = 0.5	x: 0 m η = 0.5	x: 0 m η = 3.8	x: 0 m η = 4.3	x: 0 m η = 0.1	x: 0 m η = 0.2	N.P.(1)	x: 0 m η = 9.3	x: 0 m η = 9.0	CUMPLE η = 9.3
N722/N708	$w/t \leq (w/t)_{max}$ Cumple	x: 0.929 m η = 2.9	x: 0 m η = 4.6	x: 0.929 m η = 1.5	x: 0 m η = 2.9	x: 0 m η = 1.4	η < 0.1	x: 0 m η = 0.3	x: 0 m η = 3.0	x: 0 m η = 2.0	x: 0 m η = 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 7.6	x: 0 m η = 8.0	CUMPLE η = 8.0
N721/N708	$w/t \leq (w/t)_{max}$ Cumple	x: 0.802 m η = 2.7	x: 0 m η = 3.0	η = 0.5	x: 0 m η = 0.2	x: 0 m η = 0.4	x: 0 m η < 0.1	x: 0 m η < 0.1	x: 0 m η = 0.4	x: 0 m η = 0.6	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 3.9	x: 0.201 m η = 3.5	CUMPLE η = 3.9
N721/N709	$w/t \leq (w/t)_{max}$ Cumple	x: 0.929 m η = 2.7	x: 0 m η = 4.0	x: 0.929 m η = 1.1	x: 0.929 m η = 0.5	x: 0 m η = 1.0	η < 0.1	x: 0.929 m η < 0.1	x: 0.465 m η = 0.8	x: 0 m η = 1.5	x: 0.465 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0.929 m η = 4.6	x: 0.929 m η = 4.5	CUMPLE η = 4.6
N720/N709	$w/t \leq (w/t)_{max}$ Cumple	x: 0.802 m η = 2.5	x: 0 m η = 3.0	x: 0.401 m η = 0.6	x: 0.802 m η = 0.9	x: 0 m η = 0.8	x: 0.401 m η = 0.1	x: 0 m η = 0.1	x: 0.802 m η = 1.1	x: 0 m η = 1.1	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 4.5	x: 0.802 m η = 4.1	CUMPLE η = 4.5
N720/N710	$w/t \leq (w/t)_{max}$ Cumple	x: 0.929 m η = 2.8	x: 0 m η = 3.9	x: 0.465 m η = 0.9	x: 0.929 m η = 0.4	x: 0 m η = 0.9	η < 0.1	x: 0.929 m η = 0.1	x: 0.465 m η = 0.7	x: 0 m η = 1.3	x: 0.465 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0.929 m η = 4.5	x: 0.929 m η = 4.5	CUMPLE η = 4.5
N719/N710	$w/t \leq (w/t)_{max}$ Cumple	x: 0.802 m η = 2.5	x: 0 m η = 3.1	x: 0.401 m η = 0.6	x: 0.802 m η = 0.7	x: 0 m η = 0.7	x: 0.401 m η = 0.1	x: 0 m η = 0.1	x: 0.802 m η = 1.0	x: 0 m η = 0.9	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 4.4	x: 0 m η = 4.1	CUMPLE η = 4.4
N719/N711	$w/t \leq (w/t)_{max}$ Cumple	x: 0.929 m η = 2.9	x: 0 m η = 3.8	x: 0.697 m η = 0.6	x: 0.929 m η = 0.4	x: 0 m η = 0.7	η < 0.1	x: 0 m η = 0.1	x: 0.929 m η = 0.6	x: 0 m η = 0.9	x: 0.929 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 4.4	x: 0.929 m η = 4.3	CUMPLE η = 4.4
N718/N711	$w/t \leq (w/t)_{max}$ Cumple	x: 0.802 m η = 2.4	x: 0 m η = 3.2	x: 0 m η = 0.8	x: 0.802 m η = 0.8	x: 0 m η = 0.7	η = 0.1	x: 0.802 m η = 0.1	x: 0.802 m η = 1.0	x: 0 m η = 0.9	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 4.4	x: 0.802 m η = 4.2	CUMPLE η = 4.4
N718/N712	$w/t \leq (w/t)_{max}$ Cumple	x: 0.929 m η = 3.0	x: 0 m η = 3.7	x: 0.232 m η = 0.4	x: 0.929 m η = 0.3	x: 0 m η = 0.6	η < 0.1	x: 0 m η = 0.1	x: 0.929 m η = 0.5	x: 0 m η = 0.8	x: 0.929 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 4.3	x: 0 m η = 4.2	CUMPLE η = 4.3
N717/N712	$w/t \leq (w/t)_{max}$ Cumple	x: 0.802 m η = 2.3	x: 0 m η = 3.3	x: 0.602 m η = 1.0	x: 0.802 m η = 0.6	x: 0 m η = 0.7	η = 0.1	x: 0.802 m η = 0.1	x: 0.802 m η = 1.0	x: 0 m η = 1.0	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 4.7	x: 0.802 m η = 4.4	CUMPLE η = 4.7
N717/N713	$w/t \leq (w/t)_{max}$ Cumple	x: 0.929 m η = 3.1	x: 0 m η = 3.5	η = 0.6	x: 0 m η = 0.5	x: 0 m η = 0.6	η < 0.1	x: 0 m η = 0.1	x: 0 m η = 0.7	x: 0 m η = 0.8	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 4.6	x: 0 m η = 4.3	CUMPLE η = 4.6
N716/N713	$w/t \leq (w/t)_{max}$ Cumple	x: 0.802 m η = 2.2	x: 0 m η = 3.4	x: 0.201 m η = 1.1	x: 0.802 m η = 0.7	x: 0 m η = 0.6	x: 0 m η < 0.1	x: 0.802 m η < 0.1	x: 0 m η = 0.9	x: 0 m η = 1.0	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0.802 m η = 4.3	x: 0.802 m η = 4.2	CUMPLE η = 4.3
N716/N714	$w/t \leq (w/t)_{max}$ Cumple	x: 0.697 m η = 3.4	x: 0.697 m η = 3.7	x: 0.465 m η = 1.0	x: 0 m η = 0.5	x: 0 m η = 0.6	x: 0.697 m η = 0.1	x: 0 m η = 0.1	x: 0 m η = 0.7	x: 0 m η = 0.8	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.(1)	x: 0 m η = 5.2	x: 0 m η = 4.7	CUMPLE η = 5.2
N715/N714	$w/t \leq (w/t)_{max}$ Cumple	x: 0.802 m η = 2.2	x: 0 m η = 3.6	η = 1.4	x: 0 m η = 4.9	x: 0 m η = 3.3	x: 0.401 m η = 0.3	x: 0 m η = 0.5	x: 0 m η = 5.2	x: 0 m η = 3.5	x: 0 m η = 0.3	x: 0 m η = 0.1	N.P.(1)	x: 0 m η = 11.2	x: 0 m η = 10.3	CUMPLE η = 11.2
N377/N707	$w/t \leq (w/t)_{max}$ Cumple	x: 0.929 m η = 1.2	x: 0 m η = 2.2	η = 2.1	x: 0 m η = 19.4	x: 0 m η = 9.9	x: 0.697 m η = 0.7	x: 0.929 m η = 1.5	x: 0 m η = 20.1	x: 0 m η = 10.2	x: 0 m η = 4.1	x: 0 m η = 1.0	x: 0 m η = 38.1	x: 0 m η = 31.5	x: 0 m η = 28.8	CUMPLE η = 38.1
N715/N471	$w/t \leq (w/t)_{max}$ Cumple	x: 0.929 m η = 1.4	x: 0 m η = 0.6	x: 0.465 m η = 1.9	x: 0 m η = 3.1	x: 0.929 m η = 4.1	η = 0.3	x: 0.929 m η = 0.1	x: 0 m η = 3.2	x: 0.929 m η = 4.5	x: 0 m η = 0.1	x: 0.929 m η = 0.2	N.P.(1)	x: 0.929 m η = 6.2	x: 0.929 m η = 7.3	CUMPLE η = 7.3
N463/N723	$w/t \leq (w/t)_{max}$ Cumple	x: 0.315 m η = 8.2	x: 0.315 m η = 8.2	η = 1.2	x: 0 m η = 8.2	x: 0 m η = 15.9	η = 0.9	x: 0 m η = 0.9	x: 0 m η = 8.8	x: 0 m η = 16.1	x: 0 m η = 0.8	x: 0 m η = 2.6	x: 0 m η = 25.6	x: 0 m η = 17.5	x: 0 m η = 21.9	CUMPLE η = 25.6
N723/N724	$w/t \leq (w/t)_{max}$ Cumple	η = 5.4	η = 5.4	x: 0.315 m η = 0.8	x: 0 m η = 1.0	x: 0 m η = 6.6	η = 0.9	x: 0 m η = 0.2	x: 0 m η = 1.2	x: 0 m η = 6.8	x: 0 m η < 0.1	x: 0 m η = 0.5	x: 0 m η = 11.1	x: 0 m η = 7.2	x: 0 m η = 9.5	CUMPLE η = 11.1
N724/N725	$w/t \leq (w/t)_{max}$ Cumple	x: 0.473 m η = 3.0	x: 0.473 m η = 3.0	η = 1.1	x: 0 m η = 0.9	x: 0 m η = 5.6	η = 0.3	x: 0 m η = 0.1	x: 0 m η = 1.3	x: 0 m η = 6.0	x: 0 m η < 0.1	x: 0 m η = 0.4	x: 0.63 m η = 9.9	x: 0 m η = 7.5	x: 0.63 m η = 8.0	CUMPLE η = 9.9
N725/N726	$w/t \leq (w/t)_{max}$ Cumple	η = 1.3	x: 0.63 m η = 1.1	x: 0.63 m η = 1.3	x: 0.473 m η = 0.9	x: 0.63 m η_x = 6.5	η = 0.3	x: 0 m η = 0.2	x: 0.473 m η = 1.5	x: 0.63 m η = 7.1	x: 0.315 m η < 0.1	x: 0.63 m η = 0.5	x: 0.63 m η = 11.7	x: 0.63 m η = 8.0	x: 0.63 m η = 9.4	CUMPLE η = 11.7
N726/N727	$w/t \leq (w/t)_{max}$ Cumple	x: 0.158 m η = 2.3	x: 0.158 m η = 2.5	η = 0.8	x: 0.158 m η = 1.0	x: 0 m η = 6.7	η = 0.2	x: 0.63 m η = 0.2	x: 0.158 m η = 1.3	x: 0 m η = 7.0	x: 0.158 m η < 0.1	x: 0 m η = 0.5	x: 0 m η = 11.6	x: 0 m η = 8.0	x: 0 m η = 9.6	CUMPLE η = 11.6
N727/N736	$w/t \leq (w/t)_{max}$ Cumple	x: 0.158 m η = 4.7	x: 0.158 m η = 5.2	η = 0.7	x: 0 m η = 0.8	x: 0 m η = 5.5	η = 0.2	x: 0.63 m η = 0.1	x: 0 m η = 1.0	x: 0 m η = 5.7	x: 0 m η < 0.1	x: 0 m η = 0.3	x: 0 m η = 9.4	x: 0.63 m η = 6.6	x: 0 m η = 8.0	CUMPLE η = 9.4
N736/N737	$w/t \leq (w/t)_{max}$ Cumple	x: 0 m η = 7.1	x: 0 m η = 7.9	η = 0.9	x: 0.63 m η = 1.8	x: 0.63 m η = 4.1	η = 0.3	x: 0.63 m η = 0.3	x: 0.63 m η = 2.0	x: 0.63 m η = 4.3	x: 0.63 m η < 0.1	x: 0.63 m η = 0.2	N.P.(1)	x: 0.63 m η = 10.4	x: 0.63 m η = 9.9	CUMPLE η = 10.4
N737/N738	$w/t \leq (w/t)_{max}$ Cumple	η = 9.8	η = 10.7	η = 1.0	x: 0.63 m η = 1.8	x: 0.63 m η = 6.7	x: 0 m η = 0.4	x: 0 m η = 0.2	x: 0.63 m η = 1.9	x: 0.63 m η = 7.0	x: 0.63 m η < 0.1	x: 0.63 m η = 0.5	x: 0.63 m η = 11.0	x: 0.63 m η = 12.5	x: 0.63 m η = 13.1	CUMPLE η = 13.1
N738/N370	$w/t \leq (w/t)_{max}$ Cumple	x: 0.245 m η = 11.2	x: 0.245 m η = 11.4	x: 0.245 m η = 2.0	x: 0.49 m η = 8.5	x: 0.49 m η = 9.2	x: 0.245 m η = 0.5	x: 0.49 m η = 0.9	x: 0.49 m η = 9.3	x: 0.49 m η = 9.6	x: 0.49 m η = 0.9	x: 0.49 m η = 0.9	x: 0.49 m η = 32.3	x: 0.49 m η = 21.8	x: 0.49 m η = 24.7	CUMPLE η = 32.3
N462/N735	$w/t \leq (w/t)_{max}$ Cumple	x: 0.245 m η = 9.2	x: 0.245 m η = 11.3	η = 2.1	x: 0 m η = 39.4	x: 0 m η = 14.7	x: 0.245 m η = 1.4	x: 0.49 m η = 5.6	x: 0 m η = 39.9	x: 0 m η = 15.2	x: 0 m η = 16.2	x: 0 m η = 2.3	x: 0 m η = 77.9	x: 0 m η = 62.9	x: 0 m η = 61.6	CUMPLE η = 77.9
N735/N734	$w/t \leq (w/t)_{max}$ Cumple	x: 0.63 m η = 8.0	x: 0.63 m η = 9.7	x: 0.473 m η = 1.0	x: 0 m η = 5.8	x: 0 m η = 9.0	η = 0.8	x: 0 m η = 0.6	x: 0 m η = 5.8	x: 0 m η = 9.3	x: 0 m η = 0.3	x: 0 m η = 0.9	x: 0 m η = 18.1	x: 0 m η = 15.1	x: 0 m η = 15.7	CUMPLE η = 18.1
N734/N733	$w/t \leq (w/t)_{max}$ Cumple	η = 5.8	η = 6.7	x: 0 m η = 0.8	x: 0 m η = 1.8	x: 0 m η = 5.5	η = 0.4	x: 0 m η = 0.2	x: 0 m η = 2.0	x: 0 m η = 5.7	x: 0 m η < 0.1	x: 0 m η = 0.3	x: 0 m η = 9.1	x: 0 m η = 10.5	x: 0 m η = 9.8	CUMPLE η = 10.5
N733/N732	$w/t \leq (w/t)_{max}$ Cumple	η = 3.6	η = 3.8	x: 0.63 m η = 1.3	x: 0.63 m η = 1.0	x: 0.63 m η = 6.9	η = 0.3	x: 0 m η = 0.1	x: 0.63 m η = 1.5	x: 0.63 m η = 7.5	x: 0.63 m η < 0.1	x: 0.63 m η = 0.6	x: 0.63 m η = 12.1	x: 0.63 m η = 8.1	x: 0.63 m η = 9.6	CUMPLE η = 12.1
N732/N731	$w/t \leq (w/t)_{max}$ Cumple	η = 1.4	η = 0.9	x: 0.158 m η = 1.2	x: 0.63 m η = 1.3	x: 0.63 m η = 9.1	x: 0.63 m η = 0.3	x: 0 m η = 0.1	x: 0.63 m η = 1.7	x: 0.63 m η = 9.5	x: 0.63 m η < 0.1	x: 0.63 m η = 0.9	x: 0.63 m η = 14.7	x: 0.63 m η = 9.9	x: 0.63 m η = 12.1	CUMPLE η = 14.7
N731/N730	$w/t \leq (w/t)_{max}$ Cumple	x: 0.473 m η = 1.8	x: 0.473 m η = 1.3	η = 0.6	x: 0 m η = 1.4	x: 0 m η = 10.4	η = 0.6	x: 0.63 m η = 0.1	x: 0 m η = 1.5	x: 0 m η = 10.5	x: 0 m η < 0.1	x: 0 m η = 1.1	x: 0 m η = 15.6	x: 0 m η = 10.5	x: 0 m η = 13.8	CUMPLE η = 15.6

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N730/N729	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.473 m η = 4.1	x: 0.473 m η = 4.2	η = 0.9	x: 0.63 m η = 1.2	x: 0 m η = 5.5	η = 0.5	x: 0.63 m η = 0.2	x: 0.63 m η = 1.4	x: 0 m η = 5.9	x: 0.63 m η < 0.1	x: 0 m η = 0.4	x: 0 m η = 9.5	x: 0.63 m η = 7.1	x: 0 m η = 7.8	CUMPLE η = 9.5
N729/N728	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.158 m η = 6.3	x: 0.158 m η = 7.0	η = 1.2	x: 0.63 m η = 3.3	x: 0.63 m η = 5.9	η = 0.5	x: 0.63 m η = 0.4	x: 0.63 m η = 3.4	x: 0.63 m η = 6.3	x: 0.63 m η = 0.1	x: 0.63 m η = 0.4	x: 0.63 m η = 10.6	x: 0.63 m η = 10.8	x: 0.63 m η = 10.8	CUMPLE η = 10.8
N728/N369	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.158 m η = 8.6	x: 0.158 m η = 10.2	η = 1.8	x: 0.63 m η = 30.0	x: 0.63 m η = 11.5	x: 0.158 m η = 0.8	x: 0.63 m η = 3.3	x: 0.63 m η = 30.6	x: 0.63 m η = 12.1	x: 0.63 m η = 9.5	x: 0.63 m η = 1.5	x: 0.63 m η = 58.9	x: 0.63 m η = 49.0	x: 0.63 m η = 48.5	CUMPLE η = 58.9
N735/N723	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 2.7	x: 0 m η = 4.1	x: 0.401 m η = 2.0	x: 0 m η = 5.1	x: 0 m η = 3.4	x: 0.401 m η = 0.3	x: 0 m η = 0.5	x: 0 m η = 5.3	x: 0 m η = 3.6	x: 0 m η = 0.3	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 12.1	x: 0 m η = 11.2	CUMPLE η = 12.1
N734/N723	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 4.0	x: 0 m η = 4.5	x: 0 m η = 1.4	x: 0 m η = 0.4	x: 0 m η = 0.8	η = 0.1	x: 0 m η = 0.1	x: 0 m η = 0.9	x: 0 m η = 1.2	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 6.1	x: 0 m η = 5.5	CUMPLE η = 6.1
N734/N724	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 2.7	x: 0 m η = 4.0	x: 0.401 m η = 1.5	x: 0.802 m η = 0.8	x: 0 m η = 0.9	η = 0.1	x: 0.802 m η = 0.1	x: 0.802 m η = 1.0	x: 0.802 m η = 1.2	x: 0.802 m η < 0.1	x: 0.802 m η < 0.1	N.P.[1]	x: 0.802 m η = 5.1	x: 0.802 m η = 5.0	CUMPLE η = 5.1
N733/N724	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 3.6	x: 0 m η = 4.3	x: 0.465 m η = 1.5	x: 0 m η = 0.6	x: 0.929 m η = 0.9	η = 0.1	x: 0 m η = 0.1	x: 0.929 m η = 0.8	x: 0.929 m η = 1.4	x: 0.929 m η < 0.1	x: 0.929 m η < 0.1	N.P.[1]	x: 0 m η = 5.5	x: 0 m η = 5.2	CUMPLE η = 5.5
N733/N725	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 2.8	x: 0 m η = 4.0	x: 0.802 m η = 1.9	x: 0.802 m η = 0.9	x: 0.802 m η = 0.9	x: 0.802 m η = 0.1	x: 0.802 m η = 0.1	x: 0.802 m η = 1.6	x: 0.802 m η = 1.7	x: 0.802 m η < 0.1	x: 0.802 m η < 0.1	N.P.[1]	x: 0 m η = 5.4	x: 0.802 m η = 5.1	CUMPLE η = 5.4
N732/N725	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 3.6	x: 0 m η = 4.4	x: 0.465 m η = 1.7	x: 0.929 m η = 0.4	x: 0 m η = 0.6	η < 0.1	x: 0 m η = 0.1	x: 0.465 m η = 0.9	x: 0.465 m η = 1.1	x: 0.465 m η < 0.1	x: 0.465 m η < 0.1	N.P.[1]	x: 0 m η = 5.2	x: 0 m η = 5.1	CUMPLE η = 5.2
N732/N726	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 2.9	x: 0 m η = 3.8	η = 2.2	x: 0.802 m η = 0.9	x: 0 m η = 0.8	x: 0.401 m η = 0.1	x: 0.802 m η = 0.1	x: 0 m η = 1.5	x: 0 m η = 1.7	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 5.3	x: 0.802 m η = 4.9	CUMPLE η = 5.3
N731/N726	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 3.5	x: 0 m η = 4.5	η = 2.3	x: 0.929 m η = 0.5	x: 0 m η = 1.7	η = 0.1	x: 0 m η = 0.1	x: 0 m η = 1.4	x: 0 m η = 2.7	x: 0 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 5.5	x: 0 m η = 5.2	CUMPLE η = 5.5
N731/N727	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 2.9	x: 0 m η = 3.7	η = 1.6	x: 0.802 m η = 0.8	x: 0 m η = 0.9	η = 0.1	x: 0 m η = 0.1	x: 0 m η = 1.3	x: 0 m η = 1.6	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 5.3	x: 0 m η = 4.9	CUMPLE η = 5.3
N730/N727	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 3.4	x: 0 m η = 4.7	η = 2.2	x: 0.929 m η = 0.6	x: 0 m η = 1.9	η < 0.1	x: 0.929 m η = 0.1	x: 0.465 m η = 1.4	x: 0 m η = 2.8	x: 0.465 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0.929 m η = 5.4	x: 0.929 m η = 5.4	CUMPLE η = 5.4
N735/N463	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 1.9	x: 0 m η = 1.4	η = 4.1	x: 0.929 m η = 3.8	x: 0.929 m η = 4.7	x: 0.465 m η = 0.3	x: 0.929 m η = 0.1	x: 0.929 m η = 4.3	x: 0.929 m η = 6.4	x: 0.929 m η = 0.2	x: 0.929 m η = 0.4	N.P.[1]	x: 0.929 m η = 8.0	x: 0.929 m η = 9.1	CUMPLE η = 9.1
N730/N736	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 3.0	x: 0 m η = 3.6	x: 0.401 m η = 0.6	x: 0.802 m η = 0.9	x: 0 m η = 0.9	x: 0.802 m η = 0.1	x: 0 m η = 0.1	x: 0.802 m η = 1.2	x: 0 m η = 1.2	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 5.3	x: 0 m η = 4.8	CUMPLE η = 5.3
N729/N736	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 3.2	x: 0.232 m η = 4.7	η = 1.4	x: 0.929 m η = 0.6	x: 0 m η = 1.3	η < 0.1	x: 0.929 m η = 0.1	x: 0.465 m η = 1.0	x: 0 m η = 1.9	x: 0.465 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0.929 m η = 5.5	x: 0.929 m η = 5.5	CUMPLE η = 5.5
N729/N737	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 3.2	x: 0 m η = 3.7	η = 0.9	x: 0.802 m η = 0.6	x: 0.802 m η = 0.6	η < 0.1	x: 0 m η < 0.1	x: 0.802 m η = 1.0	x: 0.802 m η = 1.0	x: 0.802 m η < 0.1	x: 0.802 m η < 0.1	N.P.[1]	x: 0.201 m η = 4.7	x: 0.201 m η = 4.2	CUMPLE η = 4.7
N728/N737	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 3.5	x: 0 m η = 5.3	η = 1.6	x: 0 m η = 2.9	x: 0 m η = 1.3	η < 0.1	x: 0 m η = 0.3	x: 0 m η = 3.0	x: 0 m η = 2.0	x: 0 m η = 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 8.4	x: 0 m η = 8.8	CUMPLE η = 8.8
N728/N738	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.802 m η = 2.4	x: 0 m η = 2.4	η = 1.8	x: 0 m η = 3.8	x: 0 m η = 4.3	x: 0.401 m η = 0.5	x: 0 m η = 0.5	x: 0 m η = 3.8	x: 0 m η = 4.4	x: 0 m η = 0.2	x: 0 m η = 0.2	N.P.[1]	x: 0 m η = 10.0	x: 0 m η = 9.6	CUMPLE η = 10.0
N369/N738	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.929 m η = 1.8	x: 0 m η = 3.1	η = 3.2	x: 0 m η = 18.9	x: 0 m η = 10.1	x: 0.697 m η = 0.7	x: 0.929 m η = 1.5	x: 0 m η = 19.8	x: 0 m η = 10.5	x: 0 m η = 3.9	x: 0 m η = 1.1	x: 0 m η = 38.8	x: 0 m η = 32.4	x: 0 m η = 29.4	CUMPLE η = 38.8
N235/N739	$w/t \leq (w/t)_{Max}$ Cumple	η = 8.4	η = 8.9	η = 1.2	x: 0 m η = 7.2	x: 0 m η = 15.6	η = 0.8	x: 0 m η = 0.8	x: 0 m η = 7.7	x: 0 m η = 15.9	x: 0 m η = 0.6	x: 0 m η = 2.5	x: 0 m η = 24.7	x: 0 m η = 16.7	x: 0 m η = 20.8	CUMPLE η = 24.7
N739/N740	$w/t \leq (w/t)_{Max}$ Cumple	η = 5.9	η = 6.3	x: 0.315 m η = 0.9	x: 0 m η = 1.0	x: 0 m η = 6.8	η = 0.8	x: 0 m η = 0.1	x: 0 m η = 1.3	x: 0 m η = 7.0	x: 0 m η < 0.1	x: 0 m η = 0.5	x: 0 m η = 11.2	x: 0 m η = 7.8	x: 0 m η = 9.4	CUMPLE η = 11.2
N740/N741	$w/t \leq (w/t)_{Max}$ Cumple	η = 3.8	η = 4.1	η = 1.2	x: 0 m η = 0.9	x: 0.63 m η = 6.3	η = 0.3	x: 0 m η = 0.1	x: 0 m η = 1.4	x: 0.63 m η = 6.4	x: 0 m η < 0.1	x: 0.63 m η = 0.4	x: 0 m η = 10.1	x: 0 m η = 8.1	x: 0.63 m η = 8.5	CUMPLE η = 10.1
N741/N742	$w/t \leq (w/t)_{Max}$ Cumple	η = 1.6	η = 1.6	η = 1.0	x: 0.63 m η = 1.1	x: 0.63 m η = 8.9	η = 0.3	x: 0 m η = 0.1	x: 0.473 m η = 1.3	x: 0.63 m η = 9.0	x: 0.473 m η < 0.1	x: 0.63 m η = 0.8	x: 0.63 m η = 13.4	x: 0.63 m η = 9.2	x: 0.63 m η = 11.7	CUMPLE η = 13.4
N742/N743	$w/t \leq (w/t)_{Max}$ Cumple	η = 1.2	η = 1.0	η = 0.8	x: 0.158 m η = 1.1	x: 0 m η = 7.7	η = 0.3	x: 0.63 m η = 0.1	x: 0.158 m η = 1.4	x: 0 m η = 8.0	x: 0.158 m η < 0.1	x: 0 m η = 0.6	x: 0 m η = 12.2	x: 0 m η = 8.3	x: 0 m η = 10.3	CUMPLE η = 12.2
N743/N752	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.158 m η = 3.1	x: 0.158 m η = 3.3	η = 0.6	x: 0.158 m η = 1.0	x: 0 m η = 6.6	η = 0.3	x: 0.63 m η = 0.1	x: 0.158 m η = 1.1	x: 0 m η = 6.8	x: 0.158 m η < 0.1	x: 0 m η = 0.5	x: 0 m η = 10.6	x: 0 m η = 6.9	x: 0 m η = 9.1	CUMPLE η = 10.8
N752/N753	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.473 m η = 5.4	x: 0.473 m η = 5.6	x: 0.158 m η = 0.5	x: 0.63 m η = 1.7	x: 0 m η = 6.0	η = 0.6	x: 0.63 m η = 0.2	x: 0.63 m η = 1.9	x: 0 m η = 6.1	x: 0.63 m η < 0.1	x: 0 m η = 0.4	x: 0 m η = 10.0	x: 0.473 m η = 8.2	x: 0 m η = 8.6	CUMPLE η = 10.0
N753/N754	$w/t \leq (w/t)_{Max}$ Cumple	x: 0 m η = 8.0	x: 0 m η = 8.2	η = 0.4	x: 0.63 m η = 2.1	x: 0.63 m η = 9.8	η = 0.7	x: 0 m η = 0.2	x: 0.63 m η = 2.2	x: 0.63 m η = 9.9	x: 0.63 m η < 0.1	x: 0.63 m η = 1.0	x: 0.63 m η = 14.2	x: 0.63 m η = 10.6	x: 0.63 m η = 13.3	CUMPLE η = 14.2
N754/N142	$w/t \leq (w/t)_{Max}$ Cumple	η = 9.2	η = 8.7	x: 0.49 m η = 1.8	x: 0.49 m η = 8.9	x: 0.49 m η = 14.3	η = 0.8	x: 0.49 m η = 0.9	x: 0.49 m η = 9.7	x: 0.49 m η = 14.6	x: 0.49 m η = 0.9	x: 0.49 m η = 2.1	x: 0.49 m η = 30.9	x: 0.49 m η = 19.9	x: 0.49 m η = 23.2	CUMPLE η = 30.9
N234/N751	$w/t \leq (w/t)_{Max}$ Cumple	η = 10.6	η = 12.3	η = 2.1	x: 0 m η = 39.5	x: 0 m η = 15.0	x: 0.245 m η = 1.4	x: 0.49 m η = 5.6	x: 0 m η = 40.0	x: 0 m η = 15.5	x: 0 m η = 16.3	x: 0 m η = 2.4	x: 0 m η = 79.7	x: 0 m η = 64.2	x: 0 m η = 63.2	CUMPLE η = 79.7
N751/N750	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.63 m η = 9.6	x: 0.63 m η = 11.2	x: 0.63 m η = 0.8	x: 0 m η = 5.7	x: 0 m η = 8.8	η = 0.6	x: 0 m η = 0.6	x: 0 m η = 5.7	x: 0 m η = 9.1	x: 0 m η = 0.3	x: 0 m η = 0.8	x: 0 m η = 20.0	x: 0 m η = 16.8	x: 0 m η = 17.4	CUMPLE η = 20.0
N750/N749	$w/t \leq (w/t)_{Max}$ Cumple	η = 7.6	η = 8.5	η = 1.1	x: 0 m η = 1.8	x: 0.63 m η = 6.2	η = 0.6	x: 0 m η = 0.2	x: 0 m η = 2.0	x: 0.63 m η = 6.3	x: 0 m η < 0.1	x: 0.63 m η = 0.4	x: 0.63 m η = 9.1	x: 0 m η = 11.8	x: 0 m η = 11.1	CUMPLE η = 11.8
N749/N748	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.63 m η = 5.5	x: 0.63 m η = 5.8	η = 1.1	x: 0.473 m η = 1.0	x: 0.63 m η = 6.7	η = 0.1	x: 0 m η = 0.1	x: 0.473 m η = 1.2	x: 0.63 m η = 6.9	x: 0.473 m η < 0.1	x: 0.63 m η = 0.5	x: 0.63 m η = 10.2	x: 0 m η = 8.1	x: 0.63 m η = 8.6	CUMPLE η = 10.2
N748/N747	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.473 m η = 3.5	x: 0.473 m η = 3.3	η = 0.8	x: 0.315 m η = 1.1	x: 0.63 m η = 7.7	η = 0.1	x: 0 m η = 0.1	x: 0.315 m η = 1.4	x: 0.473 m η = 7.9	x: 0.315 m η < 0.1	x: 0.473 m η = 0.6	x: 0.473 m η = 11.7	x: 0.63 m η = 8.9	x: 0.63 m η = 9.8	CUMPLE η = 11.7
N747/N746	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.473 m η = 1.3	x: 0.473 m η = 0.8	η = 0.6	x: 0 m η = 1.2	x: 0 m η = 8.8	η = 0.3	x: 0.63 m η = 0.1	x: 0 m η = 1.3	x: 0 m η = 8.9	x: 0 m η < 0.1	x: 0 m η = 0.8	x: 0 m η = 13.0	x: 0.473 m η = 6.8	x: 0 m η = 11.2	CUMPLE η = 13.0
N746/N745	$w/t \leq (w/t)_{Max}$ Cumple	x: 0.63 m η = 1.5	x: 0.63 m η = 1.3	x: 0.158 m η = 0.5	x: 0.63 m η = 1.1	x: 0 m η = 6.1	η = 0.3	x: 0.63 m η = 0.2	x: 0.63 m η = 1.3	x: 0 m η = 6.3	x: 0.63 m η < 0.1	x: 0 m η = 0.4	x: 0 m η = 8.0	x: 0 m η = 7.2	x: 0 m η = 7.7	CUMPLE η = 8.0
N745/N744	$w/t \leq (w/t)_{Max}$ Cumple	η = 3.4	η = 3.8	x: 0 m η = 0.5	x: 0.63 m η = 3.7	x: 0.63 m η = 6.8	η = 0.7	x: 0.63 m η = 0.4	x: 0.63 m η = 3.8	x: 0.63 m η = 6.9	x: 0.63 m η = 0.1	x: 0.63 m η = 0.5	x: 0.63 m η = 8.7	x: 0.63 m η = 9.3	x: 0.63 m η = 9.2	CUMPLE η = 9.3
N744/N141	$w/t \leq (w/t)_{Max}$ Cumple	η = 5.5	η = 6.9	η = 1.3	x: 0.63 m η = 30.2	x: 0.63 m η = 15.6	x: 0.158 m η = 0.9	x: 0.63 m η = 3.4	x: 0.63 m η = 30.7	x: 0.63 m η = 16.0	x: 0.63 m η = 9.6	x: 0.63 m η = 2.6	x: 0.63 m η = 57.4	x: 0.63 m η = 47.1	x: 0.63 m η = 45.9	CUMPLE η = 57.4

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Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (ANSI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N751/N739	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 2.5	x: 0 m η = 3.7	η = 2.1	x: 0 m η = 5.0	x: 0 m η = 3.3	x: 0.401 m η = 0.3	x: 0 m η = 0.5	x: 0 m η = 5.3	x: 0 m η = 3.5	x: 0 m η = 0.3	x: 0 m η = 0.1	N.P.[1]	x: 0 m η = 11.5	x: 0 m η = 10.6	CUMPLE η = 11.5
N750/N739	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 3.6	x: 0.697 m η = 4.2	x: 0.232 m η = 1.3	x: 0 m η = 0.4	x: 0 m η = 0.7	x: 0.697 m η = 0.1	x: 0 m η = 0.1	x: 0.929 m η = 0.8	x: 0.929 m η = 1.2	x: 0.929 m η < 0.1	x: 0.929 m η < 0.1	N.P.[1]	x: 0 m η = 5.7	x: 0 m η = 5.1	CUMPLE η = 5.7
N750/N740	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 2.5	x: 0.201 m η = 3.6	η = 1.5	x: 0.802 m η = 0.7	x: 0 m η = 0.8	η = 0.1	x: 0.802 m η = 0.1	x: 0.802 m η = 1.2	x: 0.802 m η = 1.4	x: 0.802 m η < 0.1	x: 0.802 m η < 0.1	N.P.[1]	x: 0.802 m η = 4.6	x: 0.802 m η = 4.5	CUMPLE η = 4.6
N749/N740	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 3.2	x: 0 m η = 4.0	x: 0.465 m η = 1.3	x: 0 m η = 0.5	x: 0 m η = 0.7	η < 0.1	x: 0 m η = 0.1	x: 0.465 m η = 0.8	x: 0.929 m η = 1.2	x: 0.465 m η < 0.1	x: 0.929 m η < 0.1	N.P.[1]	x: 0 m η = 5.2	x: 0 m η = 4.8	CUMPLE η = 5.2
N749/N741	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 2.6	x: 0 m η = 3.5	x: 0.401 m η = 1.7	x: 0.802 m η = 0.9	x: 0 m η = 0.8	x: 0.401 m η = 0.1	x: 0 m η = 0.1	x: 0 m η = 1.3	x: 0 m η = 1.5	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 4.9	x: 0.802 m η = 4.6	CUMPLE η = 4.9
N748/N741	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 3.2	x: 0 m η = 4.1	η = 2.3	x: 0.929 m η = 0.4	x: 0 m η = 1.3	x: 0.929 m η < 0.1	x: 0 m η = 0.1	x: 0.465 m η = 1.4	x: 0 m η = 2.2	x: 0.465 m η < 0.1	x: 0 m η = 0.1	N.P.[1]	x: 0.929 m η = 5.1	x: 0 m η = 4.8	CUMPLE η = 5.1
N748/N742	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 2.7	x: 0 m η = 3.4	η = 1.8	x: 0.802 m η = 0.8	x: 0 m η = 0.7	x: 0.401 m η = 0.1	x: 0 m η = 0.1	x: 0.802 m η = 1.2	x: 0.802 m η = 1.2	x: 0.802 m η < 0.1	x: 0.802 m η < 0.1	N.P.[1]	x: 0 m η = 4.7	x: 0.802 m η = 4.4	CUMPLE η = 4.7
N747/N742	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 3.1	x: 0 m η = 4.2	η = 2.7	x: 0.929 m η = 0.4	x: 0.929 m η = 1.4	η < 0.1	x: 0.929 m η = 0.1	x: 0.465 m η = 1.6	x: 0.929 m η = 2.6	x: 0.465 m η < 0.1	x: 0.929 m η = 0.1	N.P.[1]	x: 0 m η = 5.1	x: 0 m η = 4.8	CUMPLE η = 5.1
N747/N743	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 2.7	x: 0 m η = 3.3	η = 1.7	x: 0.802 m η = 0.8	x: 0 m η = 0.7	η = 0.1	x: 0 m η = 0.1	x: 0.802 m η = 1.1	x: 0 m η = 1.2	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 4.8	x: 0 m η = 4.3	CUMPLE η = 4.8
N746/N743	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 3.0	x: 0 m η = 4.4	η = 2.3	x: 0.929 m η = 0.4	x: 0.929 m η = 1.3	x: 0.232 m η < 0.1	x: 0.929 m η = 0.1	x: 0.465 m η = 1.4	x: 0.929 m η = 2.3	x: 0.465 m η < 0.1	x: 0.929 m η = 0.1	N.P.[1]	x: 0 m η = 5.0	x: 0.929 m η = 4.9	CUMPLE η = 5.0
N751/N235	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 1.6	x: 0 m η = 1.1	x: 0.929 m η = 3.9	x: 0.929 m η = 3.2	x: 0.929 m η = 4.7	x: 0.465 m η = 0.3	x: 0.929 m η = 0.2	x: 0.929 m η = 3.8	x: 0.929 m η = 6.3	x: 0.929 m η = 0.1	x: 0.929 m η = 0.4	N.P.[1]	x: 0.929 m η = 6.7	x: 0.929 m η = 8.2	CUMPLE η = 8.2
N746/N752	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 2.8	x: 0 m η = 3.2	η = 1.3	x: 0.802 m η = 0.9	x: 0 m η = 0.9	η = 0.1	x: 0 m η = 0.1	x: 0.802 m η = 1.2	x: 0 m η = 1.2	x: 0.802 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 4.9	x: 0.802 m η = 4.4	CUMPLE η = 4.9
N745/N752	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 2.9	x: 0.232 m η = 4.4	x: 0 m η = 1.7	x: 0.929 m η = 0.5	x: 0 m η = 1.2	η < 0.1	x: 0.929 m η = 0.1	x: 0.465 m η = 1.1	x: 0 m η = 2.0	x: 0.465 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0.929 m η = 5.0	x: 0.929 m η = 5.0	CUMPLE η = 5.0
N745/N753	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 3.0	x: 0 m η = 3.3	x: 0 m η = 0.5	x: 0 m η = 0.5	x: 0 m η = 0.7	η = 0.1	x: 0 m η = 0.1	x: 0 m η = 0.6	x: 0 m η = 0.7	x: 0 m η < 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 4.2	x: 0 m η = 3.7	CUMPLE η = 4.2
N744/N753	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 3.1	x: 0 m η = 5.0	x: 0.697 m η = 1.8	x: 0 m η = 3.0	x: 0 m η = 1.5	η < 0.1	x: 0.929 m η = 0.3	x: 0 m η = 3.1	x: 0 m η = 2.2	x: 0 m η = 0.1	x: 0 m η < 0.1	N.P.[1]	x: 0 m η = 8.1	x: 0 m η = 8.5	CUMPLE η = 8.5
N744/N754	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.802 m η = 2.2	x: 0 m η = 2.0	η = 1.7	x: 0 m η = 3.8	x: 0 m η = 4.4	x: 0.401 m η = 0.5	x: 0 m η = 0.5	x: 0 m η = 3.8	x: 0 m η = 4.4	x: 0 m η = 0.1	x: 0 m η = 0.2	N.P.[1]	x: 0 m η = 9.7	x: 0 m η = 9.4	CUMPLE η = 9.7
N141/N754	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.929 m η = 1.4	x: 0 m η = 2.7	x: 0.697 m η = 4.7	x: 0 m η = 19.3	x: 0 m η = 10.5	η = 0.7	x: 0.929 m η = 1.5	x: 0 m η = 20.3	x: 0 m η = 11.0	x: 0 m η = 4.1	x: 0 m η = 1.2	x: 0 m η = 39.7	x: 0 m η = 33.1	x: 0 m η = 29.6	CUMPLE η = 39.7
N138/N77	x: 0.346 m $w/t \leq (w/t)_{Máx.}$ Cumple	x: 2.765 m η = 8.3	x: 2.765 m η = 24.1	N.P.[5]	x: 2.765 m η = 18.6	x: 2.765 m η = 8.1	x: 0 m η = 1.6	x: 0 m η = 2.2	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.3	x: 2.419 m η = 0.5	x: 2.765 m η = 34.7	x: 2.765 m η = 54.4	x: 2.419 m η = 48.4	CUMPLE η = 54.4
N137/N76	x: 0.346 m $w/t \leq (w/t)_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.7	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.5	CUMPLE η = 38.3
N136/N75	x: 0.346 m $w/t \leq (w/t)_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.7	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.5	CUMPLE η = 38.3
N135/N74	x: 0.346 m $w/t \leq (w/t)_{Máx.}$ Cumple	x: 2.765 m η = 5.1	x: 2.765 m η = 9.6	N.P.[5]	x: 2.765 m η = 19.8	x: 2.765 m η = 5.0	x: 0 m η = 1.0	x: 0 m η = 2.3	N.P.[5]	N.P.[7]	x: 2.419 m η = 3.8	x: 2.419 m η = 0.2	x: 2.765 m η = 29.7	x: 2.765 m η = 34.2	x: 2.419 m η = 32.0	CUMPLE η = 34.2
N134/N73	x: 0.346 m $w/t \leq (w/t)_{Máx.}$ Cumple	x: 2.765 m η = 5.1	x: 2.765 m η = 9.6	N.P.[5]	x: 2.765 m η = 19.8	x: 2.765 m η = 5.0	x: 0 m η = 1.0	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.8	x: 2.419 m η = 0.2	x: 2.765 m η = 29.7	x: 2.765 m η = 34.2	x: 2.419 m η = 31.9	CUMPLE η = 34.2
N178/N79	x: 0.346 m $w/t \leq (w/t)_{Máx.}$ Cumple	x: 2.765 m η = 3.4	x: 2.765 m η = 6.5	N.P.[5]	x: 2.765 m η = 20.2	x: 2.765 m η = 3.3	x: 0 m η = 0.6	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.9	x: 2.419 m η = 0.1	x: 2.765 m η = 26.8	x: 2.765 m η = 29.9	x: 2.419 m η = 28.2	CUMPLE η = 29.9
N181/N81	x: 0.346 m $w/t \leq (w/t)_{Máx.}$ Cumple	x: 2.765 m η = 1.7	x: 2.765 m η = 3.3	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.7	x: 2.765 m η = 25.4	x: 2.419 m η = 24.3	CUMPLE η = 25.4
N182/N82	x: 0.346 m $w/t \leq (w/t)_{Máx.}$ Cumple	x: 2.765 m η = 1.7	x: 2.765 m η = 3.2	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.7	x: 2.765 m η = 25.3	x: 2.419 m η = 24.3	CUMPLE η = 25.3
N191/N85	x: 0.346 m $w/t \leq (w/t)_{Máx.}$ Cumple	x: 2.765 m η = 1.7	x: 2.765 m η = 3.2	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.7	x: 2.765 m η = 25.3	x: 2.419 m η = 24.3	CUMPLE η = 25.3
N192/N86	x: 0.346 m $w/t \leq (w/t)_{Máx.}$ Cumple	x: 2.765 m η = 1.6	x: 2.765 m η = 3.4	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.7	x: 2.765 m η = 25.4	x: 2.419 m η = 24.4	CUMPLE η = 25.4
N193/N87	x: 0.346 m $w/t \leq (w/t)_{Máx.}$ Cumple	x: 2.765 m η = 3.4	x: 2.765 m η = 6.4	N.P.[5]	x: 2.765 m η = 20.2	x: 2.765 m η = 3.3	x: 0 m η = 0.6	x: 0 m η = 2.4	N.P.[5]	N.P.[7]	x: 2.419 m η = 3.9	x: 2.419 m η = 0.1	x: 2.765 m η = 26.8	x: 2.765 m η = 29.8	x: 2.419 m η = 28.1	CUMPLE η = 29.8
N194/N88	x: 0.346 m $w/t \leq (w/t)_{Máx.}$ Cumple	x: 2.765 m η = 3.4	x: 2.765 m η = 6.5	N.P.[5]	x: 2.765 m η = 20.2	x: 2.765 m η = 3.3	x: 0 m η = 0.6	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.9	x: 2.419 m η = 0.1	x: 2.765 m η = 26.8	x: 2.765 m η = 29.9	x: 2.419 m η = 28.3	CUMPLE η = 29.9
N195/N89	x: 0.346 m $w/t \leq (w/t)_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.7	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.5	CUMPLE η = 38.3
N196/N90	x: 0.346 m $w/t \leq (w/t)_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.6	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.4	x: 2.765 m η = 38.2	x: 2.419 m η = 35.4	CUMPLE η = 38.2
N197/N91	x: 0.346 m $w/t \leq (w/t)_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.7	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[5]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.5	CUMPLE η = 38.3

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N198/N92	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 8.3	x: 2.765 m η = 24.1	N.P.[5]	x: 2.765 m η = 18.6	x: 2.765 m η = 8.1	x: 0 m η = 1.6	x: 0 m η = 2.2	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.3	x: 2.419 m η = 0.6	x: 2.765 m η = 34.7	x: 2.765 m η = 54.4	x: 2.419 m η = 48.4	CUMPLE η = 54.4
N268/N175	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 8.3	x: 2.765 m η = 24.0	N.P.[5]	x: 2.765 m η = 18.6	x: 2.765 m η = 8.1	x: 0 m η = 1.6	x: 0 m η = 2.2	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.3	x: 2.419 m η = 0.6	x: 2.765 m η = 34.8	x: 2.765 m η = 54.3	x: 2.419 m η = 48.2	CUMPLE η = 54.3
N267/N174	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.7	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.5	CUMPLE η = 38.3
N266/N173	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.7	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.5	CUMPLE η = 38.3
N265/N172	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 4.9	x: 2.765 m η = 9.9	N.P.[5]	x: 2.765 m η = 19.8	x: 2.765 m η = 5.0	x: 0 m η = 1.0	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.8	x: 2.419 m η = 0.2	x: 2.765 m η = 29.5	x: 2.765 m η = 34.5	x: 2.419 m η = 32.3	CUMPLE η = 34.5
N264/N171	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 5.1	x: 2.765 m η = 9.6	N.P.[5]	x: 2.765 m η = 19.8	x: 2.765 m η = 5.0	x: 0 m η = 1.0	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.8	x: 2.419 m η = 0.2	x: 2.765 m η = 29.7	x: 2.765 m η = 34.2	x: 2.419 m η = 32.0	CUMPLE η = 34.2
N308/N177	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 3.4	x: 2.765 m η = 6.5	N.P.[5]	x: 2.765 m η = 20.2	x: 2.765 m η = 3.3	x: 0 m η = 0.6	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.9	x: 2.419 m η = 0.1	x: 2.765 m η = 28.8	x: 2.765 m η = 29.9	x: 2.419 m η = 28.2	CUMPLE η = 29.9
N311/N179	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 1.6	x: 2.765 m η = 3.3	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.7	x: 2.765 m η = 25.4	x: 2.419 m η = 24.4	CUMPLE η = 25.4
N312/N180	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 1.6	x: 2.765 m η = 4.0	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.4	x: 2.765 m η = 26.0	x: 2.419 m η = 25.1	CUMPLE η = 26.0
N321/N183	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 1.4	x: 2.765 m η = 3.7	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.5	x: 2.765 m η = 25.8	x: 2.419 m η = 24.8	CUMPLE η = 25.8
N322/N184	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 1.6	x: 2.765 m η = 3.4	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.7	x: 2.765 m η = 25.4	x: 2.419 m η = 24.4	CUMPLE η = 25.4
N323/N185	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 3.4	x: 2.765 m η = 6.4	N.P.[5]	x: 2.765 m η = 20.2	x: 2.765 m η = 3.3	x: 0 m η = 0.6	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.9	x: 2.419 m η = 0.1	x: 2.765 m η = 26.8	x: 2.765 m η = 29.8	x: 2.419 m η = 28.2	CUMPLE η = 29.8
N324/N186	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 3.4	x: 2.765 m η = 6.5	N.P.[5]	x: 2.765 m η = 20.2	x: 2.765 m η = 3.3	x: 0 m η = 0.6	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.9	x: 2.419 m η = 0.1	x: 2.765 m η = 26.8	x: 2.765 m η = 29.9	x: 2.419 m η = 28.3	CUMPLE η = 29.9
N325/N187	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 6.6	x: 2.765 m η = 12.9	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.2	x: 2.765 m η = 38.6	x: 2.419 m η = 35.8	CUMPLE η = 38.6
N326/N188	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.7	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.4	CUMPLE η = 38.3
N327/N189	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.7	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.5	CUMPLE η = 38.3
N328/N190	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 8.4	x: 2.765 m η = 24.0	N.P.[5]	x: 2.765 m η = 18.6	x: 2.765 m η = 8.1	x: 0 m η = 1.6	x: 0 m η = 2.2	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.3	x: 2.419 m η = 0.6	x: 2.765 m η = 34.8	x: 2.765 m η = 54.2	x: 2.419 m η = 48.2	CUMPLE η = 54.2
N366/N305	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 8.4	x: 2.765 m η = 24.0	N.P.[5]	x: 2.765 m η = 18.6	x: 2.765 m η = 8.1	x: 0 m η = 1.6	x: 0 m η = 2.2	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.3	x: 2.419 m η = 0.6	x: 2.765 m η = 34.8	x: 2.765 m η = 54.2	x: 2.419 m η = 48.2	CUMPLE η = 54.2
N365/N304	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.7	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.5	CUMPLE η = 38.3
N364/N303	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.7	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.5	CUMPLE η = 38.3
N363/N302	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 5.1	x: 2.765 m η = 9.5	N.P.[5]	x: 2.765 m η = 19.8	x: 2.765 m η = 5.0	x: 0 m η = 1.0	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.8	x: 2.419 m η = 0.2	x: 2.765 m η = 29.7	x: 2.765 m η = 34.1	x: 2.419 m η = 31.8	CUMPLE η = 34.1
N362/N301	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 5.1	x: 2.765 m η = 9.6	N.P.[5]	x: 2.765 m η = 19.8	x: 2.765 m η = 5.0	x: 0 m η = 1.0	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.8	x: 2.419 m η = 0.2	x: 2.765 m η = 29.7	x: 2.765 m η = 34.2	x: 2.419 m η = 32.0	CUMPLE η = 34.2
N406/N307	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 3.4	x: 2.765 m η = 6.5	N.P.[5]	x: 2.765 m η = 20.2	x: 2.765 m η = 3.3	x: 0 m η = 0.6	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.9	x: 2.419 m η = 0.1	x: 2.765 m η = 26.8	x: 2.765 m η = 29.9	x: 2.419 m η = 28.2	CUMPLE η = 29.9
N409/N309	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 1.6	x: 2.765 m η = 3.3	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.7	x: 2.765 m η = 25.4	x: 2.419 m η = 24.4	CUMPLE η = 25.4
N410/N310	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 1.7	x: 2.765 m η = 3.2	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.7	x: 2.765 m η = 25.3	x: 2.419 m η = 24.2	CUMPLE η = 25.3
N419/N313	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 1.7	x: 2.765 m η = 3.2	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.8	x: 2.765 m η = 25.2	x: 2.419 m η = 24.2	CUMPLE η = 25.2
N420/N314	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 1.6	x: 2.765 m η = 3.4	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.7	x: 2.765 m η = 25.4	x: 2.419 m η = 24.4	CUMPLE η = 25.4

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2018))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N421/N315	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 3.4	x: 2.765 m η = 6.4	N.P.[5]	x: 2.765 m η = 20.2	x: 2.765 m η = 3.3	x: 0 m η = 0.6	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.9	x: 2.419 m η = 0.1	x: 2.765 m η = 26.8	x: 2.765 m η = 29.8	x: 2.419 m η = 28.2	CUMPLE η = 29.8
N422/N316	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 3.4	x: 2.765 m η = 6.5	N.P.[5]	x: 2.765 m η = 20.2	x: 2.765 m η = 3.3	x: 0 m η = 0.6	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.9	x: 2.419 m η = 0.1	x: 2.765 m η = 26.8	x: 2.765 m η = 29.9	x: 2.419 m η = 28.3	CUMPLE η = 29.9
N423/N317	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 6.8	x: 2.765 m η = 12.5	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.4	x: 2.765 m η = 38.2	x: 2.419 m η = 35.3	CUMPLE η = 38.2
N424/N318	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.6	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.4	CUMPLE η = 38.3
N425/N319	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.7	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.5	CUMPLE η = 38.3
N426/N320	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 8.4	x: 2.765 m η = 23.9	N.P.[5]	x: 2.765 m η = 18.6	x: 2.765 m η = 8.1	x: 0 m η = 1.6	x: 0 m η = 2.2	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.3	x: 2.419 m η = 0.6	x: 2.765 m η = 34.8	x: 2.765 m η = 54.2	x: 2.419 m η = 46.1	CUMPLE η = 54.2
N496/N403	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 8.3	x: 2.765 m η = 24.0	N.P.[5]	x: 2.765 m η = 18.6	x: 2.765 m η = 8.1	x: 0 m η = 1.6	x: 0 m η = 2.2	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.3	x: 2.419 m η = 0.6	x: 2.765 m η = 34.8	x: 2.765 m η = 54.3	x: 2.419 m η = 48.2	CUMPLE η = 54.3
N495/N402	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.7	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.5	CUMPLE η = 38.3
N494/N401	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.7	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.5	CUMPLE η = 38.3
N493/N400	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 4.9	x: 2.765 m η = 9.9	N.P.[5]	x: 2.765 m η = 19.8	x: 2.765 m η = 5.0	x: 0 m η = 1.0	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.8	x: 2.419 m η = 0.2	x: 2.765 m η = 29.5	x: 2.765 m η = 34.5	x: 2.419 m η = 32.3	CUMPLE η = 34.5
N492/N399	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 5.1	x: 2.765 m η = 9.8	N.P.[5]	x: 2.765 m η = 19.8	x: 2.765 m η = 5.0	x: 0 m η = 1.0	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.8	x: 2.419 m η = 0.2	x: 2.765 m η = 29.7	x: 2.765 m η = 34.2	x: 2.419 m η = 32.0	CUMPLE η = 34.2
N536/N405	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 3.4	x: 2.765 m η = 6.5	N.P.[5]	x: 2.765 m η = 20.2	x: 2.765 m η = 3.3	x: 0 m η = 0.6	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.9	x: 2.419 m η = 0.1	x: 2.765 m η = 26.8	x: 2.765 m η = 29.9	x: 2.419 m η = 28.2	CUMPLE η = 29.9
N539/N407	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 1.6	x: 2.765 m η = 3.3	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.7	x: 2.765 m η = 25.4	x: 2.419 m η = 24.4	CUMPLE η = 25.4
N540/N408	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 1.4	x: 2.765 m η = 3.8	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.4	x: 2.765 m η = 25.8	x: 2.419 m η = 24.9	CUMPLE η = 25.8
N549/N411	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 1.4	x: 2.765 m η = 3.7	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.5	x: 2.765 m η = 25.8	x: 2.419 m η = 24.8	CUMPLE η = 25.8
N550/N412	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 1.6	x: 2.765 m η = 3.4	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.7	x: 2.765 m η = 25.4	x: 2.419 m η = 24.4	CUMPLE η = 25.4
N551/N413	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 3.4	x: 2.765 m η = 6.4	N.P.[5]	x: 2.765 m η = 20.2	x: 2.765 m η = 3.3	x: 0 m η = 0.6	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.9	x: 2.419 m η = 0.1	x: 2.765 m η = 26.8	x: 2.765 m η = 29.8	x: 2.419 m η = 28.2	CUMPLE η = 29.8
N552/N414	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 3.4	x: 2.765 m η = 6.5	N.P.[5]	x: 2.765 m η = 20.2	x: 2.765 m η = 3.3	x: 0 m η = 0.6	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.9	x: 2.419 m η = 0.1	x: 2.765 m η = 26.8	x: 2.765 m η = 29.9	x: 2.419 m η = 28.3	CUMPLE η = 29.9
N553/N415	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 6.6	x: 2.765 m η = 12.9	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.2	x: 2.765 m η = 38.5	x: 2.419 m η = 35.8	CUMPLE η = 38.5
N554/N416	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.7	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.4	CUMPLE η = 38.3
N555/N417	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.7	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.5	CUMPLE η = 38.3
N556/N418	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 8.4	x: 2.765 m η = 24.0	N.P.[5]	x: 2.765 m η = 18.6	x: 2.765 m η = 8.1	x: 0 m η = 1.6	x: 0 m η = 2.2	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.3	x: 2.419 m η = 0.6	x: 2.765 m η = 34.8	x: 2.765 m η = 54.2	x: 2.419 m η = 48.2	CUMPLE η = 54.2
N596/N533	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 8.3	x: 2.765 m η = 24.1	N.P.[5]	x: 2.765 m η = 18.6	x: 2.765 m η = 8.1	x: 0 m η = 1.6	x: 0 m η = 2.2	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.3	x: 2.419 m η = 0.6	x: 2.765 m η = 34.7	x: 2.765 m η = 54.4	x: 2.419 m η = 48.4	CUMPLE η = 54.4
N595/N532	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.7	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.5	CUMPLE η = 38.3
N594/N531	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.7	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.5	CUMPLE η = 38.3
N593/N530	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 5.1	x: 2.765 m η = 9.6	N.P.[5]	x: 2.765 m η = 19.8	x: 2.765 m η = 5.0	x: 0 m η = 1.0	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.8	x: 2.419 m η = 0.2	x: 2.765 m η = 29.7	x: 2.765 m η = 34.2	x: 2.419 m η = 32.0	CUMPLE η = 34.2
N592/N529	x: 0.346 m $w / t \leq (w / t)_{Máx.}$ Cumple	x: 2.765 m η = 5.1	x: 2.765 m η = 9.6	N.P.[5]	x: 2.765 m η = 19.8	x: 2.765 m η = 5.0	x: 0 m η = 1.0	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.8	x: 2.419 m η = 0.2	x: 2.765 m η = 29.7	x: 2.765 m η = 34.2	x: 2.419 m η = 31.9	CUMPLE η = 34.2

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barra	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N638/N535	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 3.4	x: 2.765 m η = 6.5	N.P.[5]	x: 2.765 m η = 20.2	x: 2.765 m η = 3.3	x: 0 m η = 0.6	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.9	x: 2.419 m η = 0.1	x: 2.765 m η = 26.8	x: 2.765 m η = 29.9	x: 2.419 m η = 28.2	CUMPLE η = 29.9
N641/N537	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 1.7	x: 2.765 m η = 3.3	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.7	x: 2.765 m η = 25.4	x: 2.419 m η = 24.3	CUMPLE η = 25.4
N642/N538	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 1.7	x: 2.765 m η = 3.2	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.7	x: 2.765 m η = 25.3	x: 2.419 m η = 24.2	CUMPLE η = 25.3
N651/N541	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 1.7	x: 2.765 m η = 3.2	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.7	x: 2.765 m η = 25.3	x: 2.419 m η = 24.3	CUMPLE η = 25.3
N652/N542	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 1.6	x: 2.765 m η = 3.4	N.P.[5]	x: 2.765 m η = 20.4	x: 2.765 m η = 1.7	x: 0 m η = 0.3	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 4.0	x: 2.419 m η < 0.1	x: 2.765 m η = 23.7	x: 2.765 m η = 25.4	x: 2.419 m η = 24.4	CUMPLE η = 25.4
N653/N543	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 3.4	x: 2.765 m η = 6.4	N.P.[5]	x: 2.765 m η = 20.2	x: 2.765 m η = 3.3	x: 0 m η = 0.6	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.9	x: 2.419 m η = 0.1	x: 2.765 m η = 26.8	x: 2.765 m η = 29.8	x: 2.419 m η = 28.1	CUMPLE η = 29.8
N654/N544	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 3.4	x: 2.765 m η = 6.5	N.P.[5]	x: 2.765 m η = 20.2	x: 2.765 m η = 3.3	x: 0 m η = 0.6	x: 0 m η = 2.4	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.9	x: 2.419 m η = 0.1	x: 2.765 m η = 26.8	x: 2.765 m η = 29.9	x: 2.419 m η = 28.3	CUMPLE η = 29.9
N655/N545	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.7	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.5	CUMPLE η = 38.3
N656/N546	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.6	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.4	x: 2.765 m η = 38.2	x: 2.419 m η = 35.4	CUMPLE η = 38.2
N657/N547	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 6.7	x: 2.765 m η = 12.7	N.P.[5]	x: 2.765 m η = 19.3	x: 2.765 m η = 6.6	x: 0 m η = 1.3	x: 0 m η = 2.3	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.6	x: 2.419 m η = 0.4	x: 2.765 m η = 32.3	x: 2.765 m η = 38.3	x: 2.419 m η = 35.5	CUMPLE η = 38.3
N658/N548	x: 0.346 m w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 2.765 m η = 8.3	x: 2.765 m η = 24.1	N.P.[5]	x: 2.765 m η = 18.6	x: 2.765 m η = 8.1	x: 0 m η = 1.6	x: 0 m η = 2.2	N.P.[6]	N.P.[7]	x: 2.419 m η = 3.3	x: 2.419 m η = 0.6	x: 2.765 m η = 34.7	x: 2.765 m η = 54.4	x: 2.419 m η = 48.3	CUMPLE η = 54.4
N755/N756	w / t ≤ (w / t)$_{Máx.}$ Cumple	η < 0.1	η < 0.1	η = 3.5	x: 0.3 m η = 19.0	x: 0.3 m η = 2.9	η = 1.2	x: 0.3 m η = 48.9	x: 0.3 m η = 20.5	x: 0.3 m η = 4.4	x: 0.3 m η = 69.1	x: 0.3 m η = 0.2	x: 0.3 m η = 55.9	x: 0.3 m η = 24.7	x: 0.3 m η = 21.3	CUMPLE η = 21.3
N147/N154	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.217 m η = 9.2	x: 0.217 m η = 22.9	η = 1.6	x: 0.869 m η = 3.7	x: 0 m η = 7.9	η = 0.6	x: 0 m η = 0.4	x: 0 m η = 4.3	x: 0 m η = 8.6	x: 0 m η = 0.2	x: 0 m η = 0.7	x: 0 m η = 15.2	x: 0 m η = 27.1	x: 0.869 m η = 27.4	CUMPLE η = 27.4
N154/N148	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.983 m η = 14.5	x: 0 m η = 10.7	η = 0.4	x: 0 m η = 2.6	x: 0 m η = 28.3	η = 2.9	x: 0.983 m η = 0.3	x: 0 m η = 2.6	x: 0 m η = 28.5	x: 0 m η = 0.1	x: 0 m η = 8.2	x: 0 m η = 45.4	x: 0 m η = 33.1	x: 0 m η = 44.5	CUMPLE η = 45.4
N154/N117	w / t ≤ (w / t)$_{Máx.}$ Cumple	η < 0.1	η < 0.1	η = 0.1	x: 0.3 m η = 55.3	x: 0.3 m η = 4.1	x: 0.15 m η = 1.8	x: 0.15 m η = 66.1	x: 0.3 m η = 55.3	x: 0.3 m η = 4.1	x: 0 m η = 84.7	x: 0.3 m η = 0.2	x: 0.3 m η = 99.2	x: 0.3 m η = 59.4	x: 0.3 m η = 76.6	CUMPLE η = 76.6
N148/N111	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.15 m η < 0.1	x: 0.15 m η < 0.1	x: 0.15 m η = 1.1	x: 0 m η = 48.8	x: 0 m η = 30.9	x: 0.15 m η = 13.2	x: 0.15 m η = 63.3	x: 0 m η = 49.2	x: 0 m η = 31.4	x: 0 m η = 62.6	x: 0 m η = 11.6	x: 0 m η = 25.4	x: 0 m η = 80.6	x: 0 m η = 60.7	CUMPLE η = 60.7
N140/N103	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.15 m η < 0.1	x: 0.15 m η < 0.1	x: 0.15 m η = 1.1	x: 0 m η = 53.5	x: 0 m η = 31.5	x: 0.15 m η = 13.4	x: 0.15 m η = 65.3	x: 0 m η = 54.0	x: 0 m η = 32.0	x: 0 m η = 79.6	x: 0 m η = 12.0	x: 0 m η = 32.3	x: 0 m η = 85.8	x: 0 m η = 83.4	CUMPLE η = 83.4
N146/N107	w / t ≤ (w / t)$_{Máx.}$ Cumple	η < 0.1	η < 0.1	x: 0.15 m η = 1.5	x: 0 m η = 40.4	x: 0 m η = 16.3	x: 0.15 m η = 5.5	x: 0 m η = 47.0	x: 0 m η = 41.1	x: 0 m η = 16.9	x: 0 m η = 21.1	x: 0 m η = 3.2	x: 0 m η = 97.5	x: 0 m η = 57.8	x: 0 m η = 30.7	CUMPLE η = 30.7
N558/N559	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.7 m η = 12.1	x: 0.7 m η = 15.6	x: 0.7 m η = 0.5	x: 1.4 m η = 1.6	x: 0 m η = 37.6	x: 1.4 m η = 4.6	x: 1.4 m η = 0.2	x: 1.4 m η = 1.0	x: 0 m η = 37.8	x: 1.4 m η < 0.1	x: 0 m η = 14.5	x: 0 m η = 60.3	x: 0 m η = 55.0	x: 0 m η = 62.1	CUMPLE η = 62.1
N559/N560	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.35 m η = 4.0	x: 0 m η = 1.8	x: 0.225 m η = 1.0	x: 1.35 m η = 13.2	x: 1.35 m η = 53.2	η = 6.2	x: 0 m η = 1.2	x: 1.35 m η = 13.3	x: 1.35 m η = 53.6	x: 1.35 m η = 1.8	x: 1.35 m η = 29.1	x: 1.35 m η = 77.0	x: 1.35 m η = 61.3	x: 1.35 m η = 69.6	CUMPLE η = 77.0
N560/N561	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.79 m η = 8.7	x: 0.592 m η = 3.3	x: 0 m η = 6.4	x: 0 m η = 1.6	x: 0 m η = 45.5	η = 9.0	x: 0.79 m η = 0.3	x: 0 m η = 3.6	x: 0 m η = 48.3	x: 0 m η = 0.1	x: 0 m η = 24.1	x: 0 m η = 71.2	x: 0 m η = 52.4	x: 0 m η = 63.2	CUMPLE η = 71.2
N597/N598	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.467 m η = 13.9	x: 0.467 m η = 16.9	η = 0.5	x: 1.4 m η = 1.3	x: 0 m η = 37.7	x: 0.7 m η = 4.7	x: 1.4 m η = 0.2	x: 1.4 m η = 1.3	x: 0 m η = 37.9	x: 1.4 m η < 0.1	x: 0 m η = 14.6	x: 0 m η = 61.3	x: 0 m η = 56.6	x: 0 m η = 63.7	CUMPLE η = 63.7
N598/N599	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.35 m η = 5.6	x: 0.225 m η = 0.9	η = 0.9	x: 1.35 m η = 11.9	x: 1.35 m η = 49.9	x: 0.675 m η = 5.9	x: 0 m η = 1.1	x: 1.35 m η = 12.1	x: 1.35 m η = 50.3	x: 1.35 m η = 1.5	x: 1.35 m η = 25.6	x: 1.35 m η = 75.4	x: 1.35 m η = 4.0	x: 1.35 m η = 66.2	CUMPLE η = 75.4
N599/N600	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.79 m η = 9.5	x: 0 m η = 3.0	x: 0.395 m η = 6.6	x: 0 m η = 1.8	x: 0 m η = 49.9	x: 0.592 m η = 9.7	x: 0.79 m η = 0.3	x: 0 m η = 3.5	x: 0 m η = 52.9	x: 0 m η = 0.1	x: 0 m η = 28.9	x: 0 m η = 78.0	x: 0 m η = 58.1	x: 0 m η = 70.0	CUMPLE η = 78.0
N601/N597	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.234 m η = 25.1	x: 1.234 m η = 38.8	η = 2.0	x: 0 m η = 1.9	x: 1.41 m η = 17.3	x: 1.234 m η = 1.6	x: 0 m η = 0.1	x: 0 m η = 2.8	x: 1.41 m η = 18.1	x: 0 m η = 0.1	x: 1.41 m η = 3.3	x: 1.41 m η = 48.1	x: 1.41 m η = 59.0	x: 1.41 m η = 59.3	CUMPLE η = 59.3
N557/N558	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.41 m η = 21.5	x: 1.41 m η = 34.6	x: 1.41 m η = 2.0	x: 0 m η = 1.8	x: 1.41 m η = 17.3	x: 0.529 m η = 1.6	x: 0 m η = 0.1	x: 0 m η = 2.7	x: 1.41 m η = 18.2	x: 0 m η = 0.1	x: 1.41 m η = 3.3	x: 1.41 m η = 46.1	x: 1.41 m η = 55.7	x: 1.41 m η = 55.8	CUMPLE η = 55.8
N563/N562	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.121 m η = 0.5	x: 0 m η = 17.2	x: 0 m η = 2.6	x: 1.121 m η = 7.6	x: 1.121 m η = 26.8	x: 0.187 m η = 3.1	x: 1.121 m η = 0.8	x: 1.121 m η = 7.9	x: 1.121 m η = 27.9	x: 1.121 m η = 0.6	x: 1.121 m η = 7.9	N.P.[1]	x: 1.121 m η = 41.4	x: 1.121 m η = 42.3	CUMPLE η = 42.3
N564/N563	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 14.3	η = 1.6	x: 0 m η = 2.2	x: 0 m η = 30.2	η = 4.0	x: 0 m η = 0.2	x: 0 m η = 2.9	x: 0 m η = 31.0	x: 0 m η = 0.1	x: 0 m η = 9.8	N.P.[1]	x: 0 m η = 40.9	x: 0 m η = 46.2	CUMPLE η = 46.2
N565/N564	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.7 m η = 13.5	x: 0.7 m η = 20.8	η = 0.1	x: 0 m η = 8.7	x: 0 m η = 44.8	η = 5.4	x: 1.167 m η = 0.8	x: 0 m η = 8.7	x: 0 m η = 44.8	x: 0 m η = 0.8	x: 0 m η = 20.4	x: 0 m η = 75.8	x: 0 m η = 70.2	x: 0 m η = 76.3	CUMPLE η = 76.3
N605/N603	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.121 m η = 1.2	x: 0 m η = 14.5	x: 0 m η = 2.5	x: 1.121 m η = 6.4	x: 1.121 m η = 26.5	x: 0.187 m η = 3.1	x: 1.121 m η = 0.6	x: 1.121 m η = 6.8	x: 1.121 m η = 27.6	x: 1.121 m η = 0.5	x: 1.121 m η = 7.7	x: 1.121 m η = 35.0	x: 1.121 m η = 43.0	x: 1.121 m η = 43.3	CUMPLE η = 43.3
N604/N605	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.4 m η = 4.5	x: 0 m η = 13.9	x: 1.167 m η = 1.7	x: 0 m η = 1.9	x: 0 m η = 30.4	η = 4.1	x: 0 m η = 0.2	x: 0 m η = 2.4	x: 0 m η = 31.1	x: 0 m η = 0.1	x: 0 m η = 9.8	x: 0 m η = 45.5	x: 0 m η = 45.9	x: 0 m η = 51.8	CUMPLE η = 51.8
N636/N604	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.4 m η = 17.0	x: 1.4 m η = 24.3	η = 0.3	x: 0 m η = 9.2	x: 0 m η = 44.2	η = 5.4	x: 1.167 m η = 0.9	x: 0 m η = 9.3	x: 0 m η = 44.4	x: 0 m η = 0.9	x: 0 m η = 20.0	x: 0 m η = 76.1	x: 0 m η = 71.3	x: 0 m η = 78.9	CUMPLE η = 78.9
N12/N6	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.121 m η = 2.6	x: 0 m η = 14.5	η = 2.7	x: 1.121 m η = 6.4	x: 1.121 m η = 26.6	x: 0.187 m η = 3.1	x: 1.121 m η = 0.6	x: 1.121 m η = 6.7	x: 1.121 m η = 27.8	x: 1.121 m η = 0.5	x: 1.121 m η = 7.8	x: 1.121 m η = 35.1	x: 1.121 m η = 43.0	x: 1.121 m η = 43.2	CUMPLE η = 43.2

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N11/N12	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.4 m η = 3.8	x: 0 m η = 13.1	x: 1.167 m η = 1.8	x: 0 m η = 2.2	x: 0 m η = 30.7	x: 1.167 m η = 4.1	x: 0 m η = 0.2	x: 0 m η = 2.6	x: 0 m η = 31.5	x: 0 m η = 0.1	x: 0 m η = 10.1	x: 0 m η = 45.4	x: 0 m η = 45.7	x: 0 m η = 51.3	CUMPLE η = 51.3
N10/N11	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.4 m η = 15.8	x: 1.4 m η = 23.1	η = 0.2	x: 0 m η = 10.3	x: 0 m η = 43.3	x: 1.4 m η = 5.3	x: 1.4 m η = 1.0	x: 0 m η = 10.3	x: 0 m η = 43.4	x: 0 m η = 1.1	x: 0 m η = 19.1	x: 0 m η = 73.2	x: 0 m η = 69.1	x: 0 m η = 76.4	CUMPLE η = 76.4
N25/N23	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.121 m η = 3.3	x: 0 m η = 16.2	x: 0.56 m η = 2.6	x: 1.121 m η = 5.3	x: 1.121 m η = 25.4	x: 0.56 m η = 2.9	x: 0 m η = 0.7	x: 1.121 m η = 5.6	x: 1.121 m η = 26.6	x: 1.121 m η = 0.3	x: 1.121 m η = 7.2	x: 1.121 m η = 35.1	x: 1.121 m η = 40.8	x: 1.121 m η = 42.8	CUMPLE η = 42.8
N24/N25	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.167 m η = 3.9	x: 0 m η = 14.5	x: 0.467 m η = 1.8	x: 0 m η = 1.8	x: 0 m η = 29.5	x: 0.467 m η = 4.0	x: 0.467 m η = 0.1	x: 0 m η = 2.4	x: 0 m η = 30.3	x: 0 m η = 0.1	x: 0 m η = 9.4	x: 0 m η = 43.6	x: 0 m η = 45.9	x: 0 m η = 51.0	CUMPLE η = 51.0
N756/N24	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.4 m η = 15.0	x: 1.4 m η = 23.4	η = 0.2	x: 0 m η = 10.1	x: 0 m η = 42.0	x: 1.4 m η = 5.1	x: 1.4 m η = 0.9	x: 0 m η = 10.1	x: 0 m η = 42.1	x: 0 m η = 1.0	x: 0 m η = 18.0	x: 0 m η = 70.1	x: 0 m η = 68.1	x: 0 m η = 75.1	CUMPLE η = 75.1
N573/N572	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.56 m η = 3.0	x: 0 m η = 19.3	x: 0.187 m η = 2.9	x: 1.121 m η = 5.7	x: 1.121 m η = 27.5	η = 3.2	x: 0 m η = 0.7	x: 1.121 m η = 6.0	x: 1.121 m η = 28.8	x: 1.121 m η = 0.4	x: 1.121 m η = 8.4	x: 1.121 m η = 5.8	x: 1.121 m η = 45.1	x: 1.121 m η = 45.5	CUMPLE η = 45.5
N574/N573	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 16.1	x: 0.933 m η = 1.7	x: 0 m η = 1.8	x: 0 m η = 31.3	x: 0.933 m η = 4.1	x: 0.933 m η = 0.1	x: 0 m η = 2.6	x: 0 m η = 32.0	x: 0 m η = 0.1	x: 0 m η = 10.4	N.P.[1]	x: 0 m η = 42.6	x: 0 m η = 48.0	CUMPLE η = 48.0
N575/N574	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.7 m η = 13.7	x: 0.7 m η = 22.3	η = 0.2	x: 0 m η = 9.8	x: 0 m η = 44.2	x: 0.7 m η = 5.3	x: 1.167 m η = 0.9	x: 0 m η = 9.8	x: 0 m η = 44.3	x: 0 m η = 1.0	x: 0 m η = 19.9	x: 0 m η = 75.7	x: 0 m η = 71.9	x: 0 m η = 76.9	CUMPLE η = 76.9
N612/N611	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.121 m η = 3.0	x: 0 m η = 16.1	x: 0.747 m η = 2.8	x: 1.121 m η = 5.2	x: 1.121 m η = 27.5	x: 0 m η = 3.2	x: 0 m η = 0.7	x: 1.121 m η = 5.6	x: 1.121 m η = 28.7	x: 1.121 m η = 0.3	x: 1.121 m η = 8.4	x: 1.121 m η = 37.9	x: 1.121 m η = 42.6	x: 1.121 m η = 45.2	CUMPLE η = 45.2
N613/N612	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.167 m η = 4.5	x: 1.167 m η = 14.9	x: 1.167 m η = 1.7	x: 0 m η = 1.8	x: 0 m η = 31.3	x: 1.167 m η = 4.1	x: 0.467 m η = 0.1	x: 0 m η = 2.3	x: 0 m η = 32.0	x: 0 m η = 0.1	x: 0 m η = 10.4	x: 0 m η = 46.3	x: 0 m η = 48.1	x: 0 m η = 53.8	CUMPLE η = 53.8
N614/N613	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.4 m η = 16.6	x: 1.4 m η = 25.1	x: 1.4 m η = 0.2	x: 0 m η = 9.9	x: 0 m η = 44.2	η = 5.3	x: 1.167 m η = 0.9	x: 0 m η = 9.9	x: 0 m η = 44.3	x: 0 m η = 1.0	x: 0 m η = 19.9	x: 0 m η = 75.1	x: 0 m η = 72.8	x: 0 m η = 79.8	CUMPLE η = 79.8
N474/N473	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.187 m η = 1.8	x: 0 m η = 34.1	η = 1.9	x: 1.121 m η = 8.5	x: 1.121 m η = 24.7	x: 0.374 m η = 2.8	x: 1.121 m η = 0.8	x: 1.121 m η = 8.5	x: 1.121 m η = 25.5	x: 1.121 m η = 0.7	x: 1.121 m η = 6.6	N.P.[1]	x: 1.121 m η = 49.2	x: 1.121 m η = 48.4	CUMPLE η = 49.2
N475/N474	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.4 m η = 1.6	x: 0 m η = 29.6	x: 0.467 m η = 1.5	x: 0 m η = 3.1	x: 0 m η = 30.4	x: 0.467 m η = 4.1	x: 0 m η = 0.2	x: 0 m η = 2.9	x: 0 m η = 31.1	x: 0 m η = 0.1	x: 0 m η = 9.8	x: 0 m η = 43.1	x: 0 m η = 52.7	x: 0 m η = 57.1	CUMPLE η = 57.1
N476/N475	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.4 m η = 13.8	x: 0 m η = 26.9	η = 0.4	x: 0 m η = 10.9	x: 0 m η = 44.2	η = 5.4	x: 1.4 m η = 1.1	x: 0 m η = 11.0	x: 0 m η = 44.4	x: 0 m η = 1.2	x: 0 m η = 20.0	x: 0 m η = 73.7	x: 0 m η = 75.2	x: 0 m η = 82.1	CUMPLE η = 82.1
N511/N510	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.121 m η = 0.8	x: 0 m η = 34.2	x: 0.374 m η = 2.1	x: 1.121 m η = 8.5	x: 1.121 m η = 25.8	x: 0.374 m η = 2.9	x: 1.121 m η = 0.8	x: 1.121 m η = 5.7	x: 1.121 m η = 26.7	x: 1.121 m η = 0.7	x: 1.121 m η = 7.2	N.P.[1]	x: 1.121 m η = 47.2	x: 1.121 m η = 47.7	CUMPLE η = 47.7
N512/N511	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 29.6	η = 1.5	x: 0 m η = 3.1	x: 0 m η = 30.4	η = 4.1	x: 0.933 m η = 0.2	x: 0 m η = 3.4	x: 0 m η = 31.0	x: 0 m η = 0.1	x: 0 m η = 9.8	N.P.[1]	x: 0 m η = 44.9	x: 0 m η = 50.7	CUMPLE η = 50.7
N513/N512	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.7 m η = 11.8	x: 0.7 m η = 24.4	x: 0.7 m η = 0.4	x: 0 m η = 11.3	x: 0 m η = 44.3	η = 5.4	x: 1.4 m η = 1.1	x: 0 m η = 11.4	x: 0 m η = 44.4	x: 0 m η = 1.3	x: 0 m η = 20.0	x: 0 m η = 74.8	x: 0 m η = 74.6	x: 0 m η = 79.4	CUMPLE η = 79.4
N344/N343	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.121 m η = 3.9	x: 0 m η = 35.2	x: 0.187 m η = 2.2	x: 1.121 m η = 8.7	x: 1.121 m η = 24.2	x: 0.187 m η = 2.7	x: 1.121 m η = 0.8	x: 1.121 m η = 7.0	x: 1.121 m η = 25.2	x: 1.121 m η = 0.8	x: 1.121 m η = 6.4	x: 1.121 m η = 7.2	x: 1.121 m η = 44.6	x: 1.121 m η = 46.1	CUMPLE η = 46.1
N345/N344	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 30.5	x: 0.7 m η = 2.0	x: 0 m η = 3.2	x: 0 m η = 28.9	x: 1.167 m η = 3.9	x: 0.7 m η = 0.2	x: 0 m η = 3.8	x: 0 m η = 29.8	x: 0 m η = 0.1	x: 0 m η = 9.0	N.P.[1]	x: 0 m η = 43.3	x: 0 m η = 48.1	CUMPLE η = 48.1
N346/N345	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.233 m η = 10.3	x: 0.233 m η = 22.8	η = 0.3	x: 0 m η = 12.4	x: 0 m η = 42.6	η = 5.2	x: 1.167 m η = 1.2	x: 0 m η = 12.5	x: 0 m η = 42.7	x: 0 m η = 1.6	x: 0 m η = 18.5	x: 0 m η = 71.3	x: 0 m η = 71.3	x: 0 m η = 76.0	CUMPLE η = 76.0
N381/N380	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.187 m η = 4.2	x: 0 m η = 34.9	x: 0.187 m η = 2.3	x: 1.121 m η = 8.6	x: 1.121 m η = 25.2	x: 0.187 m η = 2.8	x: 1.121 m η = 0.8	x: 1.121 m η = 8.7	x: 1.121 m η = 26.2	x: 1.121 m η = 0.8	x: 1.121 m η = 6.9	x: 1.121 m η = 7.5	x: 1.121 m η = 50.8	x: 1.121 m η = 49.6	CUMPLE η = 50.8
N382/N381	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.4 m η = 0.8	x: 0 m η = 30.3	η = 2.0	x: 0 m η = 3.1	x: 0 m η = 28.9	η = 3.9	x: 0 m η = 0.2	x: 0 m η = 3.1	x: 0 m η = 29.7	x: 0 m η = 0.1	x: 0 m η = 9.0	x: 0 m η = 41.1	x: 0 m η = 50.9	x: 0 m η = 54.6	CUMPLE η = 54.6
N383/N382	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.4 m η = 12.4	x: 0 m η = 25.3	η = 0.3	x: 0 m η = 12.5	x: 0 m η = 42.6	η = 5.2	x: 1.4 m η = 1.2	x: 0 m η = 12.6	x: 0 m η = 42.7	x: 0 m η = 1.6	x: 0 m η = 18.5	x: 0 m η = 70.1	x: 0 m η = 71.3	x: 0 m η = 78.5	CUMPLE η = 78.5
N246/N245	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.187 m η = 3.9	x: 0 m η = 34.9	η = 2.5	x: 1.121 m η = 8.7	x: 1.121 m η = 25.3	η = 2.9	x: 1.121 m η = 0.8	x: 1.121 m η = 8.7	x: 1.121 m η = 26.4	x: 1.121 m η = 0.8	x: 1.121 m η = 7.1	x: 1.121 m η = 7.2	x: 1.121 m η = 49.8	x: 1.121 m η = 48.7	CUMPLE η = 49.8
N247/N246	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.4 m η = 0.4	x: 0 m η = 30.3	x: 0.467 m η = 1.8	x: 0 m η = 3.1	x: 0 m η = 29.9	x: 0.467 m η = 4.0	x: 0 m η = 0.2	x: 0 m η = 3.2	x: 0 m η = 30.7	x: 0 m η = 0.1	x: 0 m η = 9.6	x: 0 m η = 41.7	x: 0 m η = 51.4	x: 0 m η = 55.4	CUMPLE η = 55.4
N248/N247	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.4 m η = 12.0	x: 0 m η = 24.8	η = 0.2	x: 0 m η = 12.3	x: 0 m η = 42.3	η = 5.2	x: 1.4 m η = 1.2	x: 0 m η = 12.4	x: 0 m η = 42.4	x: 0 m η = 1.6	x: 0 m η = 18.3	x: 0 m η = 68.9	x: 0 m η = 70.9	x: 0 m η = 77.7	CUMPLE η = 77.7
N283/N282	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.121 m η = 4.2	x: 0 m η = 35.1	x: 0.187 m η = 2.6	x: 1.121 m η = 8.7	x: 1.121 m η = 25.9	η = 2.9	x: 1.121 m η = 0.8	x: 1.121 m η = 7.0	x: 1.121 m η = 27.1	x: 1.121 m η = 0.8	x: 1.121 m η = 7.4	x: 1.121 m η = 7.3	x: 1.121 m η = 47.8	x: 1.121 m η = 48.0	CUMPLE η = 48.0
N284/N283	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 30.5	x: 1.167 m η = 1.8	x: 0 m η = 3.1	x: 0 m η = 29.8	x: 1.167 m η = 4.0	x: 0.7 m η = 0.2	x: 0 m η = 3.6	x: 0 m η = 30.6	x: 0 m η = 0.1	x: 0 m η = 9.5	N.P.[1]	x: 0 m η = 43.8	x: 0 m η = 49.2	CUMPLE η = 49.2
N285/N284	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.233 m η = 10.2	x: 0.233 m η = 22.7	η = 0.2	x: 0 m η = 12.6	x: 0 m η = 42.4	η = 5.2	x: 1.4 m η = 1.2	x: 0 m η = 12.7	x: 0 m η = 42.4	x: 0 m η = 1.6	x: 0 m η = 18.3	x: 0 m η = 70.7	x: 0 m η = 70.7	x: 0 m η = 75.5	CUMPLE η = 75.5
N116/N115	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.121 m η = 2.4	x: 0 m η = 34.3	η = 2.2	x: 1.121 m η = 8.5	x: 1.121 m η = 25.0	η = 2.8	x: 1.121 m η = 0.8	x: 1.121 m η = 6.3	x: 1.121 m η = 26.0	x: 1.121 m η = 0.7	x: 1.121 m η = 6.8	N.P.[1]	x: 1.121 m η = 47.7	x: 1.121 m η = 47.8	CUMPLE η = 47.8
N117/N116	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 29.9	x: 0.7 m η = 1.7	x: 0 m η = 3.0	x: 0 m η = 29.7	x: 0.7 m η = 4.0	x: 0.7 m η = 0.2	x: 0 m η = 3.5	x: 0 m η = 30.5	x: 0 m η = 0.1	x: 0 m η = 9.5	N.P.[1]	x: 0 m η = 43.3	x: 0 m η = 48.6	CUMPLE η = 48.6
N118/N117	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.467 m η = 9.9	x: 0.467 m η = 22.3	η = 0.2	x: 0 m η = 10.9	x: 0 m η = 42.5	x: 0.467 m η = 5.2	x: 1.167 m η = 1.1	x: 0 m η = 10.9	x: 0 m η = 42.5	x: 0 m η = 1.2	x: 0 m η = 18.3	x: 0 m η = 70.0	x: 0 m η = 70.2	x: 0 m η = 75.4	CUMPLE η = 75.4
N153/N152	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.121 m η = 3.0	x: 0 m η = 34.2	x: 0.187 m η = 2.3	x: 1.121 m η = 8.5	x: 1.121 m η = 25.5	x: 0 m η = 2.8	x: 1.121 m η = 0.8	x: 1.121 m η = 8.5	x: 1.121 m η = 26.5	x: 1.121 m η = 0.7	x: 1.121 m η = 7.1	x: 1.121 m η = 6.5	x: 1.121 m η = 50.0	x: 1.121 m η = 49.1	CUMPLE η = 50.0
N154/N153	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.4 m η = 0.6	x: 0 m η = 29.8	η = 1.7	x: 0 m η = 3.0	x: 0 m η = 29.7	η = 4.0	x: 0 m η = 0.2	x: 0 m η = 2.8	x: 0 m η = 30.4	x: 0 m η = 0.1	x: 0 m η = 9.4	x: 0 m η = 41.6	x: 0 m η = 51.1	x: 0 m η = 55.2	CUMPLE η = 55.2
N155/N154	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.4 m η = 12.2	x: 0 m η = 25.1	η = 0.2	x: 0 m η = 10.8	x: 0 m η = 42.3	η = 5.2	x: 1.4 m η = 1.1	x: 0 m η = 10.9	x: 0 m η = 42.4	x: 0 m η = 1.2	x: 0 m η = 18.2	x: 0 m η = 69.5	x: 0 m η = 70.9	x: 0 m η = 78.0	CUMPLE η = 78.0
N55/N54	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 1.121 m η = 2.6	x: 0 m η = 19.4	η = 2.8	x: 1.121 m η = 5.7	x: 1.121 m η = 25.9	η = 3.0	x: 0 m η = 0.7	x: 1.121 m η = 6.1	x: 1.121 m η = 27.1	x: 1.121 m η = 0.4	x: 1.121 m η = 7.5	N.P.[1]	x: 1.121 m η = 42.1	x: 1.121 m η = 42.3	CUMPLE η = 42.3
N56/N55	$w/t \leq (w/t)_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 16.3	x: 1.4 m η = 1.8	x: 0 m η = 1.8	x: 0 m η = 29.5	x: 1.4 m η = 3.9	x: 0.933 m η = 0.1	x: 0 m η = 2.6	x: 0 m η = 30.3	x: 0 m η = 0.1	x: 0 m η = 9.3	N.P.[1]	x: 0 m η = 40.5	x: 0 m η = 45.3	CUMPLE η = 45.3
N755/N56	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.7 m η = 12.2	x: 0.7 m η = 20.6	x: 0.7 m η = 0.2	x: 0 m η = 10.2	x: 0 m η = 41.9	η = 5.1	x: 1.4 m η = 1.0	x: 0 m η = 10.3	x: 0 m η = 42.0	x: 0 m η = 1.1	x: 0 m η = 17.9	x: 0 m η = 70.9	x: 0 m η = 67.4	x: 0 m η = 72.1	CUMPLE η = 72.1

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N47/N46	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.121 m η = 2.0	x: 0 m η = 17.2	x: 0.187 m η = 2.8	x: 1.121 m η = 7.6	x: 1.121 m η = 27.0	x: 0.187 m η = 3.1	x: 1.121 m η = 0.8	x: 1.121 m η = 7.9	x: 1.121 m η = 28.2	x: 1.121 m η = 0.6	x: 1.121 m η = 8.1	x: 1.121 m η = 5.6	x: 1.121 m η = 40.5	x: 1.121 m η = 41.6	CUMPLE η = 41.6
N48/N47	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 14.3	x: 0.933 m η = 1.7	x: 0 m η = 2.2	x: 0 m η = 30.6	x: 0.933 m η = 4.1	x: 0.7 m η = 0.2	x: 0 m η = 3.0	x: 0 m η = 31.4	x: 0 m η = 0.1	x: 0 m η = 10.0	N.P.[1]	x: 0 m η = 41.3	x: 0 m η = 46.6	CUMPLE η = 46.6
N78/N48	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.467 m η = 13.3	x: 0.467 m η = 20.6	x: 0.467 m η = 0.2	x: 0 m η = 10.3	x: 0 m η = 43.2	η = 5.3	x: 1.4 m η = 1.0	x: 0 m η = 10.4	x: 0 m η = 43.3	x: 0 m η = 1.1	x: 0 m η = 19.1	x: 0 m η = 73.9	x: 0 m η = 68.4	x: 0 m η = 73.9	CUMPLE η = 73.9
N107/N106	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.121 m η = 1.8	x: 0 m η = 35.2	η = 2.6	x: 1.121 m η = 9.7	x: 1.121 m η = 26.5	η = 2.9	x: 1.121 m η = 0.9	x: 1.121 m η = 6.7	x: 1.121 m η = 27.7	x: 1.121 m η = 1.0	x: 1.121 m η = 7.7	N.P.[1]	x: 1.121 m η = 50.2	x: 1.121 m η = 50.0	CUMPLE η = 50.2
N108/N107	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 30.4	x: 0.7 m η = 1.9	x: 0 m η = 3.2	x: 0 m η = 30.9	x: 0.7 m η = 4.2	x: 0.7 m η = 0.2	x: 0 m η = 3.6	x: 0 m η = 31.7	x: 0 m η = 0.1	x: 0 m η = 10.2	N.P.[1]	x: 0 m η = 44.7	x: 0 m η = 50.2	CUMPLE η = 50.2
N109/N108	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.467 m η = 10.0	x: 0.467 m η = 22.5	η = 0.2	x: 0 m η = 11.1	x: 0 m η = 44.2	x: 0.467 m η = 5.4	x: 1.4 m η = 1.1	x: 0 m η = 11.1	x: 0 m η = 44.2	x: 0 m η = 1.2	x: 0 m η = 19.9	x: 0 m η = 72.1	x: 0 m η = 71.6	x: 0 m η = 77.6	CUMPLE η = 77.6
N146/N144	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.121 m η = 2.0	x: 0 m η = 35.0	x: 0 m η = 2.6	x: 1.121 m η = 9.7	x: 1.121 m η = 27.0	x: 0 m η = 3.0	x: 1.121 m η = 0.9	x: 1.121 m η = 9.7	x: 1.121 m η = 28.2	x: 1.121 m η = 0.9	x: 1.121 m η = 8.0	N.P.[1]	x: 1.121 m η = 50.8	x: 1.121 m η = 49.8	CUMPLE η = 50.8
N145/N146	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 30.3	η = 1.9	x: 0 m η = 3.2	x: 0 m η = 30.8	η = 4.2	x: 0 m η = 0.2	x: 0 m η = 3.1	x: 0 m η = 31.7	x: 0 m η = 0.1	x: 0 m η = 10.2	N.P.[1]	x: 0 m η = 51.8	x: 0 m η = 56.1	CUMPLE η = 56.1
N176/N145	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.167 m η = 12.7	x: 1.167 m η = 25.7	η = 0.2	x: 0 m η = 10.7	x: 0 m η = 44.0	η = 5.4	x: 1.167 m η = 1.1	x: 0 m η = 10.7	x: 0 m η = 44.1	x: 0 m η = 1.2	x: 0 m η = 19.7	x: 0 m η = 72.0	x: 0 m η = 72.8	x: 0 m η = 80.3	CUMPLE η = 80.3
N237/N236	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.121 m η = 3.3	x: 0 m η = 35.2	η = 2.6	x: 1.121 m η = 9.7	x: 1.121 m η = 26.4	η = 3.0	x: 1.121 m η = 0.9	x: 1.121 m η = 9.7	x: 1.121 m η = 27.6	x: 1.121 m η = 1.0	x: 1.121 m η = 7.7	x: 1.121 m η = 6.1	x: 1.121 m η = 50.7	x: 1.121 m η = 49.5	CUMPLE η = 50.7
N238/N237	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.4 m η = 0.1	x: 0 m η = 30.5	x: 0.467 m η = 1.9	x: 0 m η = 3.2	x: 0 m η = 30.7	x: 0.467 m η = 4.1	x: 1.4 m η = 0.2	x: 0 m η = 3.1	x: 0 m η = 31.5	x: 0 m η = 0.1	x: 0 m η = 10.1	x: 0 m η = 42.7	x: 0 m η = 51.9	x: 0 m η = 56.2	CUMPLE η = 56.2
N239/N238	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.4 m η = 12.3	x: 0 m η = 25.3	η = 0.2	x: 0 m η = 12.1	x: 0 m η = 43.7	η = 5.4	x: 1.4 m η = 1.2	x: 0 m η = 12.1	x: 0 m η = 43.8	x: 0 m η = 1.5	x: 0 m η = 19.5	x: 0 m η = 71.6	x: 0 m η = 72.6	x: 0 m η = 80.0	CUMPLE η = 80.0
N276/N274	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.121 m η = 3.1	x: 0 m η = 35.4	η = 2.7	x: 1.121 m η = 9.8	x: 1.121 m η = 26.8	η = 3.0	x: 1.121 m η = 0.9	x: 1.121 m η = 7.3	x: 1.121 m η = 28.0	x: 1.121 m η = 1.0	x: 1.121 m η = 7.9	x: 1.121 m η = 5.5	x: 1.121 m η = 51.2	x: 1.121 m η = 50.7	CUMPLE η = 51.2
N275/N276	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 30.7	x: 1.167 m η = 1.9	x: 0 m η = 3.2	x: 0 m η = 30.7	x: 1.4 m η = 4.1	x: 0.7 m η = 0.2	x: 0 m η = 3.6	x: 0 m η = 31.5	x: 0 m η = 0.1	x: 0 m η = 10.1	N.P.[1]	x: 0 m η = 44.8	x: 0 m η = 50.3	CUMPLE η = 50.3
N306/N275	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0 m η = 10.1	x: 0 m η = 22.7	x: 0 m η = 0.2	x: 0 m η = 12.2	x: 0 m η = 43.7	η = 5.4	x: 1.4 m η = 1.2	x: 0 m η = 12.3	x: 0 m η = 43.8	x: 0 m η = 1.5	x: 0 m η = 19.5	x: 0 m η = 72.1	x: 0 m η = 72.0	x: 0 m η = 77.4	CUMPLE η = 77.4
N335/N334	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.121 m η = 3.1	x: 0 m η = 35.4	η = 2.6	x: 1.121 m η = 9.8	x: 1.121 m η = 26.5	x: 0.187 m η = 3.0	x: 1.121 m η = 0.9	x: 1.121 m η = 7.2	x: 1.121 m η = 27.7	x: 1.121 m η = 1.0	x: 1.121 m η = 7.7	x: 1.121 m η = 5.5	x: 1.121 m η = 48.6	x: 1.121 m η = 48.7	CUMPLE η = 48.7
N336/N335	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 30.7	x: 1.4 m η = 1.9	x: 0 m η = 3.2	x: 0 m η = 30.7	x: 1.167 m η = 4.1	x: 0.7 m η = 0.2	x: 0 m η = 3.6	x: 0 m η = 31.5	x: 0 m η = 0.1	x: 0 m η = 10.1	N.P.[1]	x: 0 m η = 44.9	x: 0 m η = 50.3	CUMPLE η = 50.3
N337/N336	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.4 m η = 10.1	x: 0 m η = 22.7	η = 0.1	x: 0 m η = 12.2	x: 0 m η = 43.8	η = 5.4	x: 1.167 m η = 1.2	x: 0 m η = 12.2	x: 0 m η = 43.8	x: 0 m η = 1.5	x: 0 m η = 19.5	x: 0 m η = 71.9	x: 0 m η = 71.7	x: 0 m η = 77.3	CUMPLE η = 77.3
N374/N372	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.121 m η = 3.4	x: 0 m η = 35.1	x: 0 m η = 2.6	x: 1.121 m η = 9.7	x: 1.121 m η = 26.6	x: 0.187 m η = 3.0	x: 1.121 m η = 0.9	x: 1.121 m η = 9.7	x: 1.121 m η = 27.7	x: 1.121 m η = 1.0	x: 1.121 m η = 7.8	x: 1.121 m η = 6.1	x: 1.121 m η = 50.9	x: 1.121 m η = 49.7	CUMPLE η = 50.9
N373/N374	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.4 m η = 0.2	x: 0 m η = 30.5	x: 0.467 m η = 1.9	x: 0 m η = 3.2	x: 0 m η = 30.8	x: 0.467 m η = 4.2	x: 1.4 m η = 0.2	x: 0 m η = 3.1	x: 0 m η = 31.6	x: 0 m η = 0.1	x: 0 m η = 10.2	x: 0 m η = 42.7	x: 0 m η = 52.0	x: 0 m η = 56.2	CUMPLE η = 56.2
N404/N373	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.4 m η = 12.3	x: 0 m η = 25.3	η = 0.1	x: 0 m η = 12.2	x: 0 m η = 43.8	η = 5.4	x: 1.4 m η = 1.2	x: 0 m η = 12.2	x: 0 m η = 43.8	x: 0 m η = 1.5	x: 0 m η = 19.5	x: 0 m η = 71.5	x: 0 m η = 72.6	x: 0 m η = 80.0	CUMPLE η = 80.0
N465/N464	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 35.1	x: 0.187 m η = 2.4	x: 1.121 m η = 9.7	x: 1.121 m η = 26.0	η = 2.9	x: 1.121 m η = 0.9	x: 1.121 m η = 9.7	x: 1.121 m η = 27.1	x: 1.121 m η = 1.0	x: 1.121 m η = 7.4	N.P.[1]	x: 1.121 m η = 49.8	x: 1.121 m η = 48.8	CUMPLE η = 49.8
N466/N465	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.4 m η < 0.1	x: 0 m η = 30.4	x: 0.7 m η = 1.8	x: 0 m η = 3.2	x: 0 m η = 29.9	x: 0.7 m η = 4.1	x: 0 m η = 0.2	x: 0 m η = 3.0	x: 0 m η = 30.7	x: 0 m η = 0.1	x: 0 m η = 9.6	x: 1.4 m η = 37.9	x: 0 m η = 50.9	x: 0 m η = 55.1	CUMPLE η = 55.1
N467/N466	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 1.4 m η = 13.0	x: 1.4 m η = 26.0	η < 0.1	x: 0 m η = 9.6	x: 0 m η = 44.6	η = 5.5	x: 1.167 m η = 0.9	x: 0 m η = 9.6	x: 0 m η = 44.6	x: 0 m η = 0.9	x: 0 m η = 20.2	x: 0 m η = 72.5	x: 0 m η = 73.5	x: 0 m η = 80.9	CUMPLE η = 80.9
N504/N502	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 35.2	η = 2.4	x: 1.121 m η = 9.7	x: 1.121 m η = 25.9	x: 0.187 m η = 2.9	x: 1.121 m η = 0.9	x: 1.121 m η = 5.9	x: 1.121 m η = 26.9	x: 1.121 m η = 1.0	x: 1.121 m η = 7.3	N.P.[1]	x: 1.121 m η = 48.6	x: 1.121 m η = 48.4	CUMPLE η = 48.6
N503/N504	w / t ≤ (w / t)$_{Máx.}$ Cumple	N.P.[4]	x: 0 m η = 30.4	x: 0.7 m η = 1.8	x: 0 m η = 3.2	x: 0 m η = 29.9	η = 4.1	x: 0.7 m η = 0.2	x: 0 m η = 3.5	x: 0 m η = 30.7	x: 0 m η = 0.1	x: 0 m η = 9.6	N.P.[1]	x: 0 m η = 44.2	x: 0 m η = 49.7	CUMPLE η = 49.7
N534/N503	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.7 m η = 10.0	x: 0.7 m η = 22.4	η < 0.1	x: 0 m η = 9.6	x: 0 m η = 44.5	η = 5.5	x: 1.167 m η = 0.9	x: 0 m η = 9.6	x: 0 m η = 44.5	x: 0 m η = 0.9	x: 0 m η = 20.1	x: 0 m η = 71.9	x: 0 m η = 71.3	x: 0 m η = 77.8	CUMPLE η = 77.8
N794/N575	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.525 m η = 28.2	x: 0.525 m η = 26.1	x: 0.35 m η = 10.8	x: 0.7 m η = 10.5	x: 0 m η = 47.2	x: 0.525 m η = 7.5	x: 0.525 m η = 2.4	x: 0 m η = 13.1	x: 0 m η = 51.9	x: 0 m η = 1.8	x: 0 m η = 27.5	x: 0 m η = 88.4	x: 0 m η = 90.8	x: 0 m η = 87.1	CUMPLE η = 88.4
N793/N614	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.7 m η = 25.8	x: 0.7 m η = 23.2	x: 0 m η = 10.8	x: 0.7 m η = 10.5	x: 0 m η = 47.2	x: 0.35 m η = 7.5	x: 0.7 m η = 2.2	x: 0 m η = 13.4	x: 0 m η = 51.9	x: 0 m η = 1.8	x: 0 m η = 27.5	x: 0 m η = 86.0	x: 0 m η = 88.6	x: 0 m η = 84.3	CUMPLE η = 86.0
N797/N513	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.525 m η = 29.7	x: 0.525 m η = 26.4	x: 0.525 m η = 11.1	x: 0.7 m η = 11.8	x: 0 m η = 47.5	x: 0.35 m η = 7.5	x: 0.525 m η = 2.5	x: 0.7 m η = 14.1	x: 0 m η = 52.4	x: 0.7 m η = 2.1	x: 0 m η = 28.0	x: 0 m η = 85.6	x: 0 m η = 92.3	x: 0 m η = 88.8	CUMPLE η = 85.6
N798/N476	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.7 m η = 26.2	x: 0.7 m η = 22.4	x: 0.35 m η = 11.1	x: 0.7 m η = 11.6	x: 0 m η = 47.6	x: 0.7 m η = 7.5	x: 0.7 m η = 2.2	x: 0 m η = 13.4	x: 0 m η = 52.4	x: 0 m η = 1.8	x: 0 m η = 28.0	x: 0 m η = 97.3	x: 0 m η = 88.4	x: 0 m η = 85.6	CUMPLE η = 97.3
N799/N383	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0 m η = 38.0	x: 0 m η = 33.3	η = 12.8	x: 0.7 m η = 17.0	x: 0 m η = 55.9	η = 9.6	x: 0 m η = 3.2	x: 0.7 m η = 17.4	x: 0 m η = 61.6	x: 0.7 m η = 3.1	x: 0 m η = 38.9	x: 0 m η = 27.7	x: 0 m η = 14.7	x: 0 m η = 16.9	CUMPLE η = 27.7
N800/N346	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0 m η = 38.0	x: 0 m η = 33.3	x: 0.175 m η = 12.8	x: 0.7 m η = 17.0	x: 0 m η = 55.9	x: 0.525 m η = 9.6	x: 0 m η = 3.2	x: 0.7 m η = 17.5	x: 0 m η = 61.5	x: 0.7 m η = 3.2	x: 0 m η = 38.8	x: 0 m η = 32.2	x: 0 m η = 19.8	x: 0 m η = 15.8	CUMPLE η = 32.2
N801/N285	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0 m η = 37.8	x: 0 m η = 33.1	x: 0.525 m η = 12.3	x: 0.7 m η = 17.1	x: 0 m η = 55.0	x: 0 m η = 9.4	x: 0 m η = 3.2	x: 0.7 m η = 17.5	x: 0 m η = 60.4	x: 0.7 m η = 3.2	x: 0 m η = 37.4	x: 0 m η = 29.4	x: 0 m η = 17.3	x: 0 m η = 11.6	CUMPLE η = 29.4
N802/N248	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0 m η = 37.1	x: 0 m η = 32.3	x: 0.35 m η = 12.3	x: 0.7 m η = 16.8	x: 0 m η = 55.0	x: 0 m η = 9.4	x: 0 m η = 3.1	x: 0.7 m η = 16.9	x: 0 m η = 60.4	x: 0.7 m η = 3.0	x: 0 m η = 37.4	x: 0 m η = 24.8	x: 0 m η = 12.2	x: 0 m η = 12.7	CUMPLE η = 24.8
N803/N155	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0 m η = 32.0	x: 0 m η = 27.3	x: 0.35 m η = 12.1	x: 0.7 m η = 14.7	x: 0 m η = 55.0	x: 0.35 m η = 9.5	x: 0 m η = 2.7	x: 0.7 m η = 14.9	x: 0 m η = 60.4	x: 0.7 m η = 2.3	x: 0 m η = 37.3	x: 0 m η = 23.8	x: 0 m η = 11.6	x: 0 m η = 11.0	CUMPLE η = 23.8
N804/N118	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.525 m η = 35.5	x: 0.525 m η = 31.2	x: 0.525 m η = 12.1	x: 0.7 m η = 15.0	x: 0 m η = 55.1	x: 0.525 m η = 9.5	x: 0.525 m η = 3.0	x: 0.7 m η = 16.5	x: 0 m η = 60.4	x: 0.7 m η = 2.8	x: 0 m η = 37.4	x: 0 m η = 28.2	x: 0 m η = 16.8	x: 0 m η = 19.7	CUMPLE η = 28.2
N805/N755	w / t ≤ (w / t)$_{Máx.}$ Cumple	x: 0.525 m η = 34.2	x: 0.525 m η = 31.4	η = 12.2	x: 0.7 m η = 13.6	x: 0 m η = 54.5	x: 0.7 m η = 9.3	x: 0.525 m η = 2.9	x: 0.7 m η = 15.8	x: 0 m η = 60.0	x: 0.7 m η = 2.6	x: 0 m η = 36.8	x: 0 m η = 26.4	x: 0 m η = 16.0	x: 0 m η = 15.7	CUMPLE η = 26.4

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Barras	COMPROBACIONES (AISI S100-16 (2016))															Estado
	w / t	T	P	Tr	M_x	M_y	V_x	V_y	M_xTr	M_yTr	M_xV_y	M_yV_x	MT	MP	TPTrMV	
N806/N756	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 31.7	x: 0 m η = 26.5	x: 0.7 m η = 12.3	x: 0.7 m η = 13.7	x: 0 m η = 54.6	x: 0 m η = 9.4	x: 0.7 m η = 2.7	x: 0 m η = 15.2	x: 0 m η = 60.1	x: 0 m η = 2.4	x: 0 m η = 37.0	x: 0 m η = 23.5	x: 0 m η = 13.3	x: 0 m η = 99.3	CUMPLE η = 23.5
N817/N636	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.7 m η = 26.7	x: 0.7 m η = 22.8	x: 0.35 m η = 11.3	x: 0.7 m η = 10.0	x: 0 m η = 51.9	x: 0 m η = 8.3	x: 0.7 m η = 2.2	x: 0 m η = 13.9	x: 0 m η = 56.9	x: 0 m η = 2.0	x: 0 m η = 33.0	x: 0 m η = 13.8	x: 0 m η = 93.7	x: 0 m η = 91.2	CUMPLE η = 13.8
N818/N565	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.525 m η = 34.8	x: 0.525 m η = 30.8	x: 0.525 m η = 12.1	x: 0.7 m η = 11.6	x: 0 m η = 52.5	x: 0.7 m η = 8.8	x: 0.525 m η = 2.9	x: 0.7 m η = 15.9	x: 0 m η = 57.8	x: 0.7 m η = 2.6	x: 0 m η = 34.2	x: 0 m η = 25.3	x: 0 m η = 13.8	x: 0 m η = 13.1	CUMPLE η = 25.3
N819/N534	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.525 m η = 35.0	x: 0.525 m η = 29.6	x: 0.35 m η = 12.4	x: 0.7 m η = 13.2	x: 0 m η = 57.5	x: 0.35 m η = 9.9	x: 0.525 m η = 2.9	x: 0.7 m η = 16.3	x: 0 m η = 63.0	x: 0.7 m η = 2.8	x: 0 m η = 40.7	x: 0 m η = 31.4	x: 0 m η = 18.1	x: 0 m η = 15.5	CUMPLE η = 31.4
N820/N467	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.525 m η = 34.0	x: 0.525 m η = 28.4	x: 0.525 m η = 12.4	x: 0.7 m η = 13.1	x: 0 m η = 57.5	x: 0.525 m η = 9.9	x: 0.525 m η = 2.8	x: 0 m η = 15.3	x: 0 m η = 63.0	x: 0 m η = 2.4	x: 0 m η = 40.7	x: 0 m η = 30.2	x: 0 m η = 16.4	x: 0 m η = 12.4	CUMPLE η = 30.2
N821/N404	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 37.1	x: 0 m η = 32.3	x: 0.7 m η = 12.7	x: 0.7 m η = 16.6	x: 0 m η = 57.3	x: 0.7 m η = 9.9	x: 0 m η = 3.1	x: 0.7 m η = 16.9	x: 0 m η = 62.9	x: 0.7 m η = 2.9	x: 0 m η = 40.5	x: 0 m η = 30.3	x: 0 m η = 17.2	x: 0 m η = 12.1	CUMPLE η = 30.3
N822/N337	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 37.2	x: 0 m η = 32.4	x: 0.525 m η = 12.6	x: 0.7 m η = 16.7	x: 0 m η = 57.2	x: 0.175 m η = 9.8	x: 0 m η = 3.1	x: 0.7 m η = 17.0	x: 0 m η = 62.8	x: 0.7 m η = 3.0	x: 0 m η = 40.4	x: 0 m η = 32.4	x: 0 m η = 19.5	x: 0 m η = 16.8	CUMPLE η = 32.4
N823/N306	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 36.9	x: 0 m η = 32.0	x: 0.525 m η = 12.7	x: 0.7 m η = 16.7	x: 0 m η = 57.1	x: 0 m η = 9.8	x: 0 m η = 3.1	x: 0.7 m η = 17.0	x: 0 m η = 62.8	x: 0.7 m η = 3.0	x: 0 m η = 40.4	x: 0 m η = 32.5	x: 0 m η = 19.7	x: 0 m η = 16.7	CUMPLE η = 32.5
N824/N239	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0 m η = 36.7	x: 0 m η = 31.8	x: 0.35 m η = 12.7	x: 0.7 m η = 16.5	x: 0 m η = 57.1	x: 0 m η = 9.8	x: 0 m η = 3.1	x: 0.7 m η = 16.7	x: 0 m η = 62.8	x: 0.7 m η = 2.9	x: 0 m η = 40.4	x: 0 m η = 30.3	x: 0 m η = 17.1	x: 0 m η = 12.0	CUMPLE η = 30.3
N825/N176	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.525 m η = 34.7	x: 0.525 m η = 29.3	x: 0.35 m η = 12.8	x: 0.7 m η = 14.6	x: 0 m η = 57.4	x: 0.35 m η = 9.9	x: 0.525 m η = 2.9	x: 0.7 m η = 15.6	x: 0 m η = 63.0	x: 0.7 m η = 2.5	x: 0 m η = 40.7	x: 0 m η = 30.5	x: 0 m η = 17.0	x: 0 m η = 12.4	CUMPLE η = 30.5
N826/N109	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.525 m η = 35.8	x: 0.525 m η = 30.6	x: 0.525 m η = 12.8	x: 0.7 m η = 15.0	x: 0 m η = 57.5	x: 0.525 m η = 9.9	x: 0.525 m η = 3.0	x: 0.7 m η = 16.8	x: 0 m η = 63.1	x: 0.7 m η = 2.9	x: 0 m η = 40.8	x: 0 m η = 32.3	x: 0 m η = 19.0	x: 0 m η = 16.6	CUMPLE η = 32.3
N827/N78	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.525 m η = 35.1	x: 0.525 m η = 31.1	x: 0.175 m η = 12.6	x: 0.7 m η = 13.7	x: 0 m η = 56.3	x: 0.175 m η = 9.6	x: 0.525 m η = 2.9	x: 0.7 m η = 16.2	x: 0 m η = 61.8	x: 0.7 m η = 2.7	x: 0 m η = 39.2	x: 0 m η = 30.3	x: 0 m η = 17.9	x: 0 m η = 12.2	CUMPLE η = 30.3
N828/N10	$w/t \leq (w/t)_{Máx.}$ Cumple	x: 0.525 m η = 34.4	x: 0.525 m η = 30.0	x: 0.525 m η = 12.7	x: 0.7 m η = 13.9	x: 0 m η = 56.4	x: 0.525 m η = 9.7	x: 0.525 m η = 2.9	x: 0 m η = 15.8	x: 0 m η = 61.9	x: 0 m η = 2.6	x: 0 m η = 39.3	x: 0 m η = 28.9	x: 0 m η = 16.7	x: 0 m η = 18.4	CUMPLE η = 28.9

Notación:
w / t: Limitaciones geométricas
T: Resistencia a tracción
P: Resistencia a compresión
Tr: Resistencia a torsión
M_x: Resistencia a flexión alrededor del eje X
M_y: Resistencia a flexión alrededor del eje Y
V_x: Resistencia a corte en la dirección del eje X
V_y: Resistencia a corte en la dirección del eje Y
M_xTr: Resistencia a flexión alrededor del eje X combinada con torsión
M_yTr: Resistencia a flexión alrededor del eje Y combinada con torsión
M_xV_y: Resistencia a flexión alrededor del eje X combinada con corte en la dirección del eje Y
M_yV_x: Resistencia a flexión alrededor del eje Y combinada con corte en la dirección del eje X
MT: Resistencia a flexión combinada con tracción
MP: Resistencia a flexión combinada con compresión
TPTrMV: Flexión combinada con cortante, axil y torsión - Comprobación de Von Mises
x: Distancia al origen de la barra
η: Coeficiente de aprovechamiento (%)
N.P.: No procede

Comprobaciones que no proceden (N.P.):
(1) No hay interacción entre axil de tracción y momento flector para ninguna combinación. Por lo tanto, la comprobación no procede.
(2) La comprobación no procede, ya que no hay axil de compresión.
(3) No hay interacción entre axil de compresión y momento flector para ninguna combinación. Por lo tanto, la comprobación no procede.
(4) La comprobación no procede, ya que no hay axil de tracción.
(5) La comprobación no procede, ya que no hay torsión.
(6) No hay interacción entre torsión y flexión alrededor del eje X para ninguna combinación. Por lo tanto, la comprobación no procede.
(7) No hay interacción entre torsión y flexión alrededor del eje Y para ninguna combinación. Por lo tanto, la comprobación no procede.

2.2.2. Pilares

2.2.2.1. Comprobaciones E.L.U. y E.L.S.

En las tablas de comprobación de pilares de acero no se muestran las comprobaciones con coeficiente de aprovechamiento inferior al 10%.

Disp.: Disposiciones relativas a las armaduras

Arm.: Armadura mínima y máxima

Q: Estado límite de agotamiento frente a cortante

N,M: Estado límite de agotamiento frente a solicitaciones normales

Disp. S.: Criterios de diseño por sismo

Cap.: Diseño por capacidad

2.2.2.1.1. P1

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 210 cm)	50x50	Cabeza	Cumple	Cumple	N.P.(2)	1.0	Cumple	Cumple	1.0	G(3)	N,M	-0.92	0.00	0.00	0.00	0.00	Cumple
		Pie	Cumple	Cumple	N.P.(2)	0.2	Cumple	Cumple	0.2	G(3)	N,M	0.92	0.00	0.00	0.00	0.00	Cumple
Nivel 1	50x50	Arranque	N.P.(1)	N.P.(1)	N.P.(2)	0.2	N.P.(1)	Cumple	0.2	G(3)	N,M	0.92	0.00	0.00	0.00	0.00	Cumple

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Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	

Notas:
(1) La comprobación no procede
(2) La comprobación no procede, ya que no hay esfuerzo cortante.
(3) 1.4·PP+1.4·CM1

2.2.2.1.2. P2

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 210 cm)	50x50	Cabeza	Cumple	Cumple	N.P.(2)	1.0	Cumple	Cumple	1.0	G(3)	N,M	-0.92	0.00	0.00	0.00	0.00	Cumple
		Pie	Cumple	Cumple	N.P.(2)	0.2	Cumple	Cumple	0.2	G(3)	N,M	0.92	0.00	0.00	0.00	0.00	Cumple
Nivel 1	50x50	Arranque	N.P.(1)	N.P.(1)	N.P.(2)	0.2	N.P.(1)	Cumple	0.2	G(3)	N,M	0.92	0.00	0.00	0.00	0.00	Cumple

Notas:
(1) La comprobación no procede
(2) La comprobación no procede, ya que no hay esfuerzo cortante.
(3) 1.4·PP+1.4·CM1

2.2.2.1.3. P3

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 210 cm)	50x50	Cabeza	Cumple	Cumple	N.P.(2)	1.0	Cumple	Cumple	1.0	G(3)	N,M	-0.92	0.00	0.00	0.00	0.00	Cumple
		Pie	Cumple	Cumple	N.P.(2)	0.2	Cumple	Cumple	0.2	G(3)	N,M	0.92	0.00	0.00	0.00	0.00	Cumple
Nivel 1	50x50	Arranque	N.P.(1)	N.P.(1)	N.P.(2)	0.2	N.P.(1)	Cumple	0.2	G(3)	N,M	0.92	0.00	0.00	0.00	0.00	Cumple

Notas:
(1) La comprobación no procede
(2) La comprobación no procede, ya que no hay esfuerzo cortante
(3) 1.4·PP+1.4·CM1

2.2.2.1.4. P4

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 210 cm)	50x50	Cabeza	Cumple	Cumple	N.P.(2)	1.0	Cumple	Cumple	1.0	G(3)	N,M	-0.92	0.00	0.00	0.00	0.00	Cumple
		Pie	Cumple	Cumple	N.P.(2)	0.2	Cumple	Cumple	0.2	G(3)	N,M	0.92	0.00	0.00	0.00	0.00	Cumple
Nivel 1	50x50	Arranque	N.P.(1)	N.P.(1)	N.P.(2)	0.2	N.P.(1)	Cumple	0.2	G(3)	N,M	0.92	0.00	0.00	0.00	0.00	Cumple

Notas:
(1) La comprobación no procede
(2) La comprobación no procede, ya que no hay esfuerzo cortante.
(3) 1.4·PP+1.4·CM1

2.2.2.1.5. P5

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 210 cm)	50x50	Cabeza	Cumple	Cumple	N.P.(2)	1.0	Cumple	Cumple	1.0	G(3)	N,M	-0.92	0.00	0.00	0.00	0.00	Cumple
		Pie	Cumple	Cumple	N.P.(2)	0.2	Cumple	Cumple	0.2	G(3)	N,M	0.92	0.00	0.00	0.00	0.00	Cumple
Nivel 1	50x50	Arranque	N.P.(1)	N.P.(1)	N.P.(2)	0.2	N.P.(1)	Cumple	0.2	G(3)	N,M	0.92	0.00	0.00	0.00	0.00	Cumple

Notas:
(1) La comprobación no procede
(2) La comprobación no procede, ya que no hay esfuerzo cortante.
(3) 1.4·PP+1.4·CM1

2.2.2.1.6. P6

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 210 cm)	50x50	Cabeza	Cumple	Cumple	N.P.[2]	1.0	Cumple	Cumple	1.0	G[3]	N,M	-0.92	0.00	0.00	0.00	0.00	Cumple
		Pie	Cumple	Cumple	N.P.[2]	0.2	Cumple	Cumple	0.2	G[3]	N,M	0.92	0.00	0.00	0.00	0.00	Cumple
Nivel 1	50x50	Arranque	N.P.[1]	N.P.[1]	N.P.[2]	0.2	N.P.[1]	Cumple	0.2	G[3]	N,M	0.92	0.00	0.00	0.00	0.00	Cumple

Notas:
[1] La comprobación no procede
[2] La comprobación no procede, ya que no hay esfuerzo cortante.
[3] 1.4·PP+1.4·CM1

2.2.2.1.7. P7

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 210 cm)	50x50	Cabeza	Cumple	Cumple	N.P.[2]	1.0	Cumple	Cumple	1.0	G[3]	N,M	-0.92	0.00	0.00	0.00	0.00	Cumple
		Pie	Cumple	Cumple	N.P.[2]	0.2	Cumple	Cumple	0.2	G[3]	N,M	0.92	0.00	0.00	0.00	0.00	Cumple
Nivel 1	50x50	Arranque	N.P.[1]	N.P.[1]	N.P.[2]	0.2	N.P.[1]	Cumple	0.2	G[3]	N,M	0.92	0.00	0.00	0.00	0.00	Cumple

Notas:
[1] La comprobación no procede
[2] La comprobación no procede, ya que no hay esfuerzo cortante.
[3] 1.4·PP+1.4·CM1

2.2.2.1.8. P8

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 210 cm)	50x50	Cabeza	Cumple	Cumple	N.P.[2]	1.0	Cumple	Cumple	1.0	G[3]	N,M	-0.92	0.00	0.00	0.00	0.00	Cumple
		Pie	Cumple	Cumple	N.P.[2]	0.2	Cumple	Cumple	0.2	G[3]	N,M	0.92	0.00	0.00	0.00	0.00	Cumple
Nivel 1	50x50	Arranque	N.P.[1]	N.P.[1]	N.P.[2]	0.2	N.P.[1]	Cumple	0.2	G[3]	N,M	0.92	0.00	0.00	0.00	0.00	Cumple

Notas:
[1] La comprobación no procede
[2] La comprobación no procede, ya que no hay esfuerzo cortante.
[3] 1.4·PP+1.4·CM1

2.2.2.1.9. P9

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 210 cm)	50x50	Cabeza	Cumple	Cumple	N.P.[2]	1.0	Cumple	Cumple	1.0	G[3]	N,M	-0.92	0.00	0.00	0.00	0.00	Cumple
		Pie	Cumple	Cumple	N.P.[2]	0.2	Cumple	Cumple	0.2	G[3]	N,M	0.92	0.00	0.00	0.00	0.00	Cumple
Nivel 1	50x50	Arranque	N.P.[1]	N.P.[1]	N.P.[2]	0.2	N.P.[1]	Cumple	0.2	G[3]	N,M	0.92	0.00	0.00	0.00	0.00	Cumple

Notas:
[1] La comprobación no procede
[2] La comprobación no procede, ya que no hay esfuerzo cortante.
[3] 1.4·PP+1.4·CM1

2.2.2.1.10. P10

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 210 cm)	50x50	Cabeza	Cumple	Cumple	N.P.[2]	1.0	Cumple	Cumple	1.0	G[3]	N,M	-0.92	0.00	0.00	0.00	0.00	Cumple
		Pie	Cumple	Cumple	N.P.[2]	0.2	Cumple	Cumple	0.2	G[3]	N,M	0.92	0.00	0.00	0.00	0.00	Cumple

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Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 1	50x50	Arranque	N.P.[1]	N.P.[1]	N.P.[2]	0.2	N.P.[1]	Cumple	0.2	G[3]	N,M	0.92	0.00	0.00	0.00	0.00	Cumple

Notas:
[1] La comprobación no procede
[2] La comprobación no procede, ya que no hay esfuerzo cortante.
[3] 1.4·PP+1.4·CM1

2.2.2.1.11. P11

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 210 cm)	50x50	Cabeza	Cumple	Cumple	N.P.[2]	1.0	Cumple	Cumple	1.0	G[3]	N,M	-0.92	0.00	0.00	0.00	0.00	Cumple
		Pie	Cumple	Cumple	N.P.[2]	0.2	Cumple	Cumple	0.2	G[3]	N,M	0.92	0.00	0.00	0.00	0.00	Cumple
Nivel 1	50x50	Arranque	N.P.[1]	N.P.[1]	N.P.[2]	0.2	N.P.[1]	Cumple	0.2	G[3]	N,M	0.92	0.00	0.00	0.00	0.00	Cumple

Notas:
[1] La comprobación no procede
[2] La comprobación no procede, ya que no hay esfuerzo cortante.
[3] 1.4·PP+1.4·CM1

2.2.2.1.12. P12

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 210 cm)	50x50	Cabeza	Cumple	Cumple	N.P.[2]	1.0	Cumple	Cumple	1.0	G[3]	N,M	-0.92	0.00	0.00	0.00	0.00	Cumple
		Pie	Cumple	Cumple	N.P.[2]	0.2	Cumple	Cumple	0.2	G[3]	N,M	0.92	0.00	0.00	0.00	0.00	Cumple
Nivel 1	50x50	Arranque	N.P.[1]	N.P.[1]	N.P.[2]	0.2	N.P.[1]	Cumple	0.2	G[3]	N,M	0.92	0.00	0.00	0.00	0.00	Cumple

Notas:
[1] La comprobación no procede
[2] La comprobación no procede, ya que no hay esfuerzo cortante.
[3] 1.4·PP+1.4·CM1

2.2.2.1.13. P27

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q (%)	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 30 cm)	50x50	Cabeza	Cumple	Cumple	0.1	N.P.[3]	Cumple	Cumple	0.1	G, S[4]	Q S.	0.00	0.00	0.00	0.00	-0.04	Cumple
		Pie	Cumple	Cumple	0.1	0.1	Cumple	Cumple	0.1	G, S[4]	Q S.,N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple
Nivel 1	50x50	Arranque	N.P.[1]	N.P.[1]	N.P.[2]	0.1	N.P.[1]	Cumple	0.1	G, S[4]	N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple

Notas:
[1] La comprobación no procede
[2] La comprobación no procede, ya que no hay esfuerzo cortante.
[3] No hay interacción entre axil y momento flector para ninguna combinación. Por lo tanto, la comprobación no procede.
[4] 1.2·PP+1.2·CM1-0.3·SX-SY

2.2.2.1.14. P28

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q (%)	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 30 cm)	50x50	Cabeza	Cumple	Cumple	0.1	N.P.[3]	Cumple	Cumple	0.1	G, S[4]	Q S.	0.00	0.00	0.00	0.00	-0.04	Cumple
		Pie	Cumple	Cumple	0.1	0.1	Cumple	Cumple	0.1	G, S[4]	Q S.,N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple
Nivel 1	50x50	Arranque	N.P.[1]	N.P.[1]	N.P.[2]	0.1	N.P.[1]	Cumple	0.1	G, S[4]	N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple

Notas:
[1] La comprobación no procede
[2] La comprobación no procede, ya que no hay esfuerzo cortante.
[3] No hay interacción entre axil y momento flector para ninguna combinación. Por lo tanto, la comprobación no procede.
[4] 1.2·PP+1.2·CM1-0.3·SX-SY



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2.2.2.1.15. P29

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q (%)	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 30 cm)	50x50	Cabeza	Cumple	Cumple	0.1	N.P.[3]	Cumple	Cumple	0.1	G, S[4]	Q S.	0.00	0.00	0.00	0.00	-0.04	Cumple
		Pie	Cumple	Cumple	0.1	0.1	Cumple	Cumple	0.1	G, S[4]	Q S.,N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple
Nivel 1	50x50	Arranque	N.P.[1]	N.P.[1]	N.P.[2]	0.1	N.P.[1]	Cumple	0.1	G, S[4]	N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple

Notas:
[1] La comprobación no procede
[2] La comprobación no procede, ya que no hay esfuerzo cortante.
[3] No hay interacción entre axil y momento flector para ninguna combinación. Por lo tanto, la comprobación no procede.
[4] 1.2·PP+1.2·CM1-0.3·SX-SY

2.2.2.1.16. P30

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q (%)	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 30 cm)	50x50	Cabeza	Cumple	Cumple	0.1	N.P.[3]	Cumple	Cumple	0.1	G, S[4]	Q S.	0.00	0.00	0.00	0.00	-0.04	Cumple
		Pie	Cumple	Cumple	0.1	0.1	Cumple	Cumple	0.1	G, S[4]	Q S.,N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple
Nivel 1	50x50	Arranque	N.P.[1]	N.P.[1]	N.P.[2]	0.1	N.P.[1]	Cumple	0.1	G, S[4]	N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple

Notas:
[1] La comprobación no procede
[2] La comprobación no procede, ya que no hay esfuerzo cortante.
[3] No hay interacción entre axil y momento flector para ninguna combinación. Por lo tanto, la comprobación no procede.
[4] 1.2·PP+1.2·CM1-0.3·SX-SY

2.2.2.1.17. P31

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q (%)	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 30 cm)	50x50	Cabeza	Cumple	Cumple	0.1	N.P.[3]	Cumple	Cumple	0.1	G, S[4]	Q S.	0.00	0.00	0.00	0.00	-0.04	Cumple
		Pie	Cumple	Cumple	0.1	0.1	Cumple	Cumple	0.1	G, S[4]	Q S.,N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple
Nivel 1	50x50	Arranque	N.P.[1]	N.P.[1]	N.P.[2]	0.1	N.P.[1]	Cumple	0.1	G, S[4]	N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple

Notas:
[1] La comprobación no procede
[2] La comprobación no procede, ya que no hay esfuerzo cortante.
[3] No hay interacción entre axil y momento flector para ninguna combinación. Por lo tanto, la comprobación no procede.
[4] 1.2·PP+1.2·CM1-0.3·SX-SY

2.2.2.1.18. P32

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q (%)	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 30 cm)	50x50	Cabeza	Cumple	Cumple	0.1	N.P.[3]	Cumple	Cumple	0.1	G, S[4]	Q S.	0.00	0.00	0.00	0.00	-0.04	Cumple
		Pie	Cumple	Cumple	0.1	0.1	Cumple	Cumple	0.1	G, S[4]	Q S.,N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple
Nivel 1	50x50	Arranque	N.P.[1]	N.P.[1]	N.P.[2]	0.1	N.P.[1]	Cumple	0.1	G, S[4]	N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple

Notas:
[1] La comprobación no procede
[2] La comprobación no procede, ya que no hay esfuerzo cortante.
[3] No hay interacción entre axil y momento flector para ninguna combinación. Por lo tanto, la comprobación no procede.
[4] 1.2·PP+1.2·CM1-0.3·SX-SY

2.2.2.1.19. P33

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q (%)	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 30 cm)	50x50	Cabeza	Cumple	Cumple	0.1	N.P.[3]	Cumple	Cumple	0.1	G, S[4]	Q S.	0.00	0.00	0.00	0.00	-0.04	Cumple



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Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q (%)	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
		Pie	Cumple	Cumple	0.1	0.1	Cumple	Cumple	0.1	G, S[4]	Q S.,N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple
Nivel 1	50x50	Arranque	N.P.[1]	N.P.[1]	N.P.[2]	0.1	N.P.[1]	Cumple	0.1	G, S[4]	N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple

Notas:
[1] La comprobación no procede
[2] La comprobación no procede, ya que no hay esfuerzo cortante.
[3] No hay interacción entre axil y momento flector para ninguna combinación. Por lo tanto, la comprobación no procede.
[4] 1.2·PP+1.2·CM1-0.3·SX-SY

2.2.2.1.20. P34

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q (%)	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 30 cm)	50x50	Cabeza	Cumple	Cumple	0.1	N.P.[3]	Cumple	Cumple	0.1	G, S[4]	Q S.	0.00	0.00	0.00	0.00	-0.04	Cumple
		Pie	Cumple	Cumple	0.1	0.1	Cumple	Cumple	0.1	G, S[4]	Q S.,N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple
Nivel 1	50x50	Arranque	N.P.[1]	N.P.[1]	N.P.[2]	0.1	N.P.[1]	Cumple	0.1	G, S[4]	N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple

Notas:
[1] La comprobación no procede
[2] La comprobación no procede, ya que no hay esfuerzo cortante.
[3] No hay interacción entre axil y momento flector para ninguna combinación. Por lo tanto, la comprobación no procede.
[4] 1.2·PP+1.2·CM1-0.3·SX-SY

2.2.2.1.21. P35

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q (%)	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 30 cm)	50x50	Cabeza	Cumple	Cumple	0.1	N.P.[3]	Cumple	Cumple	0.1	G, S[4]	Q S.	0.00	0.00	0.00	0.00	-0.04	Cumple
		Pie	Cumple	Cumple	0.1	0.1	Cumple	Cumple	0.1	G, S[4]	Q S.,N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple
Nivel 1	50x50	Arranque	N.P.[1]	N.P.[1]	N.P.[2]	0.1	N.P.[1]	Cumple	0.1	G, S[4]	N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple

Notas:
[1] La comprobación no procede
[2] La comprobación no procede, ya que no hay esfuerzo cortante.
[3] No hay interacción entre axil y momento flector para ninguna combinación. Por lo tanto, la comprobación no procede.
[4] 1.2·PP+1.2·CM1-0.3·SX-SY

2.2.2.1.22. P36

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q (%)	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 30 cm)	50x50	Cabeza	Cumple	Cumple	0.1	N.P.[3]	Cumple	Cumple	0.1	G, S[4]	Q S.	0.00	0.00	0.00	0.00	-0.04	Cumple
		Pie	Cumple	Cumple	0.1	0.1	Cumple	Cumple	0.1	G, S[4]	Q S.,N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple
Nivel 1	50x50	Arranque	N.P.[1]	N.P.[1]	N.P.[2]	0.1	N.P.[1]	Cumple	0.1	G, S[4]	N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple

Notas:
[1] La comprobación no procede
[2] La comprobación no procede, ya que no hay esfuerzo cortante.
[3] No hay interacción entre axil y momento flector para ninguna combinación. Por lo tanto, la comprobación no procede.
[4] 1.2·PP+1.2·CM1-0.3·SX-SY

2.2.2.1.23. P37

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q (%)	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 30 cm)	50x50	Cabeza	Cumple	Cumple	0.1	N.P.[3]	Cumple	No cumple[4]	No cumple	G, S[5]	Q S.	0.00	0.00	0.00	0.00	-0.04	No cumple
										G[5]	Cap. Q (S)	0.00	0.00	0.00	0.00	0.00	
		Pie	Cumple	Cumple	0.1	0.1	Cumple	No cumple[4]	No cumple	G, S[5]	Q S.,N,M S.	0.23	-0.01	0.00	0.00	-0.04	No cumple
										G[5]	Cap. Q (S)	0.26	0.00	0.00	0.00	0.00	
Nivel 1	50x50	Arranque	N.P.[1]	N.P.[1]	N.P.[2]	0.1	N.P.[1]	Cumple	0.1	G, S[5]	N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q (%)	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	

Notas:
(1) La comprobación no procede
(2) La comprobación no procede, ya que no hay esfuerzo cortante.
(3) No hay interacción entre axil y momento flector para ninguna combinación. Por lo tanto, la comprobación no procede.
(4) No cumple: 'Cortante de diseño para columnas.'
(5) 1.2·PP+1.2·CM1-0.3·SX-SY
(6) 1.4·PP+1.4·CM1

2.2.2.1.24. P38

Sección de hormigón																	
Tramo	Dimensión (cm)	Posición	Comprobaciones							Esfuerzos pésimos							Estado
			Disp.	Arm.	Q (%)	N,M (%)	Disp. S.	Cap.	Aprov. (%)	Naturaleza	Comp.	N (t)	Mxx (t·m)	Myy (t·m)	Qx (t)	Qy (t)	
Nivel 2 (0 - 30 cm)	50x50	Cabeza	Cumple	Cumple	0.1	N.P.(3)	Cumple	Cumple	0.1	G, S(4)	Q S.	0.00	0.00	0.00	0.00	-0.04	Cumple
		Pie	Cumple	Cumple	0.1	0.1	Cumple	Cumple	0.1	G, S(4)	Q S.,N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple
Nivel 1	50x50	Arranque	N.P.(1)	N.P.(1)	N.P.(2)	0.1	N.P.(1)	Cumple	0.1	G, S(4)	N,M S.	0.23	-0.01	0.00	0.00	-0.04	Cumple

Notas:
(1) La comprobación no procede
(2) La comprobación no procede, ya que no hay esfuerzo cortante.
(3) No hay interacción entre axil y momento flector para ninguna combinación. Por lo tanto, la comprobación no procede.
(4) 1.2·PP+1.2·CM1-0.3·SX-SY

3. CIMENTACIÓN

3.1. Elementos de cimentación aislados

3.1.1. Descripción

Referencias	Geometría	Armado
P1, P2, P3, P4, P5 y P6	Zapata rectangular excéntrica Ancho inicial X: 50 cm Ancho inicial Y: 25 cm Ancho final X: 50 cm Ancho final Y: 50 cm Ancho zapata X: 100 cm Ancho zapata Y: 75 cm Canto: 35 cm	X: 3Ø5/8"c/27 Y: 4Ø5/8"c/26
P7, P8, P9, P10, P11 y P12	Zapata rectangular excéntrica Ancho inicial X: 50 cm Ancho inicial Y: 50 cm Ancho final X: 50 cm Ancho final Y: 25 cm Ancho zapata X: 100 cm Ancho zapata Y: 75 cm Canto: 35 cm	X: 3Ø5/8"c/27 Y: 4Ø5/8"c/26
P33, P34, P36, P37, P38, P32, P31, P30, P27, P28, P29 y P35	Zapata de hormigón en masa cuadrada Anchura: 110 cm Canto: 30 cm	

3.1.2. Comprobación

Referencia: P1
Dimensiones: 100 x 75 x 35
Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26

Comprobación	Valores	Estado
Tensiones sobre el terreno: *Criterio de CYPE*		
- Tensión media en situaciones persistentes:	Máximo: 1 kp/cm² Calculado: 0.175 kp/cm²	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: P1 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
- Tensión media en situaciones accidentales sísmicas:	Máximo: 1.3 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes sin viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes con viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones accidentales sísmicas:	Máximo: 1.625 kp/cm² Calculado: 0.262 kp/cm²	Cumple
Vuelco de la zapata:		
- En dirección X:		No procede(1)
- En dirección Y:		
Si el % de reserva de seguridad es mayor que cero, quiere decir que los coeficientes de seguridad al vuelco son mayores que los valores estrictos exigidos para todas las combinaciones de equilibrio. *(1) Sin momento de vuelco*	Reserva seguridad: 500.0 %	Cumple
Flexión en la zapata:		
- En dirección X:	Momento: 0.00 t·m	Cumple
- En dirección Y:	Momento: 0.00 t·m	Cumple
Cortante en la zapata:		
- En dirección X:	Cortante: 0.00 t	Cumple
- En dirección Y:	Cortante: 0.00 t	Cumple
Compresión oblicua en la zapata:		
Criterio de CYPE	Máximo: 735 t/m²	
- Situaciones persistentes:	Calculado: 2.77 t/m²	Cumple
- Situaciones accidentales sísmicas:	Calculado: 2.37 t/m²	Cumple
Canto mínimo:	Mínimo: 23.5 cm	
Capítulo C.15.7 (norma NSR-10)	Calculado: 35 cm	Cumple
Espacio para anclar arranques en cimentación:		
- P1:	Mínimo: 20 cm Calculado: 25 cm	Cumple
Cuantía geométrica mínima:		
Capítulo C.7.12.2.1 (norma NSR-10)	Mínimo: 0.0018	
- Armado inferior dirección X:	Calculado: 0.0023	Cumple
- Armado inferior dirección Y:	Calculado: 0.0023	Cumple
Diámetro mínimo de las barras:		
- Parrilla inferior:		
Criterio de CYPE	Mínimo: 10 mm Calculado: 15.875 mm	Cumple
Separación máxima entre barras:		
Criterio de CYPE	Máximo: 30 cm	
- Armado inferior dirección X:	Calculado: 27 cm	Cumple
- Armado inferior dirección Y:	Calculado: 26 cm	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: P1 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
Separación mínima entre barras: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.16*	Mínimo: 10 cm	
- Armado inferior dirección X:	Calculado: 27 cm	Cumple
- Armado inferior dirección Y:	Calculado: 26 cm	Cumple
Longitud de anclaje: *Criterio del libro "Cálculo de estructuras de cimentación", J. Calavera. Ed. INTEMAC, 1991*		
- Armado inf. dirección X hacia der:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección X hacia izq:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia arriba:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia abajo:	Mínimo: 0 cm Calculado: 0 cm	Cumple
Longitud mínima de las patillas:	Mínimo: 25 cm	
- Armado inf. dirección X hacia der:	Calculado: 41 cm	Cumple
- Armado inf. dirección X hacia izq:	Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia arriba:	Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia abajo:	Calculado: 41 cm	Cumple
Tensión máxima en la armadura para limitar la fisuración:	Máximo: 2520 kp/cm²	
- Armado inferior dirección X:	Calculado: 0 kp/cm²	Cumple
- Armado inferior dirección Y:	Calculado: 0 kp/cm²	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Relación rotura pésima (En dirección X): 0.00 - Relación rotura pésima (En dirección Y): 0.00 - Cortante de agotamiento (En dirección X): 0.00 t - Cortante de agotamiento (En dirección Y): 0.00 t		
Referencia: P2 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
Tensiones sobre el terreno: *Criterio de CYPE*		
- Tensión media en situaciones persistentes:	Máximo: 1 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión media en situaciones accidentales sísmicas:	Máximo: 1.3 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes sin viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes con viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple

Listados

Referencia: P2 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
- Tensión máxima en situaciones accidentales sísmicas:	Máximo: 1.625 kp/cm² Calculado: 0.262 kp/cm²	Cumple
Vuelco de la zapata: - En dirección X: - En dirección Y: *Si el % de reserva de seguridad es mayor que cero, quiere decir que los coeficientes de seguridad al vuelco son mayores que los valores estrictos exigidos para todas las combinaciones de equilibrio.* *(1) Sin momento de vuelco*	Reserva seguridad: 500.0 %	No procede(1) Cumple
Flexión en la zapata: - En dirección X: - En dirección Y:	Momento: 0.00 t·m Momento: 0.00 t·m	Cumple Cumple
Cortante en la zapata: - En dirección X: - En dirección Y:	Cortante: 0.00 t Cortante: 0.00 t	Cumple Cumple
Compresión oblicua en la zapata: *Criterio de CYPE* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Máximo: 735 t/m² Calculado: 2.77 t/m² Calculado: 2.37 t/m²	 Cumple Cumple
Canto mínimo: *Capítulo C.15.7 (norma NSR-10)*	Mínimo: 23.5 cm Calculado: 35 cm	Cumple
Espacio para anclar arranques en cimentación: - P2:	Mínimo: 20 cm Calculado: 25 cm	Cumple
Cuantía geométrica mínima: *Capítulo C.7.12.2.1 (norma NSR-10)* - Armado inferior dirección X: - Armado inferior dirección Y:	Mínimo: 0.0018 Calculado: 0.0023 Calculado: 0.0023	 Cumple Cumple
Diámetro mínimo de las barras: - Parrilla inferior: *Criterio de CYPE*	Mínimo: 10 mm Calculado: 15.875 mm	Cumple
Separación máxima entre barras: *Criterio de CYPE* - Armado inferior dirección X: - Armado inferior dirección Y:	Máximo: 30 cm Calculado: 27 cm Calculado: 26 cm	 Cumple Cumple
Separación mínima entre barras: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.16* - Armado inferior dirección X: - Armado inferior dirección Y:	Mínimo: 10 cm Calculado: 27 cm Calculado: 26 cm	 Cumple Cumple
Longitud de anclaje: *Criterio del libro "Cálculo de estructuras de cimentación", J. Calavera. Ed. INTEMAC, 1991*		

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: P2
Dimensiones: 100 x 75 x 35
Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26

Comprobación	Valores	Estado
- Armado inf. dirección X hacia der:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección X hacia izq:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia arriba:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia abajo:	Mínimo: 0 cm Calculado: 0 cm	Cumple
Longitud mínima de las patillas:	Mínimo: 25 cm	
- Armado inf. dirección X hacia der:	Calculado: 41 cm	Cumple
- Armado inf. dirección X hacia izq:	Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia arriba:	Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia abajo:	Calculado: 41 cm	Cumple
Tensión máxima en la armadura para limitar la fisuración:	Máximo: 2520 kp/cm²	
- Armado inferior dirección X:	Calculado: 0 kp/cm²	Cumple
- Armado inferior dirección Y:	Calculado: 0 kp/cm²	Cumple
Se cumplen todas las comprobaciones		

Información adicional:
- Relación rotura pésima (En dirección X): 0.00
- Relación rotura pésima (En dirección Y): 0.00
- Cortante de agotamiento (En dirección X): 0.00 t
- Cortante de agotamiento (En dirección Y): 0.00 t

Referencia: P3
Dimensiones: 100 x 75 x 35
Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26

Comprobación	Valores	Estado
Tensiones sobre el terreno: *Criterio de CYPE*		
- Tensión media en situaciones persistentes:	Máximo: 1 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión media en situaciones accidentales sísmicas:	Máximo: 1.3 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes sin viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes con viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones accidentales sísmicas:	Máximo: 1.625 kp/cm² Calculado: 0.262 kp/cm²	Cumple
Vuelco de la zapata:		
- En dirección X:		No procede[1]
- En dirección Y:		
Si el % de reserva de seguridad es mayor que cero, quiere decir que los coeficientes de seguridad al vuelco son mayores que los valores estrictos exigidos para todas las combinaciones de equilibrio.	Reserva seguridad: 500.0 %	Cumple
[1] Sin momento de vuelco		

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: P3 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
Flexión en la zapata:		
- En dirección X:	Momento: 0.00 t·m	Cumple
- En dirección Y:	Momento: 0.00 t·m	Cumple
Cortante en la zapata:		
- En dirección X:	Cortante: 0.00 t	Cumple
- En dirección Y:	Cortante: 0.00 t	Cumple
Compresión oblicua en la zapata: *Criterio de CYPE*	Máximo: 735 t/m²	
- Situaciones persistentes:	Calculado: 2.77 t/m²	Cumple
- Situaciones accidentales sísmicas:	Calculado: 2.37 t/m²	Cumple
Canto mínimo: *Capítulo C.15.7 (norma NSR-10)*	Mínimo: 23.5 cm Calculado: 35 cm	Cumple
Espacio para anclar arranques en cimentación: - P3:	Mínimo: 20 cm Calculado: 25 cm	Cumple
Cuantía geométrica mínima: *Capítulo C.7.12.2.1 (norma NSR-10)*	Mínimo: 0.0018	
- Armado inferior dirección X:	Calculado: 0.0023	Cumple
- Armado inferior dirección Y:	Calculado: 0.0023	Cumple
Diámetro mínimo de las barras: - Parrilla inferior: *Criterio de CYPE*	Mínimo: 10 mm Calculado: 15.875 mm	Cumple
Separación máxima entre barras: *Criterio de CYPE*	Máximo: 30 cm	
- Armado inferior dirección X:	Calculado: 27 cm	Cumple
- Armado inferior dirección Y:	Calculado: 26 cm	Cumple
Separación mínima entre barras: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.16*	Mínimo: 10 cm	
- Armado inferior dirección X:	Calculado: 27 cm	Cumple
- Armado inferior dirección Y:	Calculado: 26 cm	Cumple
Longitud de anclaje: *Criterio del libro "Cálculo de estructuras de cimentación", J. Calavera. Ed. INTEMAC, 1991*		
- Armado inf. dirección X hacia der:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección X hacia izq:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia arriba:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia abajo:	Mínimo: 0 cm Calculado: 0 cm	Cumple
Longitud mínima de las patillas:	Mínimo: 25 cm	

Listados

Referencia: P3 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
- Armado inf. dirección X hacia der:	Calculado: 41 cm	Cumple
- Armado inf. dirección X hacia izq:	Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia arriba:	Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia abajo:	Calculado: 41 cm	Cumple
Tensión máxima en la armadura para limitar la fisuración:	Máximo: 2520 kp/cm²	
- Armado inferior dirección X:	Calculado: 0 kp/cm²	Cumple
- Armado inferior dirección Y:	Calculado: 0 kp/cm²	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Relación rotura pésima (En dirección X): 0.00 - Relación rotura pésima (En dirección Y): 0.00 - Cortante de agotamiento (En dirección X): 0.00 t - Cortante de agotamiento (En dirección Y): 0.00 t		

Referencia: P4 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
Tensiones sobre el terreno: *Criterio de CYPE*		
- Tensión media en situaciones persistentes:	Máximo: 1 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión media en situaciones accidentales sísmicas:	Máximo: 1.3 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes sin viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes con viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones accidentales sísmicas:	Máximo: 1.625 kp/cm² Calculado: 0.262 kp/cm²	Cumple
Vuelco de la zapata: - En dirección X: - En dirección Y: *Si el % de reserva de seguridad es mayor que cero, quiere decir que los coeficientes de seguridad al vuelco son mayores que los valores estrictos exigidos para todas las combinaciones de equilibrio.* *(1) Sin momento de vuelco*	Reserva seguridad: 500.0 %	No procede(1) Cumple
Flexión en la zapata: - En dirección X: - En dirección Y:	Momento: 0.00 t·m Momento: 0.00 t·m	Cumple Cumple
Cortante en la zapata: - En dirección X: - En dirección Y:	Cortante: 0.00 t Cortante: 0.00 t	Cumple Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: P4 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
Compresión oblicua en la zapata: *Criterio de CYPE*	Máximo: 735 t/m²	
- Situaciones persistentes:	Calculado: 2.77 t/m²	Cumple
- Situaciones accidentales sísmicas:	Calculado: 2.37 t/m²	Cumple
Canto mínimo: *Capítulo C.15.7 (norma NSR-10)*	Mínimo: 23.5 cm Calculado: 35 cm	Cumple
Espacio para anclar arranques en cimentación: - P4:	Mínimo: 20 cm Calculado: 25 cm	Cumple
Cuantía geométrica mínima: *Capítulo C.7.12.2.1 (norma NSR-10)*	Mínimo: 0.0018	
- Armado inferior dirección X:	Calculado: 0.0023	Cumple
- Armado inferior dirección Y:	Calculado: 0.0023	Cumple
Diámetro mínimo de las barras: - Parrilla inferior: *Criterio de CYPE*	Mínimo: 10 mm Calculado: 15.875 mm	Cumple
Separación máxima entre barras: *Criterio de CYPE*	Máximo: 30 cm	
- Armado inferior dirección X:	Calculado: 27 cm	Cumple
- Armado inferior dirección Y:	Calculado: 26 cm	Cumple
Separación mínima entre barras: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.16*	Mínimo: 10 cm	
- Armado inferior dirección X:	Calculado: 27 cm	Cumple
- Armado inferior dirección Y:	Calculado: 26 cm	Cumple
Longitud de anclaje: *Criterio del libro "Cálculo de estructuras de cimentación", J. Calavera. Ed. INTEMAC, 1991*		
- Armado inf. dirección X hacia der:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección X hacia izq:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia arriba:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia abajo:	Mínimo: 0 cm Calculado: 0 cm	Cumple
Longitud mínima de las patillas:	Mínimo: 25 cm	
- Armado inf. dirección X hacia der:	Calculado: 41 cm	Cumple
- Armado inf. dirección X hacia izq:	Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia arriba:	Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia abajo:	Calculado: 41 cm	Cumple
Tensión máxima en la armadura para limitar la fisuración:	Máximo: 2520 kp/cm²	
- Armado inferior dirección X:	Calculado: 0 kp/cm²	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: P4 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
- Armado inferior dirección Y:	Calculado: 0 kp/cm²	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Relación rotura pésima (En dirección X): 0.00 - Relación rotura pésima (En dirección Y): 0.00 - Cortante de agotamiento (En dirección X): 0.00 t - Cortante de agotamiento (En dirección Y): 0.00 t		
Referencia: P5 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
Tensiones sobre el terreno: *Criterio de CYPE*		
- Tensión media en situaciones persistentes:	Máximo: 1 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión media en situaciones accidentales sísmicas:	Máximo: 1.3 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes sin viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes con viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones accidentales sísmicas:	Máximo: 1.625 kp/cm² Calculado: 0.262 kp/cm²	Cumple
Vuelco de la zapata: - En dirección X: - En dirección Y: *Si el % de reserva de seguridad es mayor que cero, quiere decir que los coeficientes de seguridad al vuelco son mayores que los valores estrictos exigidos para todas las combinaciones de equilibrio.* *(1) Sin momento de vuelco*	Reserva seguridad: 500.0 %	No procede(1) Cumple
Flexión en la zapata: - En dirección X: - En dirección Y:	Momento: 0.00 t·m Momento: 0.00 t·m	Cumple Cumple
Cortante en la zapata: - En dirección X: - En dirección Y:	Cortante: 0.00 t Cortante: 0.00 t	Cumple Cumple
Compresión oblicua en la zapata: *Criterio de CYPE* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Máximo: 735 t/m² Calculado: 2.77 t/m² Calculado: 2.37 t/m²	 Cumple Cumple
Canto mínimo: *Capítulo C.15.7 (norma NSR-10)*	Mínimo: 23.5 cm Calculado: 35 cm	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: P5 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
Espacio para anclar arranques en cimentación: - P5:	Mínimo: 20 cm Calculado: 25 cm	Cumple
Cuantía geométrica mínima: *Capítulo C.7.12.2.1 (norma NSR-10)* - Armado inferior dirección X: - Armado inferior dirección Y:	Mínimo: 0.0018 Calculado: 0.0023 Calculado: 0.0023	Cumple Cumple
Diámetro mínimo de las barras: - Parrilla inferior: *Criterio de CYPE*	Mínimo: 10 mm Calculado: 15.875 mm	Cumple
Separación máxima entre barras: *Criterio de CYPE* - Armado inferior dirección X: - Armado inferior dirección Y:	Máximo: 30 cm Calculado: 27 cm Calculado: 26 cm	Cumple Cumple
Separación mínima entre barras: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.16* - Armado inferior dirección X: - Armado inferior dirección Y:	Mínimo: 10 cm Calculado: 27 cm Calculado: 26 cm	Cumple Cumple
Longitud de anclaje: *Criterio del libro "Cálculo de estructuras de cimentación", J. Calavera. Ed. INTEMAC, 1991* - Armado inf. dirección X hacia der: - Armado inf. dirección X hacia izq: - Armado inf. dirección Y hacia arriba: - Armado inf. dirección Y hacia abajo:	Mínimo: 30 cm Calculado: 41 cm Mínimo: 30 cm Calculado: 41 cm Mínimo: 30 cm Calculado: 41 cm Mínimo: 0 cm Calculado: 0 cm	Cumple Cumple Cumple Cumple
Longitud mínima de las patillas: - Armado inf. dirección X hacia der: - Armado inf. dirección X hacia izq: - Armado inf. dirección Y hacia arriba: - Armado inf. dirección Y hacia abajo:	Mínimo: 25 cm Calculado: 41 cm Calculado: 41 cm Calculado: 41 cm Calculado: 41 cm	Cumple Cumple Cumple Cumple
Tensión máxima en la armadura para limitar la fisuración: - Armado inferior dirección X: - Armado inferior dirección Y:	Máximo: 2520 kp/cm² Calculado: 0 kp/cm² Calculado: 0 kp/cm²	Cumple Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Relación rotura pésima (En dirección X): 0.00 - Relación rotura pésima (En dirección Y): 0.00 - Cortante de agotamiento (En dirección X): 0.00 t - Cortante de agotamiento (En dirección Y): 0.00 t		

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: P6
Dimensiones: 100 x 75 x 35
Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26

Comprobación	Valores	Estado
Tensiones sobre el terreno: *Criterio de CYPE*		
- Tensión media en situaciones persistentes:	Máximo: 1 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión media en situaciones accidentales sísmicas:	Máximo: 1.3 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes sin viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes con viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones accidentales sísmicas:	Máximo: 1.625 kp/cm² Calculado: 0.262 kp/cm²	Cumple
Vuelco de la zapata:		
- En dirección X:		No procede[1]
- En dirección Y: *Si el % de reserva de seguridad es mayor que cero, quiere decir que los coeficientes de seguridad al vuelco son mayores que los valores estrictos exigidos para todas las combinaciones de equilibrio.* *(1) Sin momento de vuelco*	Reserva seguridad: 500.0 %	Cumple
Flexión en la zapata:		
- En dirección X:	Momento: 0.00 t·m	Cumple
- En dirección Y:	Momento: 0.00 t·m	Cumple
Cortante en la zapata:		
- En dirección X:	Cortante: 0.00 t	Cumple
- En dirección Y:	Cortante: 0.00 t	Cumple
Compresión oblicua en la zapata: *Criterio de CYPE*	Máximo: 735 t/m²	
- Situaciones persistentes:	Calculado: 2.77 t/m²	Cumple
- Situaciones accidentales sísmicas:	Calculado: 2.37 t/m²	Cumple
Canto mínimo: *Capítulo C.15.7 (norma NSR-10)*	Mínimo: 23.5 cm Calculado: 35 cm	Cumple
Espacio para anclar arranques en cimentación: - P6:	Mínimo: 20 cm Calculado: 25 cm	Cumple
Cuantía geométrica mínima: *Capítulo C.7.12.2.1 (norma NSR-10)*	Mínimo: 0.0018	
- Armado inferior dirección X:	Calculado: 0.0023	Cumple
- Armado inferior dirección Y:	Calculado: 0.0023	Cumple
Diámetro mínimo de las barras: - Parrilla inferior: *Criterio de CYPE*	Mínimo: 10 mm Calculado: 15.875 mm	Cumple
Separación máxima entre barras: *Criterio de CYPE*	Máximo: 30 cm	

Listados

Referencia: P6 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
- Armado inferior dirección X:	Calculado: 27 cm	Cumple
- Armado inferior dirección Y:	Calculado: 26 cm	Cumple
Separación mínima entre barras: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.16*	Mínimo: 10 cm	
- Armado inferior dirección X:	Calculado: 27 cm	Cumple
- Armado inferior dirección Y:	Calculado: 26 cm	Cumple
Longitud de anclaje: *Criterio del libro "Cálculo de estructuras de cimentación", J. Calavera. Ed. INTEMAC, 1991*		
- Armado inf. dirección X hacia der:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección X hacia izq:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia arriba:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia abajo:	Mínimo: 0 cm Calculado: 0 cm	Cumple
Longitud mínima de las patillas:	Mínimo: 25 cm	
- Armado inf. dirección X hacia der:	Calculado: 41 cm	Cumple
- Armado inf. dirección X hacia izq:	Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia arriba:	Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia abajo:	Calculado: 41 cm	Cumple
Tensión máxima en la armadura para limitar la fisuración:	Máximo: 2520 kp/cm²	
- Armado inferior dirección X:	Calculado: 0 kp/cm²	Cumple
- Armado inferior dirección Y:	Calculado: 0 kp/cm²	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Relación rotura pésima (En dirección X): 0.00 - Relación rotura pésima (En dirección Y): 0.00 - Cortante de agotamiento (En dirección X): 0.00 t - Cortante de agotamiento (En dirección Y): 0.00 t		

Referencia: P7 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
Tensiones sobre el terreno: *Criterio de CYPE*		
- Tensión media en situaciones persistentes:	Máximo: 1 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión media en situaciones accidentales sísmicas:	Máximo: 1.3 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes sin viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: P7 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
- Tensión máxima en situaciones persistentes con viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones accidentales sísmicas:	Máximo: 1.625 kp/cm² Calculado: 0.262 kp/cm²	Cumple
Vuelco de la zapata:		
- En dirección X:		No procede[1]
- En dirección Y:		
Si el % de reserva de seguridad es mayor que cero, quiere decir que los coeficientes de seguridad al vuelco son mayores que los valores estrictos exigidos para todas las combinaciones de equilibrio. *(1) Sin momento de vuelco*	Reserva seguridad: 500.0 %	Cumple
Flexión en la zapata:		
- En dirección X:	Momento: 0.00 t·m	Cumple
- En dirección Y:	Momento: 0.00 t·m	Cumple
Cortante en la zapata:		
- En dirección X:	Cortante: 0.00 t	Cumple
- En dirección Y:	Cortante: 0.00 t	Cumple
Compresión oblicua en la zapata: *Criterio de CYPE*	Máximo: 735 t/m²	
- Situaciones persistentes:	Calculado: 2.77 t/m²	Cumple
- Situaciones accidentales sísmicas:	Calculado: 2.37 t/m²	Cumple
Canto mínimo: *Capítulo C.15.7 (norma NSR-10)*	Mínimo: 23.5 cm Calculado: 35 cm	Cumple
Espacio para anclar arranques en cimentación: - P7:	Mínimo: 20 cm Calculado: 25 cm	Cumple
Cuantía geométrica mínima: *Capítulo C.7.12.2.1 (norma NSR-10)*	Mínimo: 0.0018	
- Armado inferior dirección X:	Calculado: 0.0023	Cumple
- Armado inferior dirección Y:	Calculado: 0.0023	Cumple
Diámetro mínimo de las barras: - Parrilla inferior: *Criterio de CYPE*	Mínimo: 10 mm Calculado: 15.875 mm	Cumple
Separación máxima entre barras: *Criterio de CYPE*	Máximo: 30 cm	
- Armado inferior dirección X:	Calculado: 27 cm	Cumple
- Armado inferior dirección Y:	Calculado: 26 cm	Cumple
Separación mínima entre barras: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.16*	Mínimo: 10 cm	
- Armado inferior dirección X:	Calculado: 27 cm	Cumple
- Armado inferior dirección Y:	Calculado: 26 cm	Cumple



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: P7 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
Longitud de anclaje: *Criterio del libro "Cálculo de estructuras de cimentación", J. Calavera. Ed. INTEMAC, 1991*		
- Armado inf. dirección X hacia der:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección X hacia izq:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia arriba:	Mínimo: 0 cm Calculado: 0 cm	Cumple
- Armado inf. dirección Y hacia abajo:	Mínimo: 30 cm Calculado: 41 cm	Cumple
Longitud mínima de las patillas:	Mínimo: 25 cm	
- Armado inf. dirección X hacia der:	Calculado: 41 cm	Cumple
- Armado inf. dirección X hacia izq:	Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia arriba:	Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia abajo:	Calculado: 41 cm	Cumple
Tensión máxima en la armadura para limitar la fisuración:	Máximo: 2520 kp/cm²	
- Armado inferior dirección X:	Calculado: 0 kp/cm²	Cumple
- Armado inferior dirección Y:	Calculado: 0 kp/cm²	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Relación rotura pésima (En dirección X): 0.00 - Relación rotura pésima (En dirección Y): 0.00 - Cortante de agotamiento (En dirección X): 0.00 t - Cortante de agotamiento (En dirección Y): 0.00 t		
Referencia: P8 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
Tensiones sobre el terreno: *Criterio de CYPE*		
- Tensión media en situaciones persistentes:	Máximo: 1 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión media en situaciones accidentales sísmicas:	Máximo: 1.3 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes sin viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes con viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones accidentales sísmicas:	Máximo: 1.625 kp/cm² Calculado: 0.262 kp/cm²	Cumple
Vuelco de la zapata:		
- En dirección X:		No procede[1]

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: P8 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
- En dirección Y: *Si el % de reserva de seguridad es mayor que cero, quiere decir que los coeficientes de seguridad al vuelco son mayores que los valores estrictos exigidos para todas las combinaciones de equilibrio.* *(1) Sin momento de vuelco*	Reserva seguridad: 500.0 %	Cumple
Flexión en la zapata:		
- En dirección X:	Momento: 0.00 t·m	Cumple
- En dirección Y:	Momento: 0.00 t·m	Cumple
Cortante en la zapata:		
- En dirección X:	Cortante: 0.00 t	Cumple
- En dirección Y:	Cortante: 0.00 t	Cumple
Compresión oblicua en la zapata: *Criterio de CYPE*	Máximo: 735 t/m²	
- Situaciones persistentes:	Calculado: 2.77 t/m²	Cumple
- Situaciones accidentales sísmicas:	Calculado: 2.37 t/m²	Cumple
Canto mínimo: *Capítulo C.15.7 (norma NSR-10)*	Mínimo: 23.5 cm Calculado: 35 cm	Cumple
Espacio para anclar arranques en cimentación: - P8:	Mínimo: 20 cm Calculado: 25 cm	Cumple
Cuantía geométrica mínima: *Capítulo C.7.12.2.1 (norma NSR-10)*	Mínimo: 0.0018	
- Armado inferior dirección X:	Calculado: 0.0023	Cumple
- Armado inferior dirección Y:	Calculado: 0.0023	Cumple
Diámetro mínimo de las barras: - Parrilla inferior: *Criterio de CYPE*	Mínimo: 10 mm Calculado: 15.875 mm	Cumple
Separación máxima entre barras: *Criterio de CYPE*	Máximo: 30 cm	
- Armado inferior dirección X:	Calculado: 27 cm	Cumple
- Armado inferior dirección Y:	Calculado: 26 cm	Cumple
Separación mínima entre barras: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.16*	Mínimo: 10 cm	
- Armado inferior dirección X:	Calculado: 27 cm	Cumple
- Armado inferior dirección Y:	Calculado: 26 cm	Cumple
Longitud de anclaje: *Criterio del libro "Cálculo de estructuras de cimentación", J. Calavera. Ed. INTEMAC, 1991*		
- Armado inf. dirección X hacia der:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección X hacia izq:	Mínimo: 30 cm Calculado: 41 cm	Cumple

Listados

Referencia: P8
Dimensiones: 100 x 75 x 35
Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26

Comprobación	Valores	Estado
- Armado inf. dirección Y hacia arriba:	Mínimo: 0 cm Calculado: 0 cm	Cumple
- Armado inf. dirección Y hacia abajo:	Mínimo: 30 cm Calculado: 41 cm	Cumple
Longitud mínima de las patillas:	Mínimo: 25 cm	
- Armado inf. dirección X hacia der:	Calculado: 41 cm	Cumple
- Armado inf. dirección X hacia izq:	Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia arriba:	Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia abajo:	Calculado: 41 cm	Cumple
Tensión máxima en la armadura para limitar la fisuración:	Máximo: 2520 kp/cm²	
- Armado inferior dirección X:	Calculado: 0 kp/cm²	Cumple
- Armado inferior dirección Y:	Calculado: 0 kp/cm²	Cumple
Se cumplen todas las comprobaciones		

Información adicional:
- Relación rotura pésima (En dirección X): 0.00
- Relación rotura pésima (En dirección Y): 0.00
- Cortante de agotamiento (En dirección X): 0.00 t
- Cortante de agotamiento (En dirección Y): 0.00 t

Referencia: P9
Dimensiones: 100 x 75 x 35
Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26

Comprobación	Valores	Estado
Tensiones sobre el terreno: *Criterio de CYPE*		
- Tensión media en situaciones persistentes:	Máximo: 1 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión media en situaciones accidentales sísmicas:	Máximo: 1.3 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes sin viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes con viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones accidentales sísmicas:	Máximo: 1.625 kp/cm² Calculado: 0.262 kp/cm²	Cumple
Vuelco de la zapata:		
- En dirección X:		No procede(1)
- En dirección Y:		
Si el % de reserva de seguridad es mayor que cero, quiere decir que los coeficientes de seguridad al vuelco son mayores que los valores estrictos exigidos para todas las combinaciones de equilibrio. *(1) Sin momento de vuelco*	Reserva seguridad: 500.0 %	Cumple
Flexión en la zapata:		
- En dirección X:	Momento: 0.00 t·m	Cumple
- En dirección Y:	Momento: 0.00 t·m	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: P9 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
Cortante en la zapata:		
- En dirección X:	Cortante: 0.00 t	Cumple
- En dirección Y:	Cortante: 0.00 t	Cumple
Compresión oblicua en la zapata:		
Criterio de CYPE	Máximo: 735 t/m²	
- Situaciones persistentes:	Calculado: 2.77 t/m²	Cumple
- Situaciones accidentales sísmicas:	Calculado: 2.37 t/m²	Cumple
Canto mínimo:	Mínimo: 23.5 cm	
Capítulo C.15.7 (norma NSR-10)	Calculado: 35 cm	Cumple
Espacio para anclar arranques en cimentación:		
- P9:	Mínimo: 20 cm Calculado: 25 cm	Cumple
Cuantía geométrica mínima:		
Capítulo C.7.12.2.1 (norma NSR-10)	Mínimo: 0.0018	
- Armado inferior dirección X:	Calculado: 0.0023	Cumple
- Armado inferior dirección Y:	Calculado: 0.0023	Cumple
Diámetro mínimo de las barras:		
- Parrilla inferior:		
Criterio de CYPE	Mínimo: 10 mm Calculado: 15.875 mm	Cumple
Separación máxima entre barras:		
Criterio de CYPE	Máximo: 30 cm	
- Armado inferior dirección X:	Calculado: 27 cm	Cumple
- Armado inferior dirección Y:	Calculado: 26 cm	Cumple
Separación mínima entre barras:		
Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.16	Mínimo: 10 cm	
- Armado inferior dirección X:	Calculado: 27 cm	Cumple
- Armado inferior dirección Y:	Calculado: 26 cm	Cumple
Longitud de anclaje:		
Criterio del libro "Cálculo de estructuras de cimentación", J. Calavera. Ed. INTEMAC, 1991		
- Armado inf. dirección X hacia der:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección X hacia izq:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia arriba:	Mínimo: 0 cm Calculado: 0 cm	Cumple
- Armado inf. dirección Y hacia abajo:	Mínimo: 30 cm Calculado: 41 cm	Cumple
Longitud mínima de las patillas:	Mínimo: 25 cm	
- Armado inf. dirección X hacia der:	Calculado: 41 cm	Cumple
- Armado inf. dirección X hacia izq:	Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia arriba:	Calculado: 41 cm	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: P9 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
- Armado inf. dirección Y hacia abajo:	Calculado: 41 cm	Cumple
Tensión máxima en la armadura para limitar la fisuración:	Máximo: 2520 kp/cm²	
- Armado inferior dirección X:	Calculado: 0 kp/cm²	Cumple
- Armado inferior dirección Y:	Calculado: 0 kp/cm²	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Relación rotura pésima (En dirección X): 0.00 - Relación rotura pésima (En dirección Y): 0.00 - Cortante de agotamiento (En dirección X): 0.00 t - Cortante de agotamiento (En dirección Y): 0.00 t		

Referencia: P10 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
Tensiones sobre el terreno: *Criterio de CYPE*		
- Tensión media en situaciones persistentes:	Máximo: 1 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión media en situaciones accidentales sísmicas:	Máximo: 1.3 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes sin viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes con viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones accidentales sísmicas:	Máximo: 1.625 kp/cm² Calculado: 0.262 kp/cm²	Cumple
Vuelco de la zapata:		
- En dirección X:		No procede[1]
- En dirección Y:		
Si el % de reserva de seguridad es mayor que cero, quiere decir que los coeficientes de seguridad al vuelco son mayores que los valores estrictos exigidos para todas las combinaciones de equilibrio. *[1] Sin momento de vuelco*	Reserva seguridad: 500.0 %	Cumple
Flexión en la zapata:		
- En dirección X:	Momento: 0.00 t·m	Cumple
- En dirección Y:	Momento: 0.00 t·m	Cumple
Cortante en la zapata:		
- En dirección X:	Cortante: 0.00 t	Cumple
- En dirección Y:	Cortante: 0.00 t	Cumple
Compresión oblicua en la zapata: *Criterio de CYPE*	Máximo: 735 t/m²	
- Situaciones persistentes:	Calculado: 2.77 t/m²	Cumple
- Situaciones accidentales sísmicas:	Calculado: 2.37 t/m²	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: P10 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
Canto mínimo: *Capítulo C.15.7 (norma NSR-10)*	Mínimo: 23.5 cm Calculado: 35 cm	Cumple
Espacio para anclar arranques en cimentación: - P10:	Mínimo: 20 cm Calculado: 25 cm	Cumple
Cuantía geométrica mínima: *Capítulo C.7.12.2.1 (norma NSR-10)* - Armado inferior dirección X: - Armado inferior dirección Y:	Mínimo: 0.0018 Calculado: 0.0023 Calculado: 0.0023	Cumple Cumple
Diámetro mínimo de las barras: - Parrilla inferior: *Criterio de CYPE*	Mínimo: 10 mm Calculado: 15.875 mm	Cumple
Separación máxima entre barras: *Criterio de CYPE* - Armado inferior dirección X: - Armado inferior dirección Y:	Máximo: 30 cm Calculado: 27 cm Calculado: 26 cm	Cumple Cumple
Separación mínima entre barras: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.16* - Armado inferior dirección X: - Armado inferior dirección Y:	Mínimo: 10 cm Calculado: 27 cm Calculado: 26 cm	Cumple Cumple
Longitud de anclaje: *Criterio del libro "Cálculo de estructuras de cimentación", J. Calavera. Ed. INTEMAC, 1991* - Armado inf. dirección X hacia der: - Armado inf. dirección X hacia izq: - Armado inf. dirección Y hacia arriba: - Armado inf. dirección Y hacia abajo:	Mínimo: 30 cm Calculado: 41 cm Mínimo: 30 cm Calculado: 41 cm Mínimo: 0 cm Calculado: 0 cm Mínimo: 30 cm Calculado: 41 cm	Cumple Cumple Cumple Cumple
Longitud mínima de las patillas: - Armado inf. dirección X hacia der: - Armado inf. dirección X hacia izq: - Armado inf. dirección Y hacia arriba: - Armado inf. dirección Y hacia abajo:	Mínimo: 25 cm Calculado: 41 cm Calculado: 41 cm Calculado: 41 cm Calculado: 41 cm	Cumple Cumple Cumple Cumple
Tensión máxima en la armadura para limitar la fisuración: - Armado inferior dirección X: - Armado inferior dirección Y:	Máximo: 2520 kp/cm² Calculado: 0 kp/cm² Calculado: 0 kp/cm²	Cumple Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Relación rotura pésima (En dirección X): 0.00		

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: P10 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
- Relación rotura pésima (En dirección Y): 0.00 - Cortante de agotamiento (En dirección X): 0.00 t - Cortante de agotamiento (En dirección Y): 0.00 t		
Referencia: P11 **Dimensiones: 100 x 75 x 35** **Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26**		
Comprobación	Valores	Estado
Tensiones sobre el terreno: *Criterio de CYPE*		
- Tensión media en situaciones persistentes:	Máximo: 1 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión media en situaciones accidentales sísmicas:	Máximo: 1.3 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes sin viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes con viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones accidentales sísmicas:	Máximo: 1.625 kp/cm² Calculado: 0.262 kp/cm²	Cumple
Vuelco de la zapata:		
- En dirección X:		No procede[1]
- En dirección Y:		
Si el % de reserva de seguridad es mayor que cero, quiere decir que los coeficientes de seguridad al vuelco son mayores que los valores estrictos exigidos para todas las combinaciones de equilibrio.	Reserva seguridad: 500.0 %	Cumple
(1) Sin momento de vuelco		
Flexión en la zapata:		
- En dirección X:	Momento: 0.00 t·m	Cumple
- En dirección Y:	Momento: 0.00 t·m	Cumple
Cortante en la zapata:		
- En dirección X:	Cortante: 0.00 t	Cumple
- En dirección Y:	Cortante: 0.00 t	Cumple
Compresión oblicua en la zapata: *Criterio de CYPE*	Máximo: 735 t/m²	
- Situaciones persistentes:	Calculado: 2.77 t/m²	Cumple
- Situaciones accidentales sísmicas:	Calculado: 2.37 t/m²	Cumple
Canto mínimo: *Capítulo C.15.7 (norma NSR-10)*	Mínimo: 23.5 cm Calculado: 35 cm	Cumple
Espacio para anclar arranques en cimentación: - P11:	Mínimo: 20 cm Calculado: 25 cm	Cumple
Cuantía geométrica mínima: *Capítulo C.7.12.2.1 (norma NSR-10)*	Mínimo: 0.0018	
- Armado inferior dirección X:	Calculado: 0.0023	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: P11 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
- Armado inferior dirección Y:	Calculado: 0.0023	Cumple
Diámetro mínimo de las barras: - Parrilla inferior: *Criterio de CYPE*	 Mínimo: 10 mm Calculado: 15.875 mm	 Cumple
Separación máxima entre barras: *Criterio de CYPE*	Máximo: 30 cm	
- Armado inferior dirección X:	Calculado: 27 cm	Cumple
- Armado inferior dirección Y:	Calculado: 26 cm	Cumple
Separación mínima entre barras: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.16*	Mínimo: 10 cm	
- Armado inferior dirección X:	Calculado: 27 cm	Cumple
- Armado inferior dirección Y:	Calculado: 26 cm	Cumple
Longitud de anclaje: *Criterio del libro "Cálculo de estructuras de cimentación", J. Calavera. Ed. INTEMAC, 1991*		
- Armado inf. dirección X hacia der:	Mínimo: 30 cm Calculado: 41 cm	 Cumple
- Armado inf. dirección X hacia izq:	Mínimo: 30 cm Calculado: 41 cm	 Cumple
- Armado inf. dirección Y hacia arriba:	Mínimo: 0 cm Calculado: 0 cm	 Cumple
- Armado inf. dirección Y hacia abajo:	Mínimo: 30 cm Calculado: 41 cm	 Cumple
Longitud mínima de las patillas:	Mínimo: 25 cm	
- Armado inf. dirección X hacia der:	Calculado: 41 cm	Cumple
- Armado inf. dirección X hacia izq:	Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia arriba:	Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia abajo:	Calculado: 41 cm	Cumple
Tensión máxima en la armadura para limitar la fisuración:	Máximo: 2520 kp/cm²	
- Armado inferior dirección X:	Calculado: 0 kp/cm²	Cumple
- Armado inferior dirección Y:	Calculado: 0 kp/cm²	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Relación rotura pésima (En dirección X): 0.00 - Relación rotura pésima (En dirección Y): 0.00 - Cortante de agotamiento (En dirección X): 0.00 t - Cortante de agotamiento (En dirección Y): 0.00 t		

Referencia: P12 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
Tensiones sobre el terreno: *Criterio de CYPE*		

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: P12
Dimensiones: 100 x 75 x 35
Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26

Comprobación	Valores	Estado
- Tensión media en situaciones persistentes:	Máximo: 1 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión media en situaciones accidentales sísmicas:	Máximo: 1.3 kp/cm² Calculado: 0.175 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes sin viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones persistentes con viento:	Máximo: 1.25 kp/cm² Calculado: 0.262 kp/cm²	Cumple
- Tensión máxima en situaciones accidentales sísmicas:	Máximo: 1.625 kp/cm² Calculado: 0.262 kp/cm²	Cumple
Vuelco de la zapata:		
- En dirección X:		No procede[1]
- En dirección Y:		
Si el % de reserva de seguridad es mayor que cero, quiere decir que los coeficientes de seguridad al vuelco son mayores que los valores estrictos exigidos para todas las combinaciones de equilibrio.	Reserva seguridad: 500.0 %	Cumple
(1) Sin momento de vuelco		
Flexión en la zapata:		
- En dirección X:	Momento: 0.00 t·m	Cumple
- En dirección Y:	Momento: 0.00 t·m	Cumple
Cortante en la zapata:		
- En dirección X:	Cortante: 0.00 t	Cumple
- En dirección Y:	Cortante: 0.00 t	Cumple
Compresión oblicua en la zapata:		
Criterio de CYPE	Máximo: 735 t/m²	
- Situaciones persistentes:	Calculado: 2.77 t/m²	Cumple
- Situaciones accidentales sísmicas:	Calculado: 2.37 t/m²	Cumple
Canto mínimo:	Mínimo: 23.5 cm	
Capítulo C.15.7 (norma NSR-10)	Calculado: 35 cm	Cumple
Espacio para anclar arranques en cimentación:	Mínimo: 20 cm	
- P12:	Calculado: 25 cm	Cumple
Cuantía geométrica mínima:		
Capítulo C.7.12.2.1 (norma NSR-10)	Mínimo: 0.0018	
- Armado inferior dirección X:	Calculado: 0.0023	Cumple
- Armado inferior dirección Y:	Calculado: 0.0023	Cumple
Diámetro mínimo de las barras:		
- Parrilla inferior:	Mínimo: 10 mm	
Criterio de CYPE	Calculado: 15.875 mm	Cumple
Separación máxima entre barras:		
Criterio de CYPE	Máximo: 30 cm	
- Armado inferior dirección X:	Calculado: 27 cm	Cumple
- Armado inferior dirección Y:	Calculado: 26 cm	Cumple

Listados

Referencia: P12 Dimensiones: 100 x 75 x 35 Armados: Xi:Ø5/8"c/27 Yi:Ø5/8"c/26		
Comprobación	Valores	Estado
Separación mínima entre barras: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.16*	Mínimo: 10 cm	
- Armado inferior dirección X:	Calculado: 27 cm	Cumple
- Armado inferior dirección Y:	Calculado: 26 cm	Cumple
Longitud de anclaje: *Criterio del libro "Cálculo de estructuras de cimentación", J. Calavera. Ed. INTEMAC, 1991*		
- Armado inf. dirección X hacia der:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección X hacia izq:	Mínimo: 30 cm Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia arriba:	Mínimo: 0 cm Calculado: 0 cm	Cumple
- Armado inf. dirección Y hacia abajo:	Mínimo: 30 cm Calculado: 41 cm	Cumple
Longitud mínima de las patillas:	Mínimo: 25 cm	
- Armado inf. dirección X hacia der:	Calculado: 41 cm	Cumple
- Armado inf. dirección X hacia izq:	Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia arriba:	Calculado: 41 cm	Cumple
- Armado inf. dirección Y hacia abajo:	Calculado: 41 cm	Cumple
Tensión máxima en la armadura para limitar la fisuración:	Máximo: 2520 kp/cm²	
- Armado inferior dirección X:	Calculado: 0 kp/cm²	Cumple
- Armado inferior dirección Y:	Calculado: 0 kp/cm²	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Relación rotura pésima (En dirección X): 0.00 - Relación rotura pésima (En dirección Y): 0.00 - Cortante de agotamiento (En dirección X): 0.00 t - Cortante de agotamiento (En dirección Y): 0.00 t		

3.2. Vigas

3.2.1. Descripción

Referencias	Geometría	Armado
C [P1-P2], C [P2-P3], C [P3-P4], C [P4-P5] y C [P5-P6]	Ancho: 40.0 cm Canto: 40.0 cm	Superior: 2Ø5/8" Inferior: 2Ø5/8" Estribos: 1xØ3/8"c/20
VC.T-1.3 [P7-P8], VC.T-1.3 [P8-P9], VC.T-1.3 [P9-P10], VC.T-1.3 [P10-P11] y VC.T-1.3 [P11-P12]	Ancho: 40.0 cm Canto: 50.0 cm	Superior: 4Ø5/8" Inferior: 3Ø5/8" Piel: 1x2Ø1/2" Estribos: 1xØ3/8"c/20
C [P1-P33], C [P2-P34], C [P3-P35], C [P4-P36], C [P5-P37], C [P6-P38], C [P12-P32], C [P11-P31], C [P10-P30], C [P9-P29], C [P8-P28] y C [P7-P27]	Ancho: 40.0 cm Canto: 40.0 cm	Superior: 2Ø5/8" Inferior: 2Ø5/8" Estribos: 1xØ3/8"c/20

3.2.2. Comprobación

Referencia: C.2.2 [P1-P2] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Anchura mínima de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 40 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Separación máxima estribos: - Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles: - Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 7.46 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de compresión: - Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción: - Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 7.96 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P1-P2] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta: - Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple)		
Referencia: C.2.2 [P2-P3] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Anchura mínima de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 40 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Separación máxima estribos: - Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	

Listados

Referencia: C.2.2 [P2-P3] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles: - Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 7.46 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de compresión: - Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción: - Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 7.96 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta: - Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple)		
Referencia: C.2.2 [P3-P4] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P3-P4] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Anchura mínima de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 40 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Separación máxima estribos: - Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles: - Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 7.46 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de compresión: - Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción: - Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 7.96 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple

Listados

Referencia: C.2.2 [P3-P4] (Viga de atado)
-Dimensiones: 40.0 cm x 40.0 cm
-Armadura superior: 2Ø5/8"
-Armadura inferior: 2Ø5/8"
-Estribos: 1xØ3/8"c/20

Comprobación	Valores	Estado
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta: - Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	Cumple
Se cumplen todas las comprobaciones		

Información adicional:
- Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple)

Referencia: C.2.2 [P4-P5] (Viga de atado)
-Dimensiones: 40.0 cm x 40.0 cm
-Armadura superior: 2Ø5/8"
-Armadura inferior: 2Ø5/8"
-Estribos: 1xØ3/8"c/20

Comprobación	Valores	Estado
Anchura mínima de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 40 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Separación máxima estribos: - Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P4-P5] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles: - Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 7.46 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de compresión: - Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción: - Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 7.96 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	Cumple Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	Cumple Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	Cumple Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	Cumple Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta: - Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple)		
Referencia: C.2.2 [P5-P6] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Anchura mínima de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 40 cm	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P5-P6] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Canto mínimo de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 40 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Separación máxima estribos: - Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles: - Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 7.46 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de compresión: - Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción: - Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 7.96 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	

Referencia: C.2.2 [P5-P6] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta:		
- Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple)		
Referencia: VC.T-1.3 [P7-P8] (Viga centradora) -Dimensiones: 40.0 cm x 50.0 cm -Armadura superior: 4Ø5/8" -Armadura de piel: 1x2Ø1/2" -Armadura inferior: 3Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Anchura mínima de la viga centradora: *Se aplica criterio de viga de atado por tener axiles de compresión.: Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga centradora: *Se aplica criterio de viga de atado por tener axiles de compresión.: Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 50 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 5.5 cm	Cumple
- Armadura inferior:	Calculado: 9.1 cm	Cumple
- Armadura de piel:	Calculado: 14.3 cm	Cumple
Separación máxima estribos: - Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 5.5 cm	Cumple
- Armadura inferior:	Calculado: 9.1 cm	Cumple

Listados

Referencia: VC.T-1.3 [P7-P8] (Viga centradora)
-Dimensiones: 40.0 cm x 50.0 cm
-Armadura superior: 4Ø5/8"
-Armadura de piel: 1x2Ø1/2"
-Armadura inferior: 3Ø5/8"
-Estribos: 1xØ3/8"c/20

Comprobación	Valores	Estado
- Armadura de piel:	Calculado: 14.3 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles: - Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 9.33 cm² Calculado: 16.46 cm²	Cumple
Armadura necesaria por cálculo para el axil de compresión: - Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 16.46 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción: - Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 16.46 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje de las barras de piel origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 26 cm Calculado: 26 cm Calculado: 26 cm	 Cumple Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje de las barras de piel extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 26 cm Calculado: 26 cm Calculado: 26 cm	 Cumple Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta: - Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	Cumple
Se cumplen todas las comprobaciones		
Información adicional:		

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: VC.T-1.3 [P7-P8] (Viga centradora) -Dimensiones: 40.0 cm x 50.0 cm -Armadura superior: 4Ø5/8" -Armadura de piel: 1x2Ø1/2" -Armadura inferior: 3Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
- Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple) - La viga centradora no es necesaria pues no existen momentos en la cimentación		
Referencia: VC.T-1.3 [P8-P9] (Viga centradora) -Dimensiones: 40.0 cm x 50.0 cm -Armadura superior: 4Ø5/8" -Armadura de piel: 1x2Ø1/2" -Armadura inferior: 3Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Anchura mínima de la viga centradora: *Se aplica criterio de viga de atado por tener axiles de compresión.: Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga centradora: *Se aplica criterio de viga de atado por tener axiles de compresión.: Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 50 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 5.5 cm	Cumple
- Armadura inferior:	Calculado: 9.1 cm	Cumple
- Armadura de piel:	Calculado: 14.3 cm	Cumple
Separación máxima estribos:		
- Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 5.5 cm	Cumple
- Armadura inferior:	Calculado: 9.1 cm	Cumple
- Armadura de piel:	Calculado: 14.3 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles: - Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 9.33 cm² Calculado: 16.46 cm²	Cumple
Armadura necesaria por cálculo para el axil de compresión: - Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 16.46 cm²	Cumple



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: VC.T-1.3 [P8-P9] (Viga centradora) -Dimensiones: 40.0 cm x 50.0 cm -Armadura superior: 4Ø5/8" -Armadura de piel: 1x2Ø1/2" -Armadura inferior: 3Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Armadura necesaria por cálculo para el axil de tracción: - Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 16.46 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje de las barras de piel origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 26 cm Calculado: 26 cm Calculado: 26 cm	 Cumple Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje de las barras de piel extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 26 cm Calculado: 26 cm Calculado: 26 cm	 Cumple Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta: - Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	 Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple) - La viga centradora no es necesaria pues no existen momentos en la cimentación		
Referencia: VC.T-1.3 [P9-P10] (Viga centradora) -Dimensiones: 40.0 cm x 50.0 cm -Armadura superior: 4Ø5/8" -Armadura de piel: 1x2Ø1/2" -Armadura inferior: 3Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: VC.T-1.3 [P9-P10] (Viga centradora)
-Dimensiones: 40.0 cm x 50.0 cm
-Armadura superior: 4Ø5/8"
-Armadura de piel: 1x2Ø1/2"
-Armadura inferior: 3Ø5/8"
-Estribos: 1xØ3/8"c/20

Comprobación	Valores	Estado
Anchura mínima de la viga centradora: *Se aplica criterio de viga de atado por tener axiles de compresión.: Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga centradora: *Se aplica criterio de viga de atado por tener axiles de compresión.: Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 50 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 5.5 cm	Cumple
- Armadura inferior:	Calculado: 9.1 cm	Cumple
- Armadura de piel:	Calculado: 14.3 cm	Cumple
Separación máxima estribos: - Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 5.5 cm	Cumple
- Armadura inferior:	Calculado: 9.1 cm	Cumple
- Armadura de piel:	Calculado: 14.3 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles: - Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 9.33 cm² Calculado: 16.46 cm²	Cumple
Armadura necesaria por cálculo para el axil de compresión: - Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 16.46 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción: - Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 16.46 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple



Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: VC.T-1.3 [P9-P10] (Viga centradora)
-Dimensiones: 40.0 cm x 50.0 cm
-Armadura superior: 4Ø5/8"
-Armadura de piel: 1x2Ø1/2"
-Armadura inferior: 3Ø5/8"
-Estribos: 1xØ3/8"c/20

Comprobación	Valores	Estado
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje de las barras de piel origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 26 cm	
- Situaciones persistentes:	Calculado: 26 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 26 cm	Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje de las barras de piel extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 26 cm	
- Situaciones persistentes:	Calculado: 26 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 26 cm	Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta:		
- Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	Cumple

Se cumplen todas las comprobaciones

Información adicional:

- Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple)
- La viga centradora no es necesaria pues no existen momentos en la cimentación

Referencia: VC.T-1.3 [P10-P11] (Viga centradora)
-Dimensiones: 40.0 cm x 50.0 cm
-Armadura superior: 4Ø5/8"
-Armadura de piel: 1x2Ø1/2"
-Armadura inferior: 3Ø5/8"
-Estribos: 1xØ3/8"c/20

Comprobación	Valores	Estado
Anchura mínima de la viga centradora: *Se aplica criterio de viga de atado por tener axiles de compresión.: Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga centradora: *Se aplica criterio de viga de atado por tener axiles de compresión.: Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 50 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: VC.T-1.3 [P10-P11] (Viga centradora)
-Dimensiones: 40.0 cm x 50.0 cm
-Armadura superior: 4Ø5/8"
-Armadura de piel: 1x2Ø1/2"
-Armadura inferior: 3Ø5/8"
-Estribos: 1xØ3/8"c/20

Comprobación	Valores	Estado
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 5.5 cm	Cumple
- Armadura inferior:	Calculado: 9.1 cm	Cumple
- Armadura de piel:	Calculado: 14.3 cm	Cumple
Separación máxima estribos:		
- Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 5.5 cm	Cumple
- Armadura inferior:	Calculado: 9.1 cm	Cumple
- Armadura de piel:	Calculado: 14.3 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles:		
- Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 9.33 cm² Calculado: 16.46 cm²	Cumple
Armadura necesaria por cálculo para el axil de compresión:		
- Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 16.46 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción:		
- Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 16.46 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje de las barras de piel origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 26 cm	
- Situaciones persistentes:	Calculado: 26 cm	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: VC.T-1.3 [P10-P11] (Viga centradora) -Dimensiones: 40.0 cm x 50.0 cm -Armadura superior: 4Ø5/8" -Armadura de piel: 1x2Ø1/2" -Armadura inferior: 3Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
- Situaciones accidentales sísmicas:	Calculado: 26 cm	Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje de las barras de piel extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 26 cm	
- Situaciones persistentes:	Calculado: 26 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 26 cm	Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta: - Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple) - La viga centradora no es necesaria pues no existen momentos en la cimentación		

Referencia: VC.T-1.3 [P11-P12] (Viga centradora) -Dimensiones: 40.0 cm x 50.0 cm -Armadura superior: 4Ø5/8" -Armadura de piel: 1x2Ø1/2" -Armadura inferior: 3Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Anchura mínima de la viga centradora: *Se aplica criterio de viga de atado por tener axiles de compresión.: Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga centradora: *Se aplica criterio de viga de atado por tener axiles de compresión.: Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 24.1 cm Calculado: 50 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 5.5 cm	Cumple
- Armadura inferior:	Calculado: 9.1 cm	Cumple
- Armadura de piel:	Calculado: 14.3 cm	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: VC.T-1.3 [P11-P12] (Viga centradora) -Dimensiones: 40.0 cm x 50.0 cm -Armadura superior: 4Ø5/8" -Armadura de piel: 1x2Ø1/2" -Armadura inferior: 3Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Separación máxima estribos: - Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 5.5 cm	Cumple
- Armadura inferior:	Calculado: 9.1 cm	Cumple
- Armadura de piel:	Calculado: 14.3 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles: - Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 9.33 cm² Calculado: 16.46 cm²	Cumple
Armadura necesaria por cálculo para el axil de compresión: - Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 16.46 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción: - Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 16.46 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje de las barras de piel origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 26 cm	
- Situaciones persistentes:	Calculado: 26 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 26 cm	Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: VC.T-1.3 [P11-P12] (Viga centradora)
-Dimensiones: 40.0 cm x 50.0 cm
-Armadura superior: 4Ø5/8"
-Armadura de piel: 1x2Ø1/2"
-Armadura inferior: 3Ø5/8"
-Estribos: 1xØ3/8"c/20

Comprobación	Valores	Estado
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje de las barras de piel extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 26 cm	
- Situaciones persistentes:	Calculado: 26 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 26 cm	Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta:		
- Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	Cumple

Se cumplen todas las comprobaciones

Información adicional:
- Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple)
- La viga centradora no es necesaria pues no existen momentos en la cimentación

Referencia: C.2.2 [P1-P33] (Viga de atado)
-Dimensiones: 40.0 cm x 40.0 cm
-Armadura superior: 2Ø5/8"
-Armadura inferior: 2Ø5/8"
-Estribos: 1xØ3/8"c/20

Comprobación	Valores	Estado
Anchura mínima de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.7 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.7 cm Calculado: 40 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Separación máxima estribos: - Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple

518
690
694

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P1-P33] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Armadura mínima por cuantía mecánica de esfuerzos axiles: - Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 7.46 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de compresión: - Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción: - Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 7.96 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta: - Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	 Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple)		

Referencia: C.2.2 [P2-P34] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Anchura mínima de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.7 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.7 cm Calculado: 40 cm	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P2-P34] (Viga de atado)
-Dimensiones: 40.0 cm x 40.0 cm
-Armadura superior: 2Ø5/8"
-Armadura inferior: 2Ø5/8"
-Estribos: 1xØ3/8"c/20

Comprobación	Valores	Estado
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Separación máxima estribos: - Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles: - Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 7.46 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de compresión: - Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción: - Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 7.96 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P2-P34] (Viga de atado)
-Dimensiones: 40.0 cm x 40.0 cm
-Armadura superior: 2Ø5/8"
-Armadura inferior: 2Ø5/8"
-Estribos: 1xØ3/8"c/20

Comprobación	Valores	Estado
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta:		
- Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	Cumple
Se cumplen todas las comprobaciones		

Información adicional:

- Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple)

Referencia: C.2.2 [P3-P35] (Viga de atado)
-Dimensiones: 40.0 cm x 40.0 cm
-Armadura superior: 2Ø5/8"
-Armadura inferior: 2Ø5/8"
-Estribos: 1xØ3/8"c/20

Comprobación	Valores	Estado
Anchura mínima de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.7 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.7 cm Calculado: 40 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Separación máxima estribos:		
- Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles:		
- Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 7.46 cm² Calculado: 7.96 cm²	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P3-P35] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Armadura necesaria por cálculo para el axil de compresión: - Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción: - Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 7.96 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta: - Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	 Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple)		

Referencia: C.2.2 [P4-P36] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Anchura mínima de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.7 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.7 cm Calculado: 40 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P4-P36] (Viga de atado)
-Dimensiones: 40.0 cm x 40.0 cm
-Armadura superior: 2Ø5/8"
-Armadura inferior: 2Ø5/8"
-Estribos: 1xØ3/8"c/20

Comprobación	Valores	Estado
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Separación máxima estribos:		
- Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles:		
- Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 7.46 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de compresión:		
- Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción:		
- Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 7.96 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P4-P36] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta: - Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple)		
Referencia: C.2.2 [P5-P37] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Anchura mínima de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.8 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.8 cm Calculado: 40 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Separación máxima estribos: - Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles: - Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 7.46 cm² Calculado: 7.96 cm²	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P5-P37] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Armadura necesaria por cálculo para el axil de compresión: - Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción: - Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 7.96 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta: - Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple)		

Referencia: C.2.2 [P6-P38] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Anchura mínima de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.7 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.7 cm Calculado: 40 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P6-P38] (Viga de atado)
-Dimensiones: 40.0 cm x 40.0 cm
-Armadura superior: 2Ø5/8"
-Armadura inferior: 2Ø5/8"
-Estribos: 1xØ3/8"c/20

Comprobación	Valores	Estado
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Separación máxima estribos: - Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles: - Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 7.46 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de compresión: - Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción: - Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 7.96 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	

Listados



Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P6-P38] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta: - Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple)		
Referencia: C.2.2 [P12-P32] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Anchura mínima de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.6 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.6 cm Calculado: 40 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Separación máxima estribos: - Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles: - Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 7.46 cm² Calculado: 7.96 cm²	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P12-P32] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Armadura necesaria por cálculo para el axil de compresión: - Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción: - Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 7.96 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta: - Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	 Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple)		

Referencia: C.2.2 [P11-P31] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Anchura mínima de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.6 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.6 cm Calculado: 40 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P11-P31] (Viga de atado)
-Dimensiones: 40.0 cm x 40.0 cm
-Armadura superior: 2Ø5/8"
-Armadura inferior: 2Ø5/8"
-Estribos: 1xØ3/8"c/20

Comprobación	Valores	Estado
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Separación máxima estribos: - Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles: - Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 7.46 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de compresión: - Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción: - Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 7.96 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P11-P31] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta: - Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple)		
Referencia: C.2.2 [P10-P30] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Anchura mínima de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.7 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.7 cm Calculado: 40 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Separación máxima estribos: - Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles: - Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 7.46 cm² Calculado: 7.96 cm²	Cumple

530
707
706

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P10-P30] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Armadura necesaria por cálculo para el axil de compresión: - Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción: - Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 7.96 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	Cumple Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	Cumple Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	Cumple Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	Cumple Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta: - Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple)		
Referencia: C.2.2 [P9-P29] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Anchura mínima de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.7 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.7 cm Calculado: 40 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P9-P29] (Viga de atado)
-Dimensiones: 40.0 cm x 40.0 cm
-Armadura superior: 2Ø5/8"
-Armadura inferior: 2Ø5/8"
-Estribos: 1xØ3/8"c/20

Comprobación	Valores	Estado
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Separación máxima estribos:		
- Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles:		
- Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 7.46 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de compresión:		
- Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción:		
- Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 7.96 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P9-P29] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta: - Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple)		
Referencia: C.2.2 [P8-P28] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Anchura mínima de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.7 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.7 cm Calculado: 40 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Separación máxima estribos: - Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles: - Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 7.46 cm² Calculado: 7.96 cm²	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P8-P28] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Armadura necesaria por cálculo para el axil de compresión: - Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción: - Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 7.96 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares* - Situaciones persistentes: - Situaciones accidentales sísmicas:	Mínimo: 32 cm Calculado: 32 cm Calculado: 32 cm	 Cumple Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta: - Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple)		
Referencia: C.2.2 [P7-P27] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
Anchura mínima de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.7 cm Calculado: 40 cm	Cumple
Canto mínimo de la viga de atado: *Norma NSR-10. Artículo C.21.12.3.2*	Mínimo: 14.7 cm Calculado: 40 cm	Cumple
Diámetro mínimo estribos:	Mínimo: 6 mm Calculado: 9.525 mm	Cumple

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P7-P27] (Viga de atado)
-Dimensiones: 40.0 cm x 40.0 cm
-Armadura superior: 2Ø5/8"
-Armadura inferior: 2Ø5/8"
-Estribos: 1xØ3/8"c/20

Comprobación	Valores	Estado
Separación mínima entre estribos: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm Calculado: 19 cm	Cumple
Separación mínima armadura longitudinal: *Norma NSR-10. Artículo C.7.6*	Mínimo: 4 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Separación máxima estribos: - Sin cortantes: *Norma NSR-10. Artículo C.7.10.5.2*	Máximo: 25.4 cm Calculado: 20 cm	Cumple
Recomendación para la separación máxima de estribos en vigas comprimidas por axiles en combinaciones sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Máximo: 23.8 cm Calculado: 20 cm	Cumple
Separación máxima armadura longitudinal: *Artículo 42.3.1 de la norma EHE-08*	Máximo: 30 cm	
- Armadura superior:	Calculado: 19.9 cm	Cumple
- Armadura inferior:	Calculado: 19.9 cm	Cumple
Armadura mínima por cuantía mecánica de esfuerzos axiles: - Armadura total (Situaciones accidentales sísmicas): *Criterio de CYPE basado en el Artículo 38.4 de la EH-91*	Mínimo: 7.46 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de compresión: - Situaciones accidentales sísmicas: *Norma NSR-10. Artículo C.10.3.6.2*	Mínimo: 0 cm² Calculado: 7.96 cm²	Cumple
Armadura necesaria por cálculo para el axil de tracción: - Situaciones accidentales sísmicas: *Criterio de CYPE, basado en: J. Calavera. "Cálculo de Estructuras de Cimentación". Capítulo 3.15*	Mínimo: 0.01 cm² Calculado: 7.96 cm²	Cumple
Longitud de anclaje barras superiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores origen: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras superiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Longitud de anclaje barras inferiores extremo: *El anclaje se realiza a partir del eje de los pilares*	Mínimo: 32 cm	

Listados

Diseño cubierta polideportivo Vda El Cedro Mpio de Tarqui

Referencia: C.2.2 [P7-P27] (Viga de atado) -Dimensiones: 40.0 cm x 40.0 cm -Armadura superior: 2Ø5/8" -Armadura inferior: 2Ø5/8" -Estribos: 1xØ3/8"c/20		
Comprobación	Valores	Estado
- Situaciones persistentes:	Calculado: 32 cm	Cumple
- Situaciones accidentales sísmicas:	Calculado: 32 cm	Cumple
Comprobación de armadura necesaria por cálculo a flexión compuesta: - Situaciones accidentales sísmicas:	Momento flector: 0.00 t·m Axil: ± 0.06 t	Cumple
Se cumplen todas las comprobaciones		
Información adicional: - Diámetro mínimo de la armadura longitudinal (Recomendación del Artículo 58.8.2 de la EHE-08): Mínimo: 12.0 mm, Calculado: 15.9 mm (Cumple)		

DISEÑADO POR:

GERMAN ALONSO LOZADA LOZADA

INGENIERO CIVIL

ESPECIALISTA EN ESTRUCTURAS

~~536~~
~~705~~
712

1. DATOS DE ENTRADA

Unidades: Kgf, m

Velocidad Viento (km/h)	100
Altura Cornisa (he)	6.75
Altura Cumbrera (hr)	9.23
Ancho Edificación (L)	18.2
Largo Edificación (B)	30.46
Factor Topografía (Ft)	1
Factor Dirección (Fd)	.85
Relación Amortiguamiento	0.05
Dirección Viento (Cumbrera)	Normal
Tipo de Cubierta	Dos Aguas
Tipo Edificación	Abierto
Exposición	B
Ocupación	II

2. RESULTADOS

Angulo de Techo	15.24
Altura Media	7.99
Coef. Muro Barlov.	0.80
Coef. Muro Sotav.	-0.50
Coef. Muro Lat.	-0.70
Coef. Pres. Int. -	0.00
Coef. Pres. Int. +	0.00
Presión x Vel.	28.10
Factor de Ráfaga	0.84
Peridodo (segs.)	0.38

Coef. Pres. Cubierta Zona 1	0.00	0.00
Coef. Pres. Cubierta Zona 2	0.00	0.00
Coef. Pres. Cubierta Zona 3	0.00	0.00
Coef. Pres. Cubierta Zona 4	0.00	0.00

Z	Kz	Qz	Cp	W/+GCpi	W/-GCpi
0.00	0.34	14.01	0.80	9.46	9.46
4.00	0.34	14.01	0.80	9.46	9.46
6.00	0.38	15.73	0.80	10.62	10.62
8.00	0.41	17.07	0.80	11.53	11.53
9.00	0.42	17.66	0.80	11.93	11.93

	Cp	W/+GCpi	W/-GCpi
Muro Sotavento	-0.50	-11.86	-11.86
Paredes Laterales	-0.70	-16.61	-16.61
Techo Barl 1	-0.13	-3.01	-3.01
Techo Barl 2	0.00	0.00	0.00
Techo Sotavento	-0.50	-11.98	-11.98

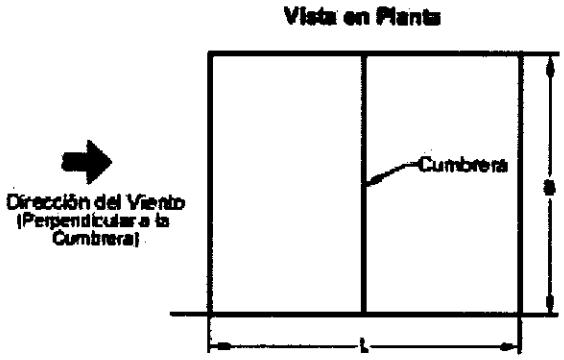
Presión neta para cubiertas en edificaciones abiertas

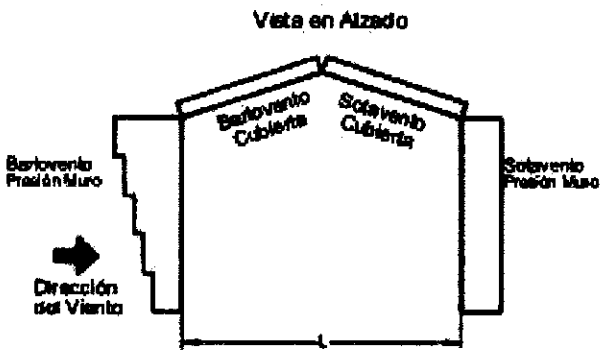
	CN	PCN
PCNWLA	1.1	26.10
PCNLLA	-0.3837027	-9.10

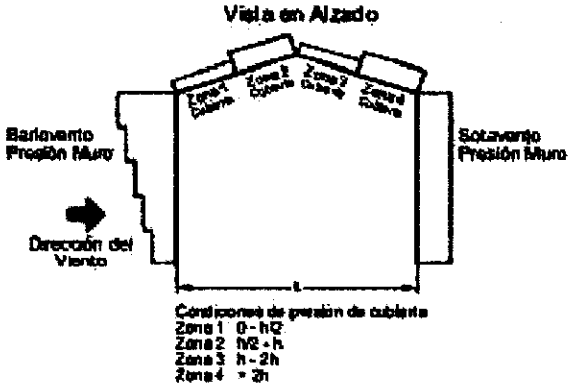
Elementos calculados con el programa de diseño Arquimet 2.0

	CN	PCN
PCNWOA	-1.2	-28.47
PCNLOA	-1.006519	-23.88
PCNWLB	0.09348106	2.22
PCNLLB	-1.090222	-25.86
PCNWOB	-0.6065189	-14.39
PCNLOB	-1.603259	-38.03

3. ESQUEMA DE APLICACIÓN DE CARGAS







Memorias de Cálculo

PROGRAMA DE DISENO Y CALCULO ESTRUCTURAL
ARQUIMET 2.0

Proyecto: _____ **Fecha:** _____

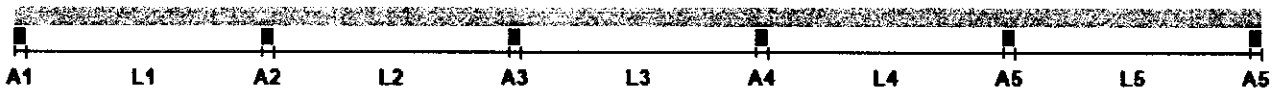
Ingeniero: _____ **Firma:** _____

Elementos calculados con el programa de diseño Arquimet 2.0 de ACESCO

REPORTE DE CORREAS

PHR Cajón 160 x 60 x 20 (1.20 mm)
con Fy = 35.15 Kgf/mm² cada 1.10 m sin arriostramiento interior.

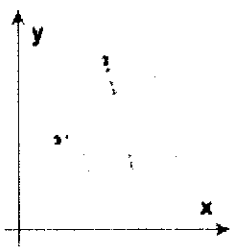
SECCION LONGITUDINAL

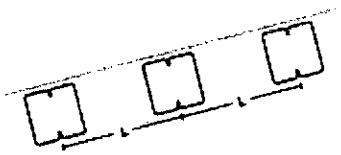


L1	5.82 m
L2	5.82 m
L3	5.82 m
L4	5.82 m
L5	5.82 m
A1	0.30 m
A2	0.30 m
A3	0.30 m
A4	0.30 m
A5	0.30 m
A6	0.30 m

CONFIGURACION	
TIPO DE CARGA	DISTRIBUIDA
Carga muerta	0.02 Ton/m²
Peso propio correa	0.01 Ton/m
Carga viva	0.05 Ton/m²
Carga granizo	0.00 Ton/m²
Viento compresión (Perpendicular)	0.04 Ton/m²
Viento succión (Perpendicular)	0.04 Ton/m²
Pendiente sección transversal	14.112° = 25.1410%

SECCION TRANSVERSAL





L = 1.10 m

716 540 772

Memorias de Cálculo

PROGRAMA DE DISENO Y CALCULO ESTRUCTURAL
ARQUIMET 2.0

Proyecto: _____ Fecha: _____

Ingeniero: _____ Firma: _____

Elementos calculados con el programa de diseño Arquimet 2.0 de ACESCO

REPORTES DE DISEÑO

REPORTE FLEXION				
	Apoyos		Interiores	
Ejes locales	3	2	3	2
Resistente (Ton.m)	1.0777	0.4948	1.0777	0.4948
Calculado (Ton.m)	0.5758	0.1229	0.5758	0.1229

REPORTE CORTANTE		
Ejes locales	2	3
Resistente (Ton)	2.2270	4.5782
Calculado (Ton)	0.5382	0.1149

REPORTE DEFLEXION		
Deflexiones máximas	Instantanea	Permanente
Admisible (m)	0.0227	0.0000
Calculado (m)	0.0081	0.0000

Memorias de Cálculo

PROGRAMA DE DISENO Y CALCULO ESTRUCTURAL
ARQUIMET 2.0

Proyecto: _____ **Fecha:** _____

Ingeniero: _____ **Firma:** _____

Elementos calculados con el programa de diseño Arquimet 2.0 de ACESCO

COMBINACIONES DE CARGA					
No	Muerta	Viva	Granizo	Viento compresión	Viento succión
1	1.4000	0.0000	0.0000	0.0000	0.0000
2	1.2000	0.5000	0.0000	0.0000	0.0000
3	1.2000	0.0000	0.5000	0.0000	0.0000
4	1.2000	1.6000	0.0000	0.5000	0.0000
5	1.2000	0.0000	1.6000	0.5000	0.0000
6	1.2000	1.6000	0.0000	0.0000	0.5000
7	1.2000	0.0000	1.6000	0.0000	0.5000
8	1.2000	0.5000	0.0000	0.0000	1.0000
9	1.2000	0.0000	0.5000	0.0000	1.0000
10	1.2000	0.5000	0.0000	1.0000	0.0000
11	1.2000	0.0000	0.5000	1.0000	0.0000
12	0.9000	0.0000	0.0000	0.0000	1.0000
13	0.9000	0.0000	0.0000	1.0000	0.0000

Memorias de Cálculo

PROGRAMA DE DISENO Y CALCULO ESTRUCTURAL
ARQUIMET 2.0

Proyecto: _____ **Fecha:** _____

Ingeniero: _____ **Firma:** _____

REACCIONES - EJES GLOBALES (Ton-m)

Elementos calculados con el programa de diseño Arquimet 2.0 de ACESCO

APOYO 1		
Combinacion	Rx	Ry
Muerta	4.1944E-09	0.0803
Viva de Cub.	3.6867E-10	0.1329
Granizo	0.0000	0.0000
Viento Comp.	-0.0259	0.1031
Viento Succion	0.0259	-0.1031
Comb. 1	6.2483E-09	0.1125
Comb. 2	2.6154E-09	0.1628
Comb. 3	6.1411E-09	0.0964
Comb. 4	-0.0130	0.3605
Comb. 5	-0.0130	0.1479
Comb. 6	-0.0130	0.3605
Comb. 7	-0.0130	0.1479
Comb. 8	-0.0259	0.2659
Comb. 9	-0.0259	0.1995
Comb. 10	-0.0259	0.2659
Comb. 11	-0.0259	0.1995
Comb. 12	-0.0259	0.1754
Comb. 13	-0.0259	0.1754

APOYO 2		
Combinacion	Rx	Ry
Muerta	1.4509E-10	0.2303
Viva de Cub.	2.7944E-09	0.3809
Granizo	0.0000	0.0000
Viento Comp.	-0.0743	0.2955
Viento Succion	0.0743	-0.2955
Comb. 1	6.8873E-09	0.3224
Comb. 2	3.0428E-09	0.4668
Comb. 3	1.6456E-09	0.2763
Comb. 4	-0.0371	1.0335
Comb. 5	-0.0371	0.4241
Comb. 6	-0.0371	1.0335
Comb. 7	-0.0371	0.4241
Comb. 8	-0.0743	0.7623
Comb. 9	-0.0743	0.5718
Comb. 10	-0.0743	0.7623
Comb. 11	-0.0743	0.5718
Comb. 12	-0.0743	0.5028
Comb. 13	-0.0743	0.5028

APOYO 3		
Combinacion	Rx	Ry
Muerta	3.6717E-09	0.1981
Viva de Cub.	4.1185E-09	0.3277
Granizo	0.0000	0.0000
Viento Comp.	-0.0639	0.2543
Viento Succion	0.0639	-0.2543
Comb. 1	6.6368E-09	0.2774
Comb. 2	3.4931E-09	0.4016
Comb. 3	5.1335E-09	0.2378
Comb. 4	-0.0320	0.8893
Comb. 5	-0.0320	0.3649
Comb. 6	-0.0320	0.8893
Comb. 7	-0.0320	0.3649
Comb. 8	-0.0639	0.6559
Comb. 9	-0.0639	0.4921
Comb. 10	-0.0639	0.6559
Comb. 11	-0.0639	0.4921
Comb. 12	-0.0639	0.4326
Comb. 13	-0.0639	0.4326

APOYO 4		
Combinacion	Rx	Ry
Muerta	-4.8678E-11	0.1981
Viva de Cub.	4.1185E-09	0.3277
Granizo	0.0000	0.0000
Viento Comp.	-0.0639	0.2543
Viento Succion	0.0639	-0.2543
Comb. 1	-8.0391E-10	0.2774
Comb. 2	-3.9476E-09	0.4016
Comb. 3	1.4131E-09	0.2378
Comb. 4	-0.0320	0.8893
Comb. 5	-0.0320	0.3649
Comb. 6	-0.0320	0.8893
Comb. 7	-0.0320	0.3649
Comb. 8	-0.0639	0.6559
Comb. 9	-0.0639	0.4921
Comb. 10	-0.0639	0.6559
Comb. 11	-0.0639	0.4921
Comb. 12	-0.0639	0.4326
Comb. 13	-0.0639	0.4326

APOYO 5		
Combinacion	Rx	Ry
Muerta	3.8447E-09	0.2303
Viva de Cub.	1.0194E-08	0.3809
Granizo	0.0000	0.0000
Viento Comp.	-0.0743	0.2955
Viento Succion	0.0743	-0.2955
Comb. 1	6.8873E-09	0.3224
Comb. 2	1.0442E-08	0.4668
Comb. 3	9.0448E-09	0.2763
Comb. 4	-0.0371	1.0335
Comb. 5	-0.0371	0.4241
Comb. 6	-0.0371	1.0335
Comb. 7	-0.0371	0.4241
Comb. 8	-0.0743	0.7623
Comb. 9	-0.0743	0.5718
Comb. 10	-0.0743	0.7623
Comb. 11	-0.0743	0.5718
Comb. 12	-0.0743	0.5028
Comb. 13	-0.0743	0.5028

APOYO 6		
Combinacion	Rx	Ry
Muerta	-1.3654E-09	0.0803
Viva de Cub.	-3.3309E-09	0.1329
Granizo	0.0000	0.0000
Viento Comp.	-0.0259	0.1031
Viento Succion	0.0259	-0.1031
Comb. 1	-3.0214E-09	0.1125
Comb. 2	-1.0841E-09	0.1628
Comb. 3	-1.2685E-09	0.0964
Comb. 4	-0.0130	0.3605
Comb. 5	-0.0130	0.1479
Comb. 6	-0.0130	0.3605
Comb. 7	-0.0130	0.1479
Comb. 8	-0.0259	0.2659
Comb. 9	-0.0259	0.1995
Comb. 10	-0.0259	0.2659
Comb. 11	-0.0259	0.1995
Comb. 12	-0.0259	0.1754
Comb. 13	-0.0259	0.1754

Memorias de Cálculo

PROGRAMA DE DISENO Y CALCULO ESTRUCTURAL
ARQUIMET 2.0

Proyecto: _____ Fecha: _____

Ingeniero: _____ Firma: _____

FUERZAS INTERNAS - EJES LOCALES (Ton-m) *Elementos calculados con el programa de diseño Arquimet 2.0 de ACESCO*

APOYO 1				
Combinacion	R2	R3	M2	M3
Muerta	0.0196	0.0779	3.9062E-09	1.5625E-08
Viva de Cub.	0.0324	0.1289	3.9062E-09	1.5625E-08
Granizo	0.0000	0.0000	0.0000	0.0000
Viento Comp.	0.0000	0.1063	0.0000	3.1250E-08
Viento Succion	0.0000	0.1063	0.0000	3.1250E-08
Comb. 1	0.0274	0.1091	5.4687E-09	2.1875E-08
Comb. 2	0.0397	0.1579	6.6406E-09	2.6562E-08
Comb. 3	0.0235	0.0935	4.6875E-09	1.8750E-08
Comb. 4	0.0753	0.3528	1.0938E-08	5.9375E-08
Comb. 5	0.0235	0.1466	4.6875E-09	3.4375E-08
Comb. 6	0.0753	0.3528	1.0938E-08	5.9375E-08
Comb. 7	0.0235	0.1466	4.6875E-09	3.4375E-08
Comb. 8	0.0397	0.2642	6.6406E-09	5.7812E-08
Comb. 9	0.0235	0.1998	4.6875E-09	5.0000E-08
Comb. 10	0.0397	0.2642	6.6406E-09	5.7812E-08
Comb. 11	0.0235	0.1998	4.6875E-09	5.0000E-08
Comb. 12	0.0176	0.1764	3.5156E-09	4.5313E-08
Comb. 13	0.0176	0.1764	3.5156E-09	4.5313E-08

APOYO 2				
Combinacion	R2	R3	M2	M3
Muerta	0.0561	0.2233	0.0320	-0.1271
Viva de Cub.	0.0929	0.3694	0.0529	-0.2103
Granizo	0.0000	0.0000	0.0000	0.0000
Viento Comp.	0.0000	0.3047	0.0000	-0.1735
Viento Succion	0.0000	0.3047	0.0000	-0.1735
Comb. 1	0.0786	0.3127	0.0447	-0.1780
Comb. 2	0.1138	0.4527	0.0648	-0.2577
Comb. 3	0.0674	0.2680	0.0384	-0.1526
Comb. 4	0.2160	1.0114	0.1229	-0.5758
Comb. 5	0.0674	0.4203	0.0384	-0.2393
Comb. 6	0.2160	1.0114	0.1229	-0.5758
Comb. 7	0.0674	0.4203	0.0384	-0.2393
Comb. 8	0.1138	0.7574	0.0648	-0.4312
Comb. 9	0.0674	0.5727	0.0384	-0.3260
Comb. 10	0.1138	0.7574	0.0648	-0.4312
Comb. 11	0.0674	0.5727	0.0384	-0.3260
Comb. 12	0.0505	0.5057	0.0288	-0.2879
Comb. 13	0.0505	0.5057	0.0288	-0.2879

APOYO 3				
Combinacion	R2	R3	M2	M3
Muerta	0.0483	0.1922	0.0240	-0.0954
Viva de Cub.	0.0799	0.3179	0.0397	-0.1577
Granizo	0.0000	0.0000	0.0000	0.0000
Viento Comp.	0.0000	0.2622	0.0000	-0.1301
Viento Succion	0.0000	0.2622	0.0000	-0.1301
Comb. 1	0.0676	0.2690	0.0336	-0.1335
Comb. 2	0.0979	0.3895	0.0486	-0.1933
Comb. 3	0.0580	0.2306	0.0288	-0.1144
Comb. 4	0.1858	0.8703	0.0922	-0.4318
Comb. 5	0.0580	0.3617	0.0288	-0.1795
Comb. 6	0.1858	0.8703	0.0922	-0.4318
Comb. 7	0.0580	0.3617	0.0288	-0.1795
Comb. 8	0.0979	0.6517	0.0486	-0.3234
Comb. 9	0.0580	0.4928	0.0288	-0.2445
Comb. 10	0.0979	0.6517	0.0486	-0.3234
Comb. 11	0.0580	0.4928	0.0288	-0.2445
Comb. 12	0.0435	0.4351	0.0216	-0.2159
Comb. 13	0.0435	0.4351	0.0216	-0.2159

APOYO 4				
Combinacion	R2	R3	M2	M3
Muerta	0.0483	0.1922	0.0240	-0.0954
Viva de Cub.	0.0799	0.3179	0.0397	-0.1577
Granizo	0.0000	0.0000	0.0000	0.0000
Viento Comp.	0.0000	0.2622	0.0000	-0.1301
Viento Succion	0.0000	0.2622	0.0000	-0.1301
Comb. 1	0.0676	0.2690	0.0336	-0.1335
Comb. 2	0.0979	0.3895	0.0486	-0.1933
Comb. 3	0.0580	0.2306	0.0288	-0.1144
Comb. 4	0.1858	0.8703	0.0922	-0.4318
Comb. 5	0.0580	0.3617	0.0288	-0.1795
Comb. 6	0.1858	0.8703	0.0922	-0.4318
Comb. 7	0.0580	0.3617	0.0288	-0.1795
Comb. 8	0.0979	0.6517	0.0486	-0.3234
Comb. 9	0.0580	0.4928	0.0288	-0.2445
Comb. 10	0.0979	0.6517	0.0486	-0.3234
Comb. 11	0.0580	0.4928	0.0288	-0.2445
Comb. 12	0.0435	0.4351	0.0216	-0.2159
Comb. 13	0.0435	0.4351	0.0216	-0.2159

Memorias de Cálculo

PROGRAMA DE DISENO Y CALCULO ESTRUCTURAL
ARQUIMET 2.0

Proyecto: _____ **Fecha:** _____

Ingeniero: _____ **Firma:** _____

FUERZAS INTERNAS - EJES LOCALES (Ton-m) *Elementos calculados con el programa de diseño Arquimet 2.0 de ACESCO*

APOYO 5				
Combinacion	R2	R3	M2	M3
Muerta	0.0561	0.2233	0.0320	-0.1271
Viva de Cub.	0.0929	0.3694	0.0529	-0.2103
Granizo	0.0000	0.0000	0.0000	0.0000
Viento Comp.	0.0000	0.3047	0.0000	-0.1735
Viento Succion	0.0000	0.3047	0.0000	-0.1735
Comb. 1	0.0786	0.3127	0.0447	-0.1780
Comb. 2	0.1138	0.4527	0.0648	-0.2577
Comb. 3	0.0674	0.2680	0.0384	-0.1526
Comb. 4	0.2160	1.0114	0.1229	-0.5758
Comb. 5	0.0674	0.4203	0.0384	-0.2393
Comb. 6	0.2160	1.0114	0.1229	-0.5758
Comb. 7	0.0674	0.4203	0.0384	-0.2393
Comb. 8	0.1138	0.7574	0.0648	-0.4312
Comb. 9	0.0674	0.5727	0.0384	-0.3260
Comb. 10	0.1138	0.7574	0.0648	-0.4312
Comb. 11	0.0674	0.5727	0.0384	-0.3260
Comb. 12	0.0505	0.5057	0.0288	-0.2879
Comb. 13	0.0505	0.5057	0.0288	-0.2879

APOYO 6				
Combinacion	R2	R3	M2	M3
Muerta	0.0196	0.0779	-1.7578E-08	3.1250E-08
Viva de Cub.	0.0324	0.1289	-3.9062E-08	1.0938E-07
Granizo	0.0000	0.0000	0.0000	0.0000
Viento Comp.	0.0000	0.1063	0.0000	-1.5625E-08
Viento Succion	0.0000	0.1063	0.0000	-1.5625E-08
Comb. 1	0.0274	0.1091	-2.4609E-08	4.3750E-08
Comb. 2	0.0397	0.1579	-4.0625E-08	9.2188E-08
Comb. 3	0.0235	0.0935	-2.1094E-08	3.7500E-08
Comb. 4	0.0753	0.3528	-8.3594E-08	2.0469E-07
Comb. 5	0.0235	0.1466	-2.1094E-08	2.9688E-08
Comb. 6	0.0753	0.3528	-8.3594E-08	2.0469E-07
Comb. 7	0.0235	0.1466	-2.1094E-08	2.9688E-08
Comb. 8	0.0397	0.2642	-4.0625E-08	7.6563E-08
Comb. 9	0.0235	0.1998	-2.1094E-08	2.1875E-08
Comb. 10	0.0397	0.2642	-4.0625E-08	7.6563E-08
Comb. 11	0.0235	0.1998	-2.1094E-08	2.1875E-08
Comb. 12	0.0176	0.1764	-1.5820E-08	1.2500E-08
Comb. 13	0.0176	0.1764	-1.5820E-08	1.2500E-08

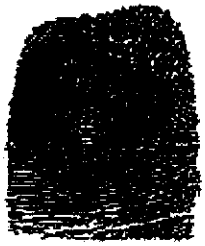
REPUBLICA DE COLOMBIA
IDENTIFICACION PERSONAL
CEDULA DE CIUDADANIA

NUMERO 12.234.265

LOZADA LOZADA
APELLIDOS

GERMAN ALONSO
NOMBRES





INDICE DERECHO

FECHA DE NACIMIENTO 06-JUN-1969
CALI
(VALLE)
LUGAR DE NACIMIENTO

1.71 ESTATURA | O+ G.S. RH | M SEXO

11-AGO-1987 PITALITO
FECHA Y LUGAR DE EXPEDICION

REGISTRADOR NACIONAL



A-1806100-5012061 1-M-0012234265-20041110 0071204310102 137328461

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MEMORIAL DE RESPONSABILIDAD

El suscrito, **GERMAN ALONSO LOZADA LOZADA,** identificado con cédula de ciudadanía No 12.234.265 de Pitalito, registra Matricula Profesional de Ingeniería Civil No. 19202-67671 CAU, de la cual anexo copia.

CERTIFICO QUE:

Realicé el Diseño Estructural pertinente al proyecto denominado: **"CONSTRUCCION CUBIERTA CON ILUMINACION DEL POLIDEPORTIVO DE LA VEREDA EL CEDRO DEL MUNICIPIO DE TARQUI HUILA"** derivado del Contrato No. CM 0008 de 2024, cuyo objeto es: **"CONSULTORIA PARA REALIZAR LOS ESTUDIOS Y DISEÑOS PARA LA CONSTRUCCIÓN DE LA CUBIERTA DE POLIDEPORTIVO DE LAS VEREDAS EUREKA Y CEDRO; INFRAESTRUCTURA DEPORTIVA VEREDA RICABRISA; CONSTRUCCIÓN DE RESTAURANTE ESCOLAR VEREDA LA ESMERALDA Y CONSTRUCCIÓN REDES DE ALCANTARILLADO SANITARIO VEREDA LA PAMPA, PARA EL MUNICIPIO DE TARQUI DEPARTAMENTO DEL HUILA",** localizado en el municipio de Tarqui, en el Departamento del Huila, de acuerdo a la normatividad y especificaciones técnicas y el marco jurídico vigente en el Territorio Nacional.

Mediante la presente certificación, me responsabilizo por los estudios mencionados, teniendo en cuenta que, en el momento de ejecutarse la obra, su construcción debe ceñirse a las directrices técnicas y diseños entregados a satisfacción realizados por el suscrito.

Atentamente,

GERMAN ALONSO LOZADA LOZADA.
C.C. No 12.234.265 de Pitalito.
MP No. 19202-67671 CAU,

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REPÚBLICA DE COLOMBIA
COPNIA
Consejo Profesional Nacional de Ingeniería

Certificado de vigencia y antecedentes disciplinarios
CVAD-2025-4099931

CONSEJO PROFESIONAL NACIONAL DE INGENIERÍA
COPNIA

EL DIRECTOR GENERAL

CERTIFICA:

1. Que GERMAN ALONSO LOZADA LOZADA, identificado(a) con CEDULA DE CIUDADANIA 12234265, se encuentra inscrito(a) en el Registro Profesional Nacional que lleva esta entidad, en la profesión de INGENIERIA CIVIL con MATRICULA PROFESIONAL 19202-67671 desde el 15 de Septiembre de 1997, otorgado(a) mediante Resolución Nacional 992.

2. Que el(la) MATRICULA PROFESIONAL es la autorización que expide el Estado para que el titular ejerza su profesión en todo el territorio de la República de Colombia, de conformidad con lo dispuesto en la Ley 842 de 2003.

3. Que el(la) referido(a) MATRICULA PROFESIONAL se encuentra **VIGENTE**

4. Que el profesional no tiene antecedentes disciplinarios ético-profesionales.

5. Que la presente certificación se expide en Bogotá, D.C., a los tres (03) días del mes de Diciembre del año dos mil veinticinco (2025).

Rubén Dario Ochoa Arbeláez

Firmal del titular (*)

(*)Con el fin de verificar que el titular autoriza su participación en procesos estatales de selección de contratistas. La falta de firma del titular no invalida el Certificado
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Para verificar la integridad e inalterabilidad del presente documento consulte en el sitio web https://tramites.copnia.gov.co/Copnia_Micrositе/CertificateOfGoodStanding/CertificateOfGoodStandingStart indicado el número del certificado que se encuentra en la esquina superior derecha de este documento.

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